



Experience with WBG Converters and Motor Drives

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HMW VSD Workshop
NIST, Gaithersburg, MD
April 16, 2014

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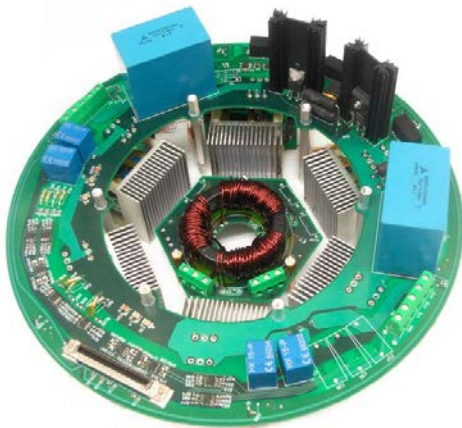


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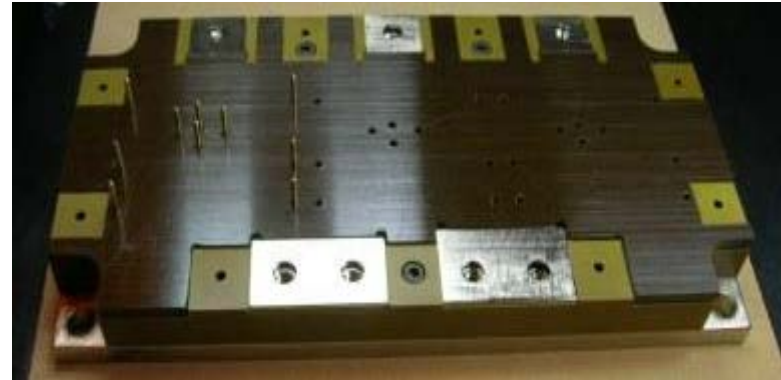


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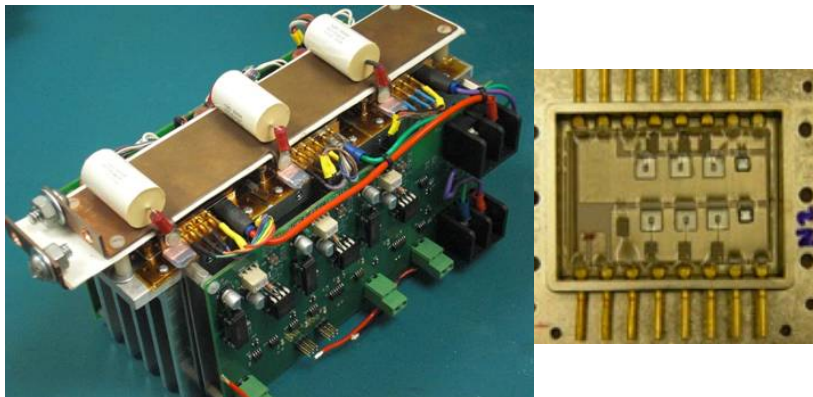
WBG Related Work



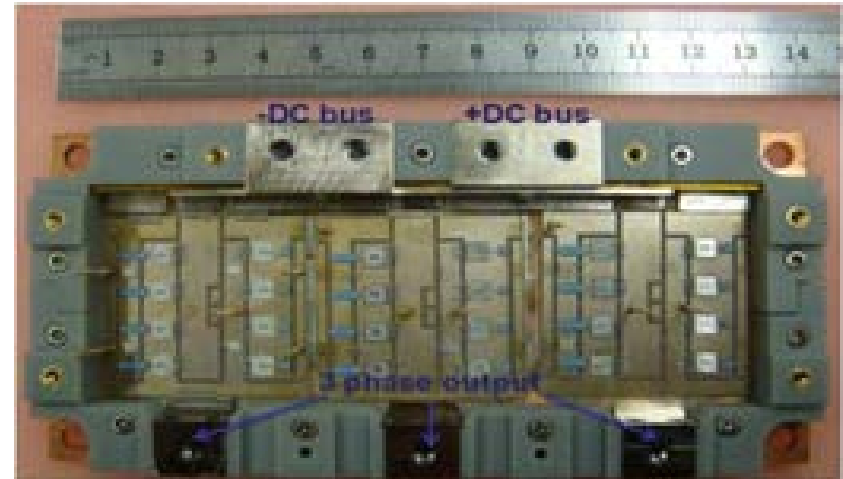
**250 °C SiC High-density
Three-level Motor Drive**



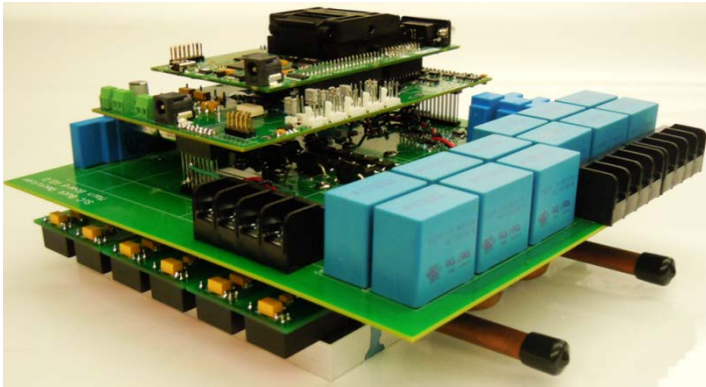
**60 kW SiC Three-phase
Inverter Module**



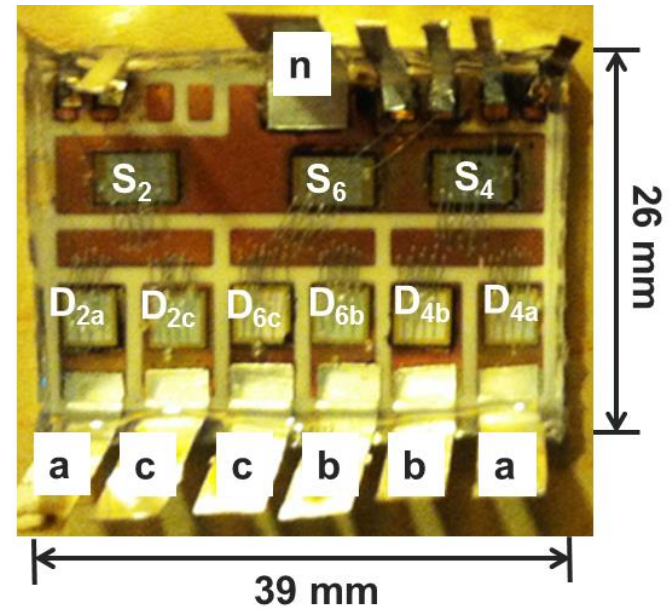
18 kW All SiC Inverter



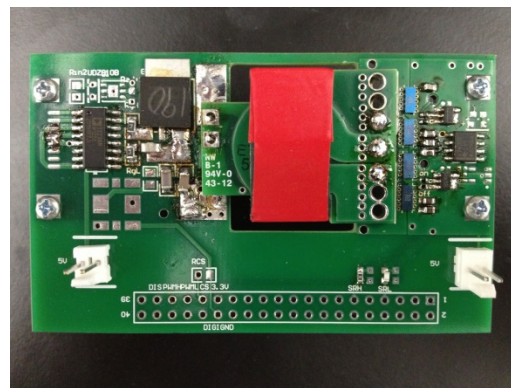
WBG Related Work



**7.5 kW, 480V to 400V
98.8% SiC Rectifier**

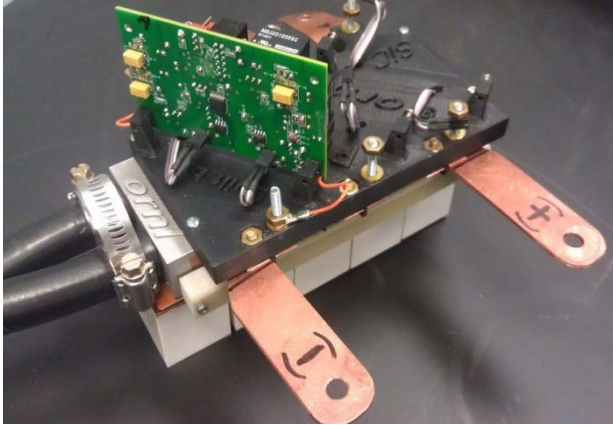


**480V to 400V Low Loss
SiC Rectifier Module**



**300W, 400 to 12 V,
96.6% GaN DC/DC IBC**

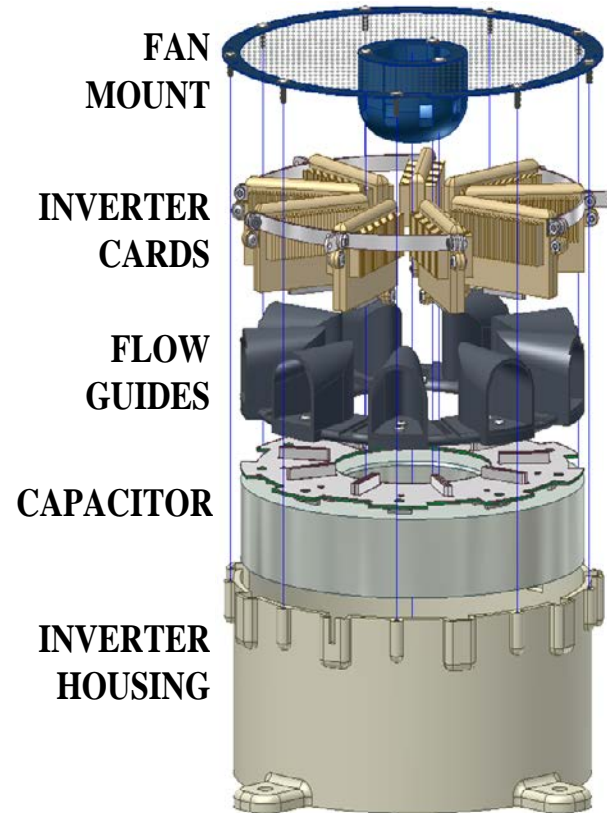
WBG Related Work - ORNL



50% PRINTED ALL-SiC Inverter



**100A/1200V SiC Phase-leg Module
with Integrated Cooling**



ORNL Motor R&D

- Machine Types
 - Field Excitation
 - Novel Flux Coupling
 - Brushless Field Excitation
 - SR Motors
 - Axial Gap
- Development and Utilization of New Materials Complimentary to WBG Drive
 - High Frequency
 - Low Loss

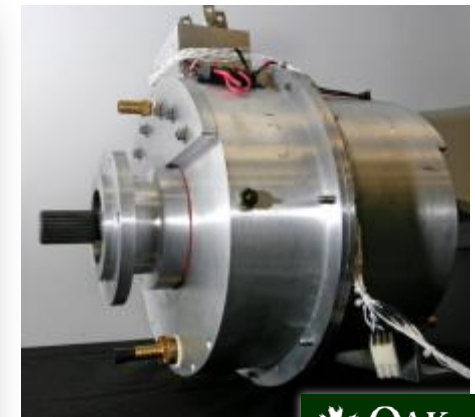
Novel Flux Coupling Motor



Axial Gap Stator



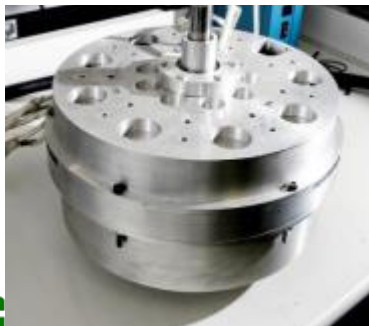
16,000 rpm Brushless Field Excitation (BFE) Motor



Multiple Isolated Flux Path SR Motor



Uncluttered Rotor (CVT)



WBG Based Motor Drives

❑ Wide band-gap (WBG) vs. Silicon

- High breakdown electric field → High breakdown voltage
- High thermal conductivity → High operation temperature
- High drift velocity → High switching-speed capability

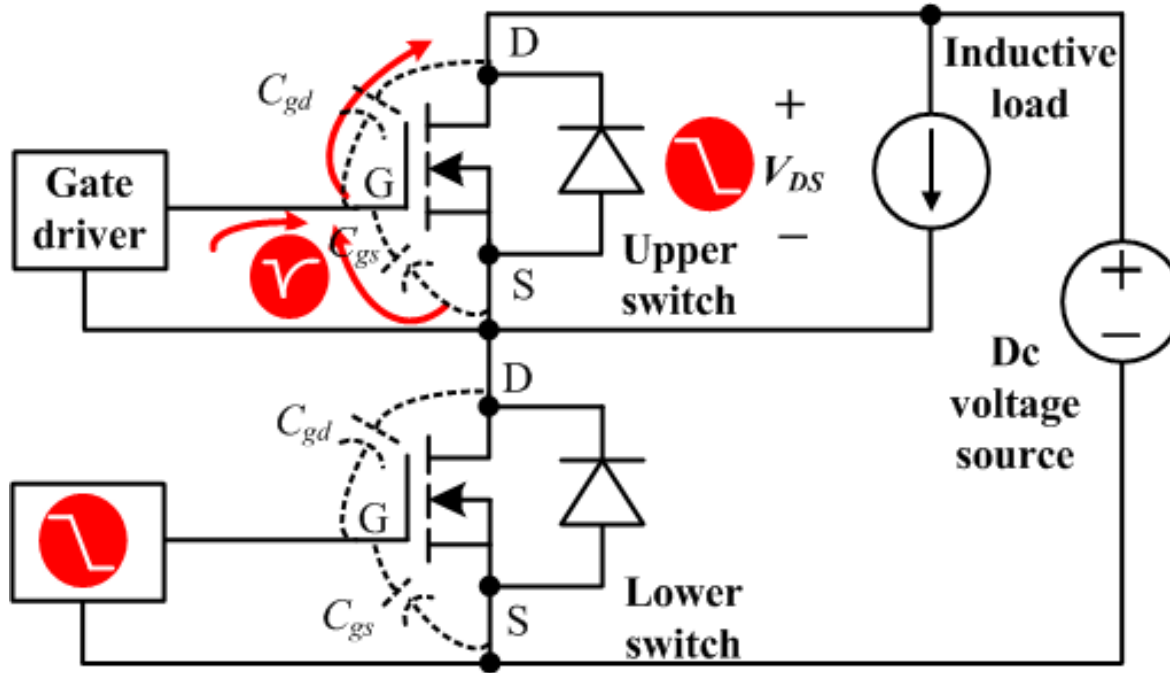
❑ Benefits of high switching-speed performance

- Low switching loss → Less cooling requirement, high power efficiency
- Short switching time → Reduced dead time, improved power quality
Increased switching frequency, high power density

❑ Can we fully utilize this potential advantage of WBG semiconductor in motor drives?

- Interference between upper & lower switches in a phase-leg (Cross talk)
- Interaction between PWM inverter and induction motor

Cross Talk in a Phase Leg



Phase-leg configuration

Turn-on
transient

Positive spurious gate voltage ↑



Shoot-through current

Cdv/dt ↑



worse

Turn-off
transient

Negative spurious gate voltage ↑



Overstress gate terminal

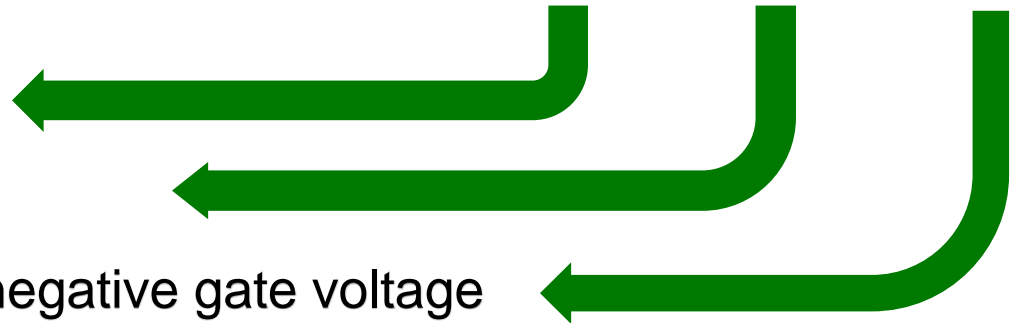
WBG (SiC) vs. Si on Cross Talk

TABLE I. Characteristics of Several Comparable Si/SiC Power Devices

Type	Manufacturer	Model	V_{DS}/I_D (100 °C)	Q_{gs}	$V_{gs(th)}$ (25 °C)	$V_{gs_max(-)}$
Si IGBT	IR	IRGP20B120U	1200 V / 20 A	169 nC	4.5 V	-20 V
Si MOSFET	Microsemi	APT34M120J	1200 V / 22 A	560 nC	4.0 V	-30 V
SiC MOSFET	CREE	CMF20120D	1200V / 24 A	90.8 nC	2.5 V	-5 V

□ Properties of SiC devices

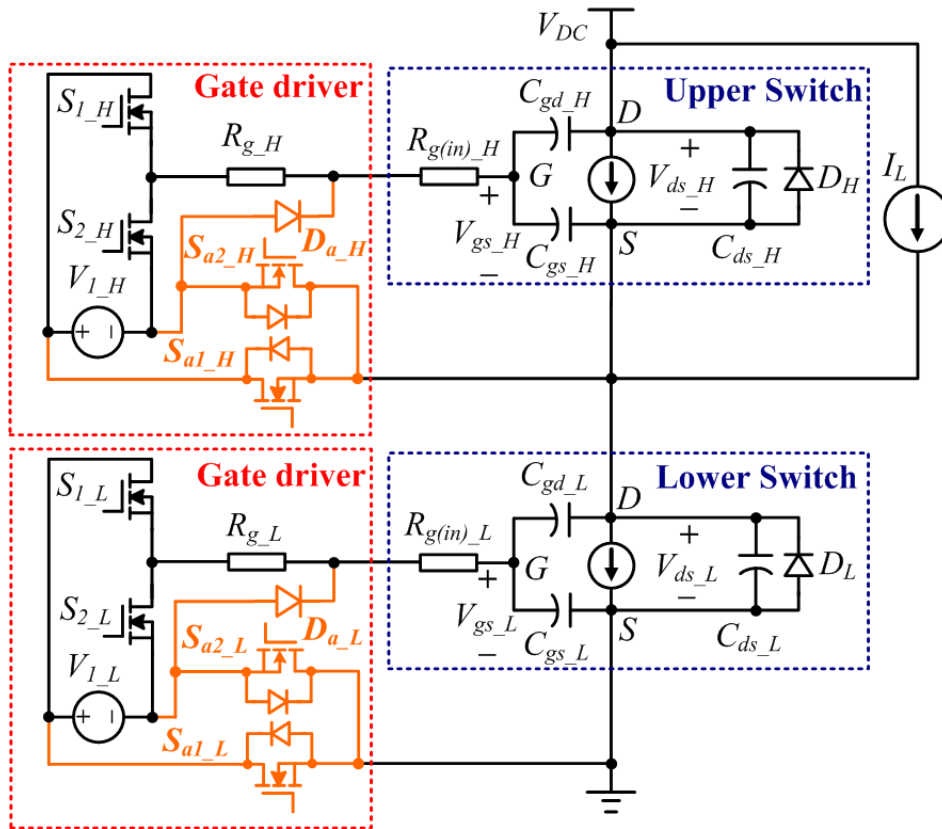
- Faster switching speed
- Lower threshold voltage
- Lower maximum allowable negative gate voltage



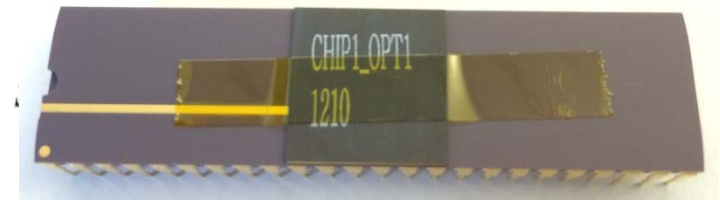
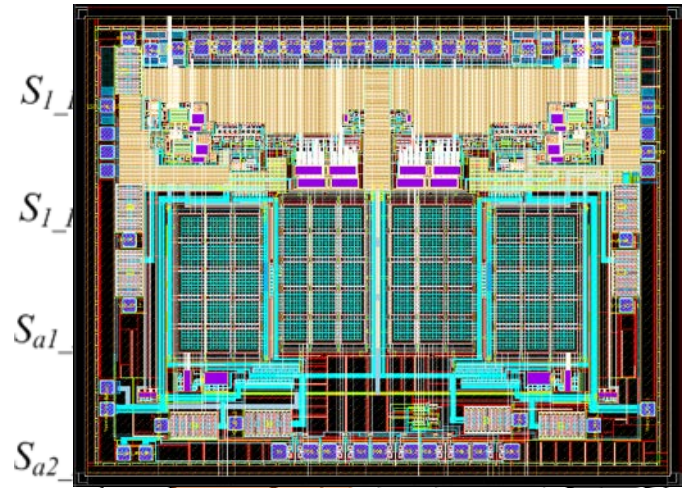
□ WBG (SiC) devices in a phase-leg are easily affected by cross talk

- Leading to extra switching losses & reliability issues
- **Have to slow down the switching speed?**

Active Gate Driver for Cross Talk Suppression



Active gate driver w/ gate assist circuit



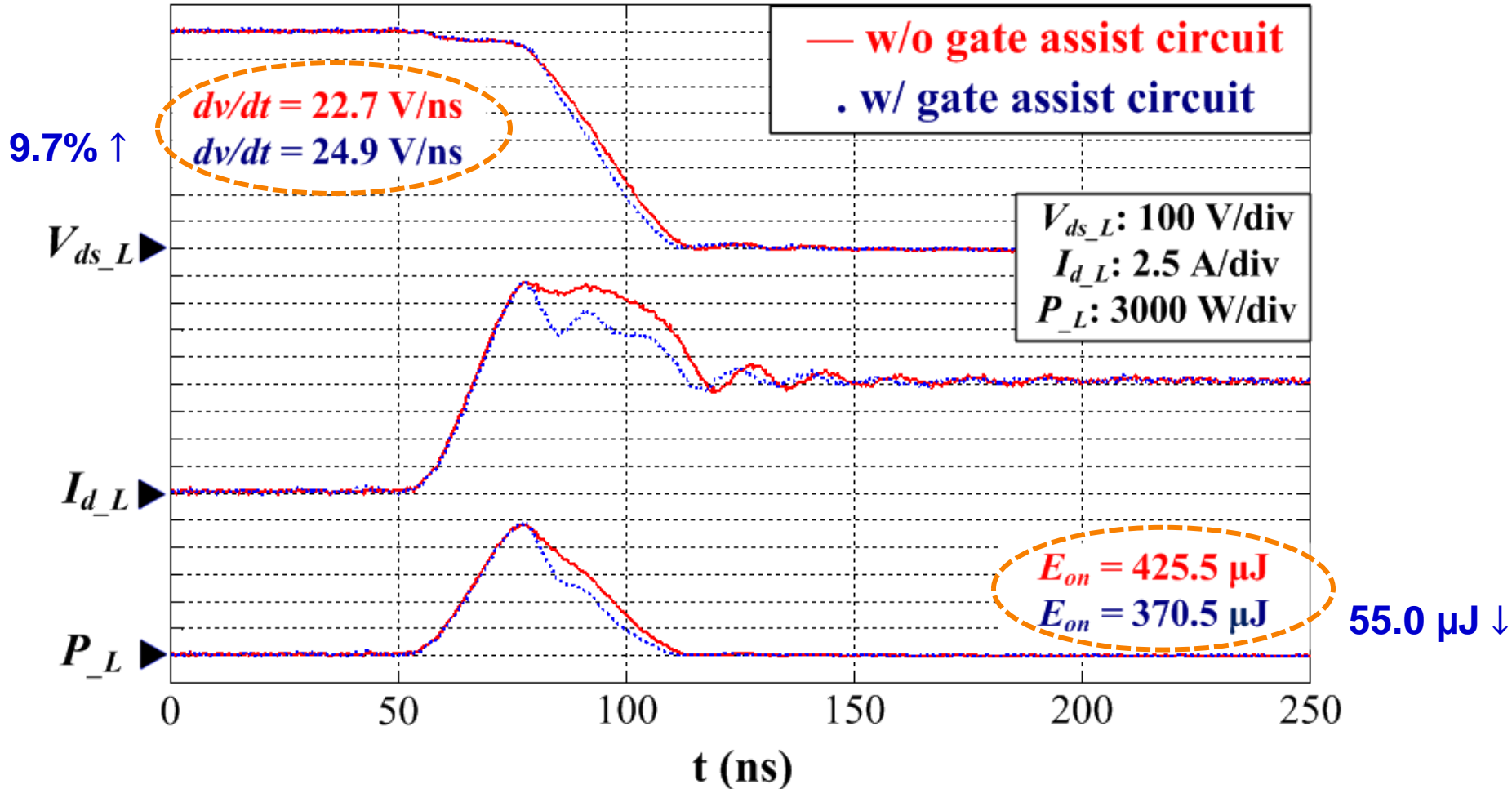
SOI HT active gate drive chip signals with anti-cross talk circuitry
Logic signals

Compared with conventional gate driver, gate assist circuit adds

- Two auxiliary transistors (S_{a1_H} , S_{a2_H} or S_{a1_L} , S_{a2_L}) along with one diode (D_{a_H} or D_{a_L}) for each device in a phase-leg.

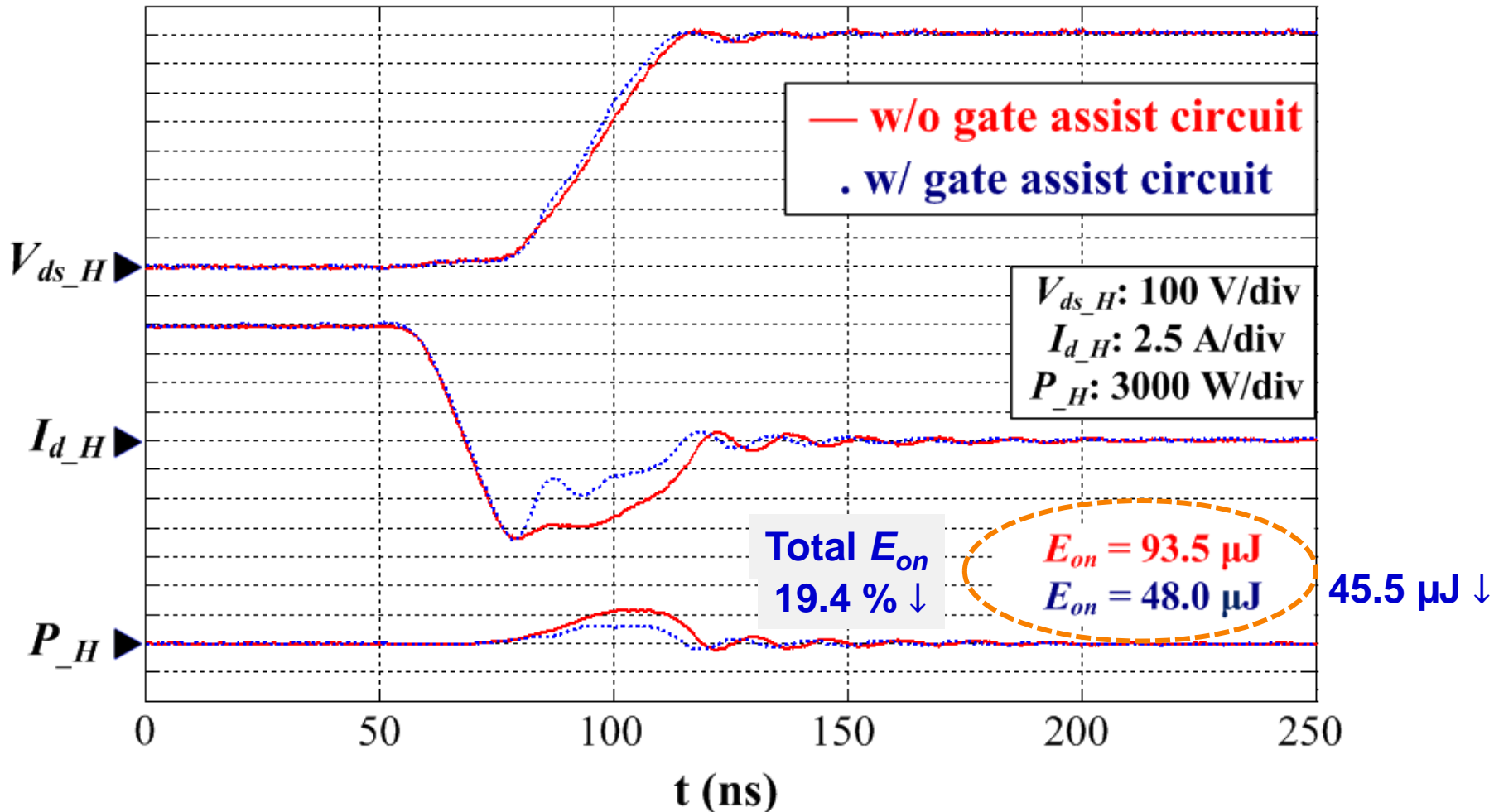
Turn-on Transient of the Lower Switch

$V_{DC} = 800\text{ V}$, $I_L = 10\text{ A}$ (Turn-on transient of the lower switch)



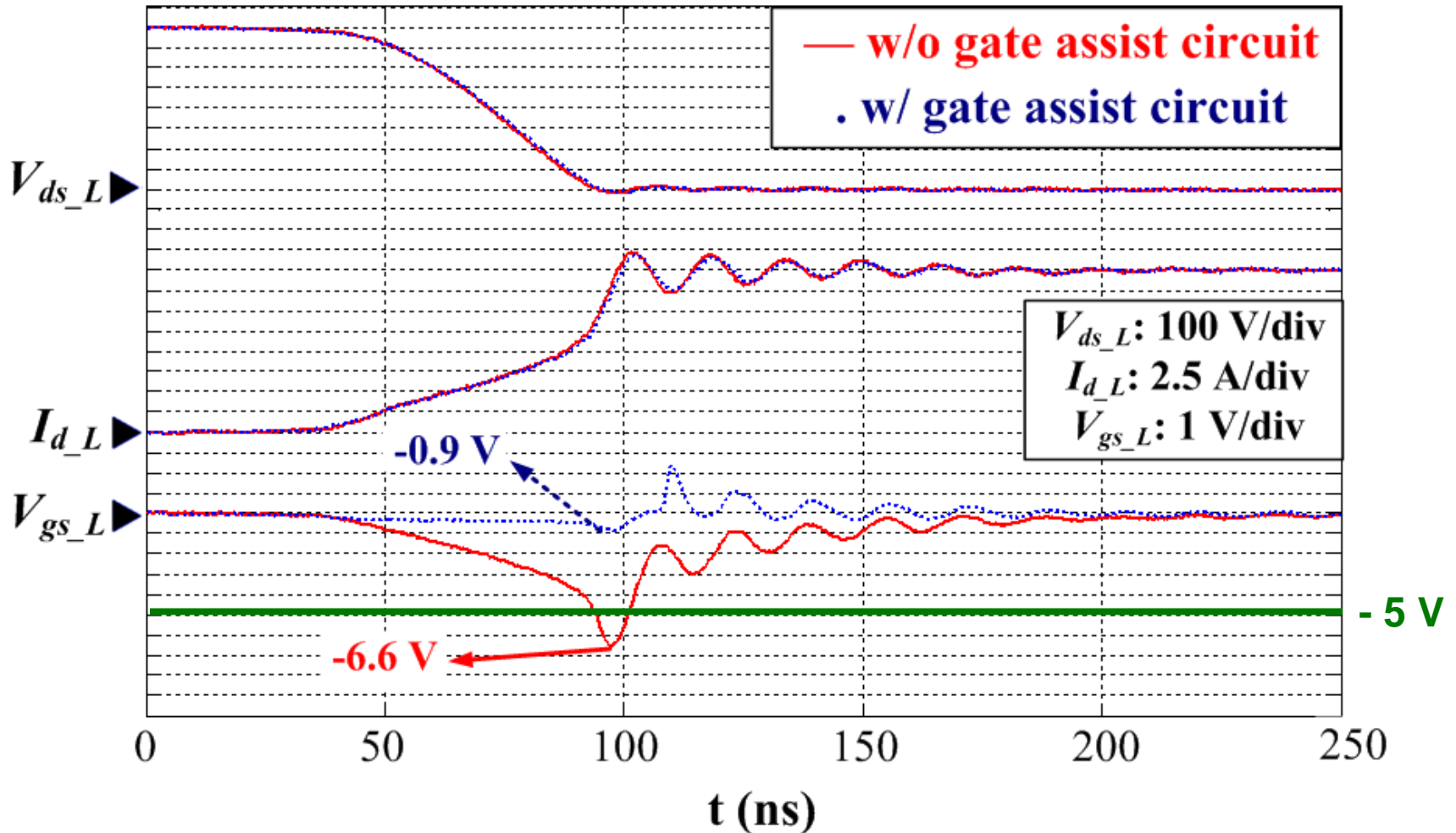
Turn-on Transient of the Lower Switch

$V_{DC} = 800$ V, $I_L = 10$ A (Turn-on transient of the lower switch)



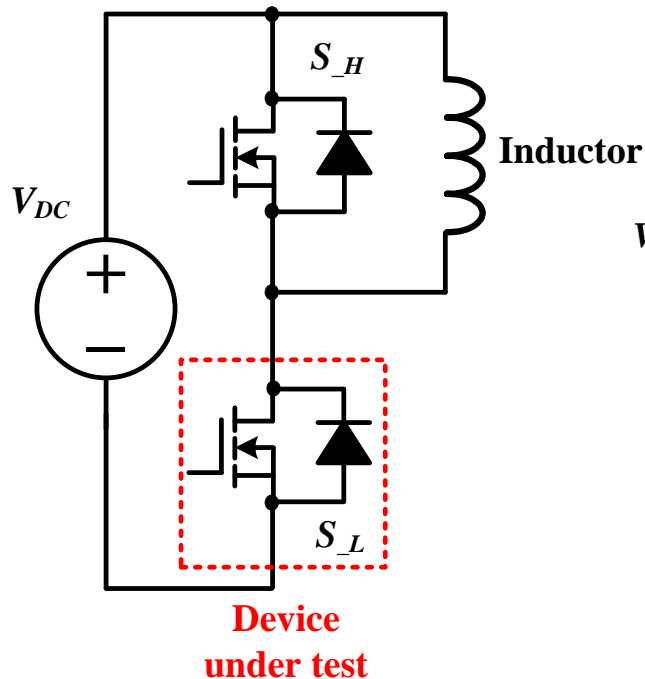
Turn-off Transient of the Upper Switch

$V_{DC} = 800 \text{ V}$, $I_L = 10 \text{ A}$ (Turn-off transient of the upper switch)

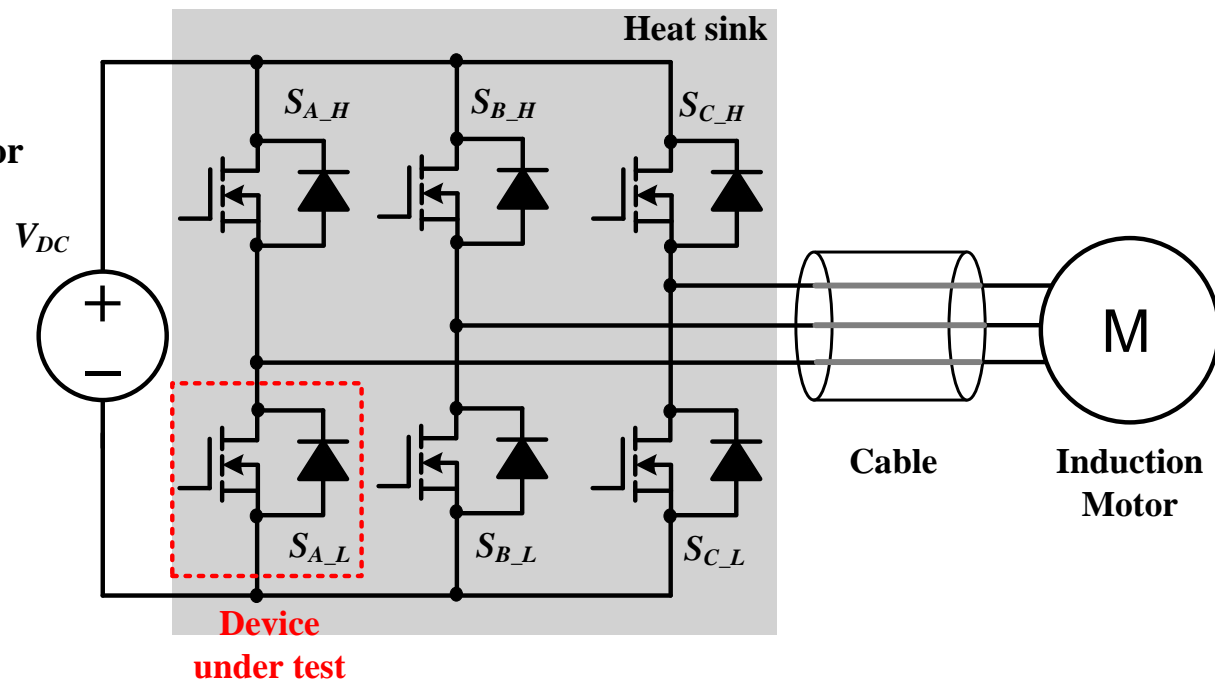


Non-motor Inductive Load vs. Induction Motor

- ❑ Switching behavior plays a significant role on motor drives design
 - Thermal management, dead time, switching frequency
- ❑ Double pulse tester (DPT) with optimally-designed inductor load is a well-accepted method for switching performance evaluation
- ❑ Actual switching performances in motor drives are different



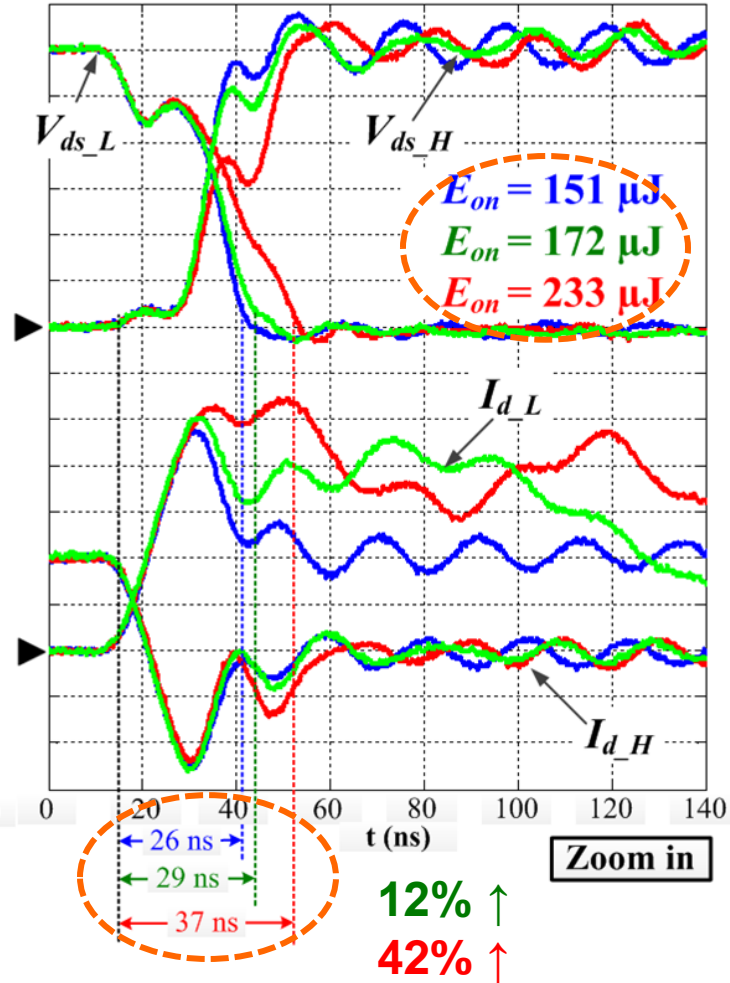
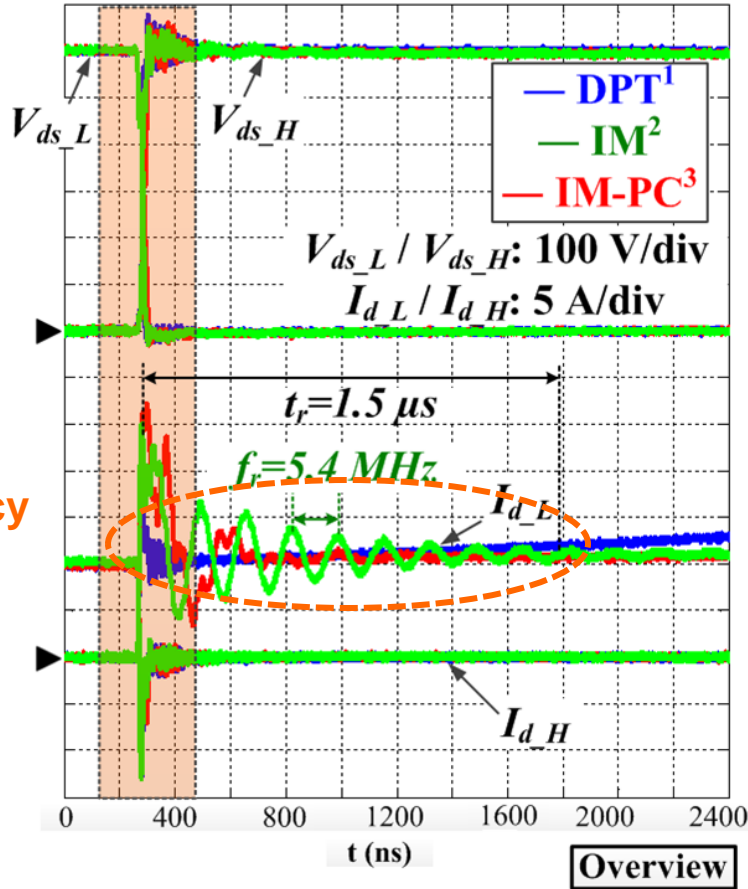
Double pulse tester circuits



Three-phase PWM inverter fed motor drives

Switching Waveforms Comparison (Turn-on)

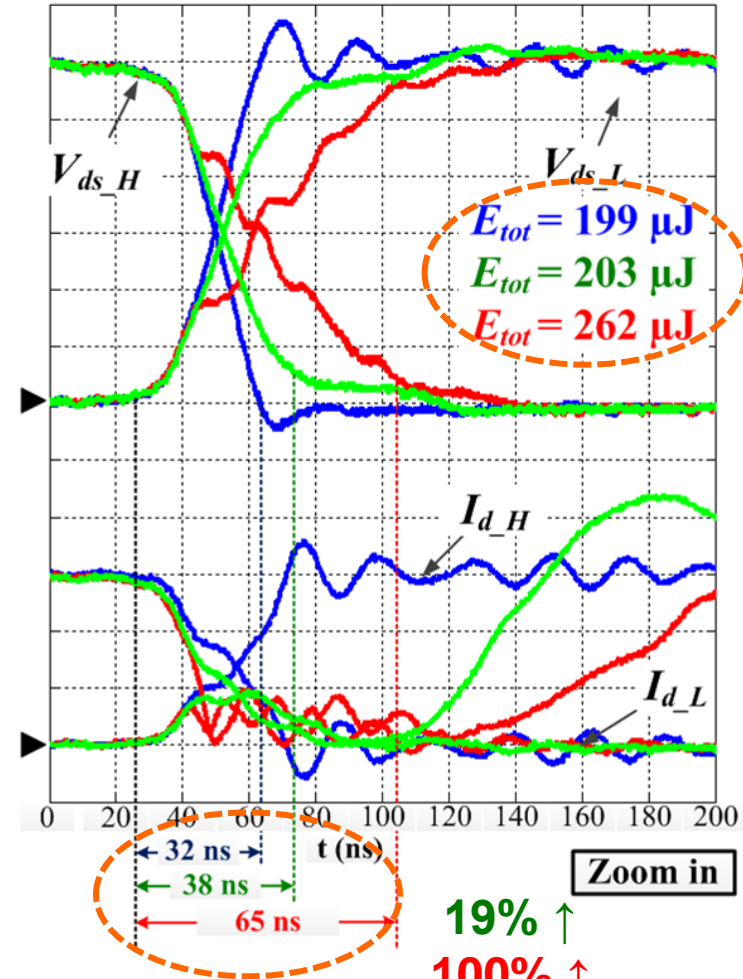
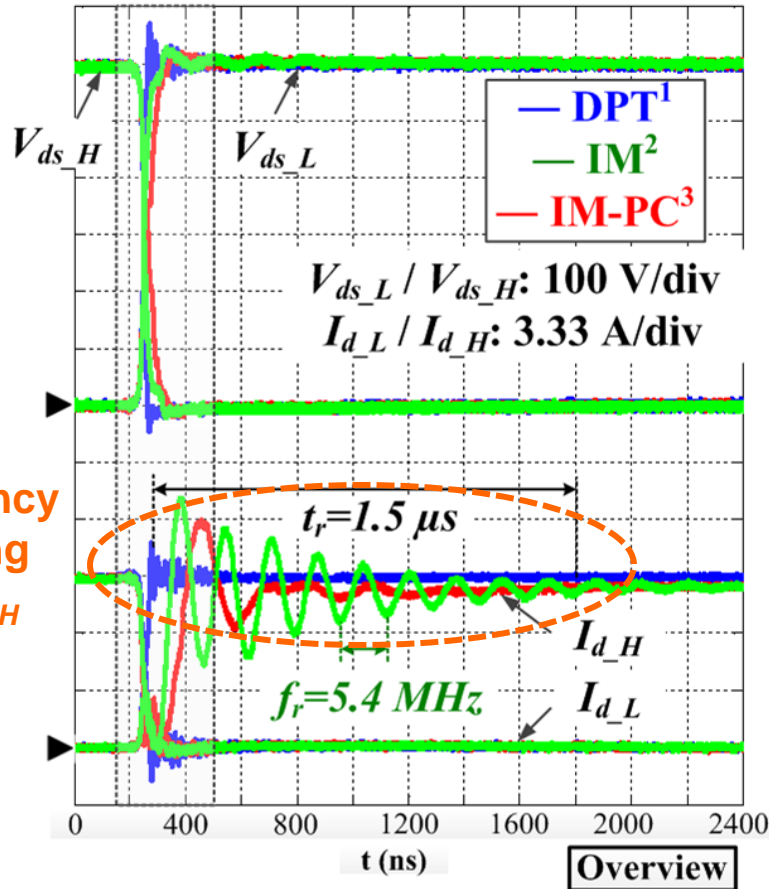
$V_{DC} = 600 \text{ V}$, $I_L = 10 \text{ A}$, $R_g = 5 \Omega$ (turn-on transient of the lower switch)



1. DPT: double pulse tester with inductor load
2. IM: pulse tester with 10 HP induction motor (IM)
3. IM-PC: pulse tester with 10 HP induction motor (IM) plus 6.6 feet power cable (PC)

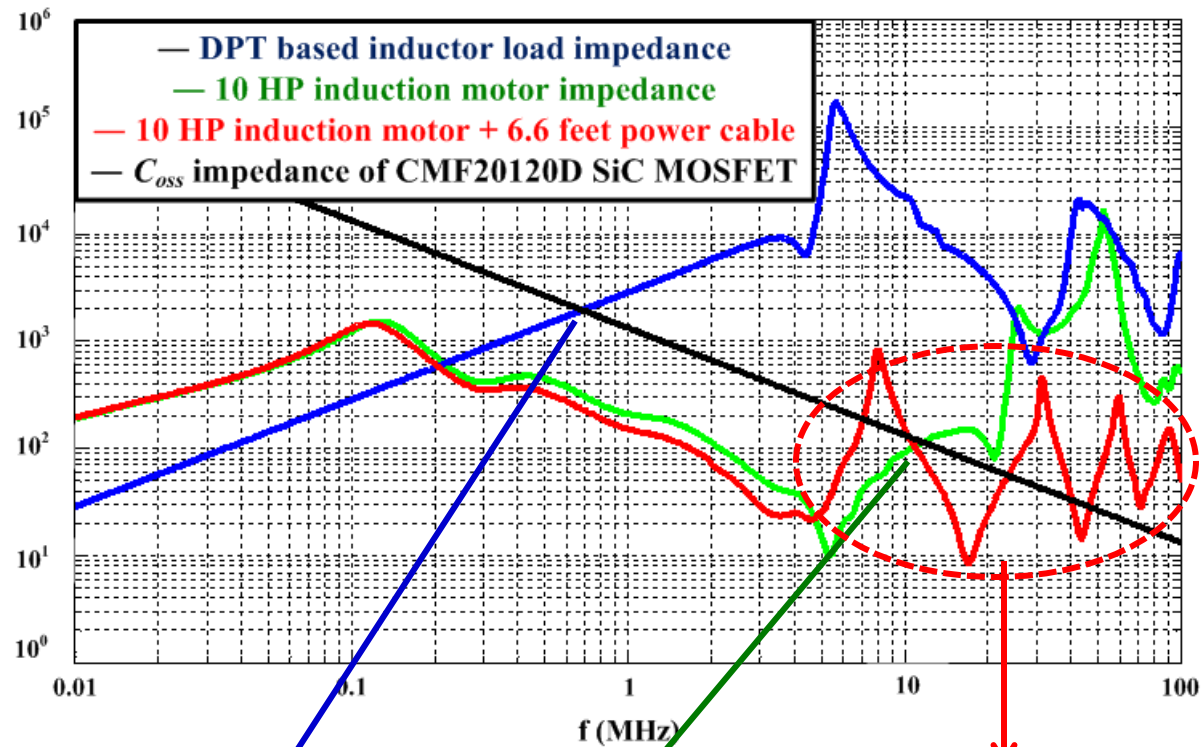
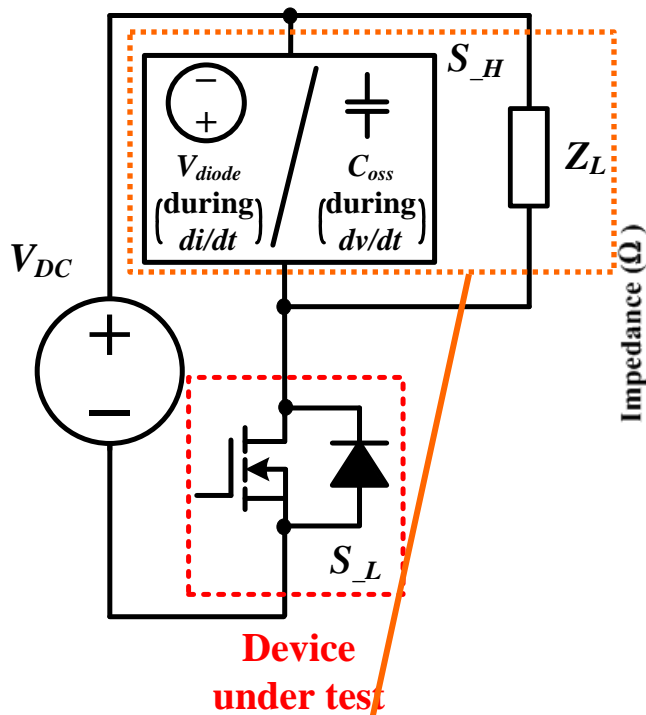
Switching Waveforms Comparison (Turn-off)

$V_{DC} = 600 \text{ V}$, $I_L = 10 \text{ A}$, $R_g = 5 \text{ } \Omega$ (turn-off transient of the lower switch)



1. DPT: double pulse tester with inductor load
2. IM: pulse tester with 10 HP induction motor (IM)
3. IM-PC: pulse tester with 10 HP induction motor (IM) plus 6.6 feet power cable (PC)

High-frequency Impedance Comparison



Z_L paralleled with C_{oss} during dv/dt

- Ideally, $|Z_L| \gg |C_{oss}|$ @ HF
 Z_L has little impact on switching
- Practically, Z_L will affect switching if $|Z_L|$ is comparable to $|C_{oss}|$ @ HF

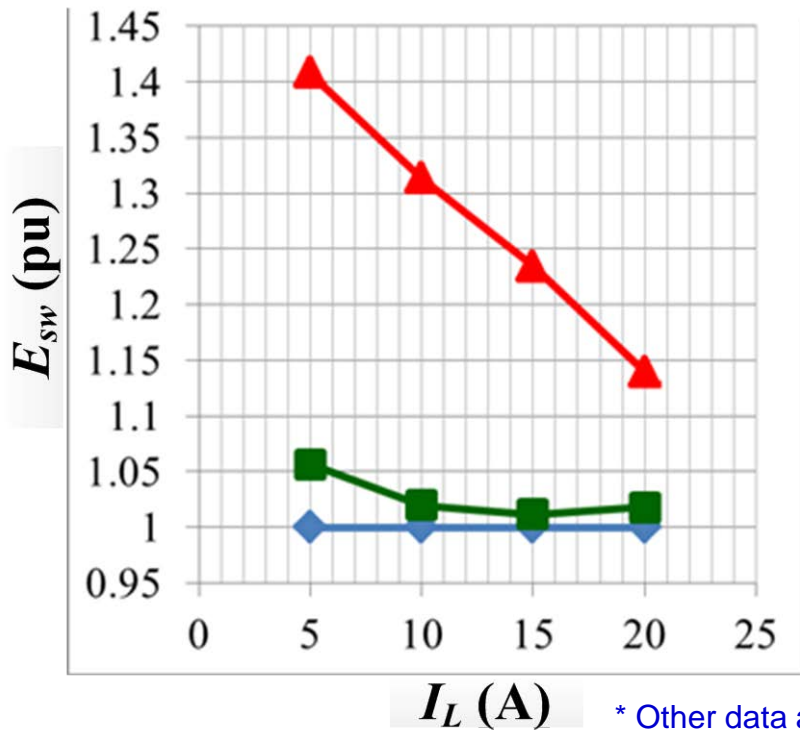
For DPT based inductor load
 $|Z_L| > |C_{oss}|$
@ 700 kHz

For 10 HP induction motor
 $|Z_L| > |C_{oss}|$
@ 10 MHz

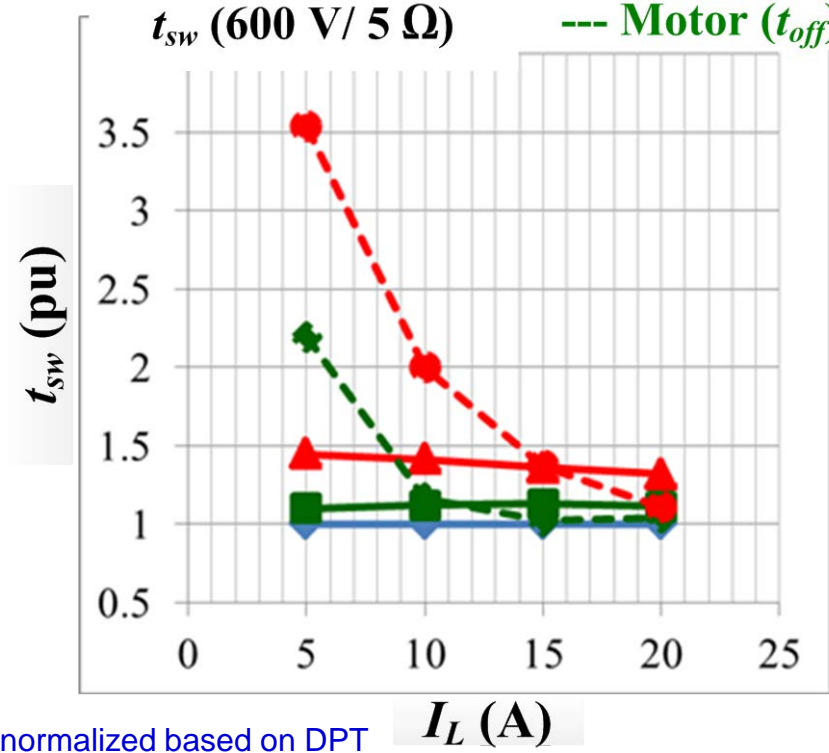
For induction motor + cable,
 $|Z_L|$ is comparable to $|C_{oss}|$ until 50 MHz

Impact of Motor on Motor Drives Design

— Motor + Cable (E_{sw}) — DPT (E_{sw})^{*}
— Motor (E_{sw})

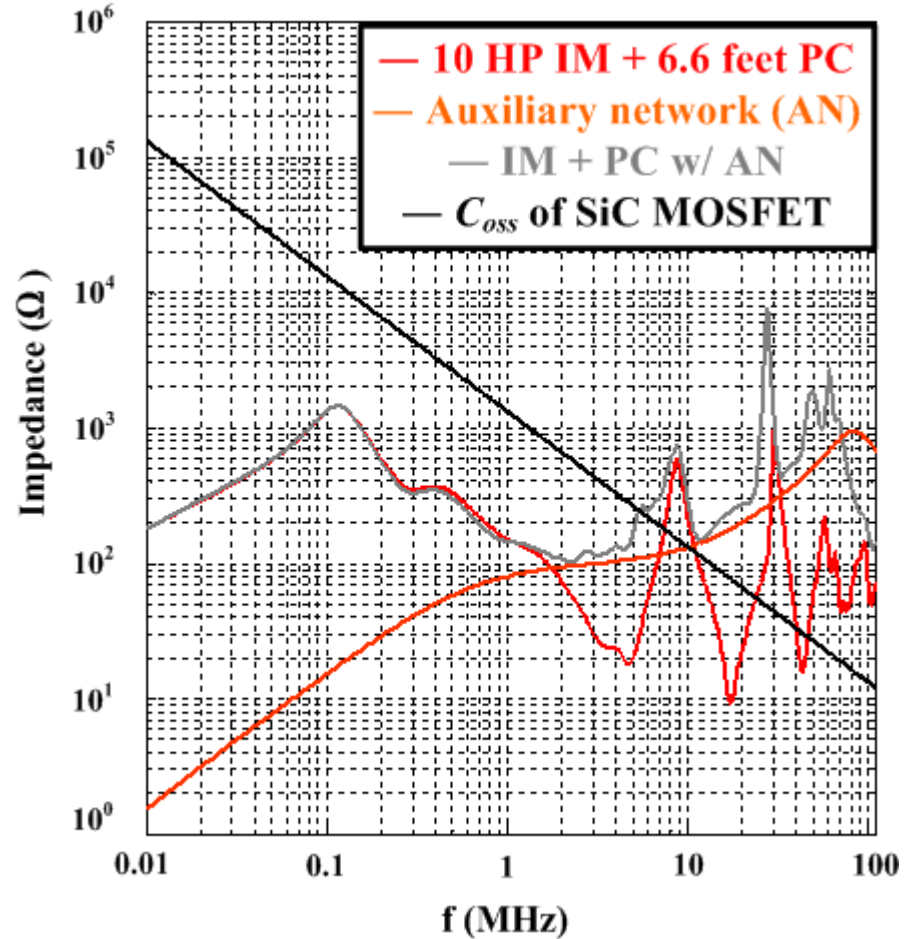
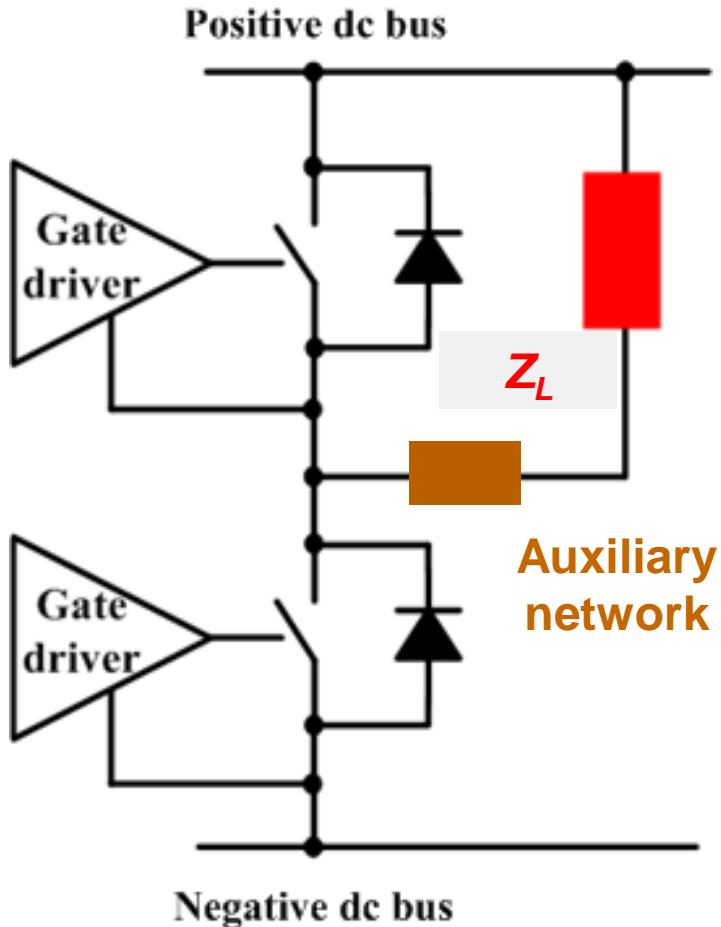


— Motor + cable (t_{on}) — DPT (t_{on} or t_{off})^{*}
- - - Motor + cable (t_{off}) — Motor (t_{on})
- - - Motor (t_{off})



- Cooling system cannot be designed based on switching loss from typical DPT
- Switching frequency and dead time cannot be set based on switching time from DPT

Auxiliary Network to Improve HF Impedance



□ Insert an auxiliary network to increase high frequency impedance of induction motor

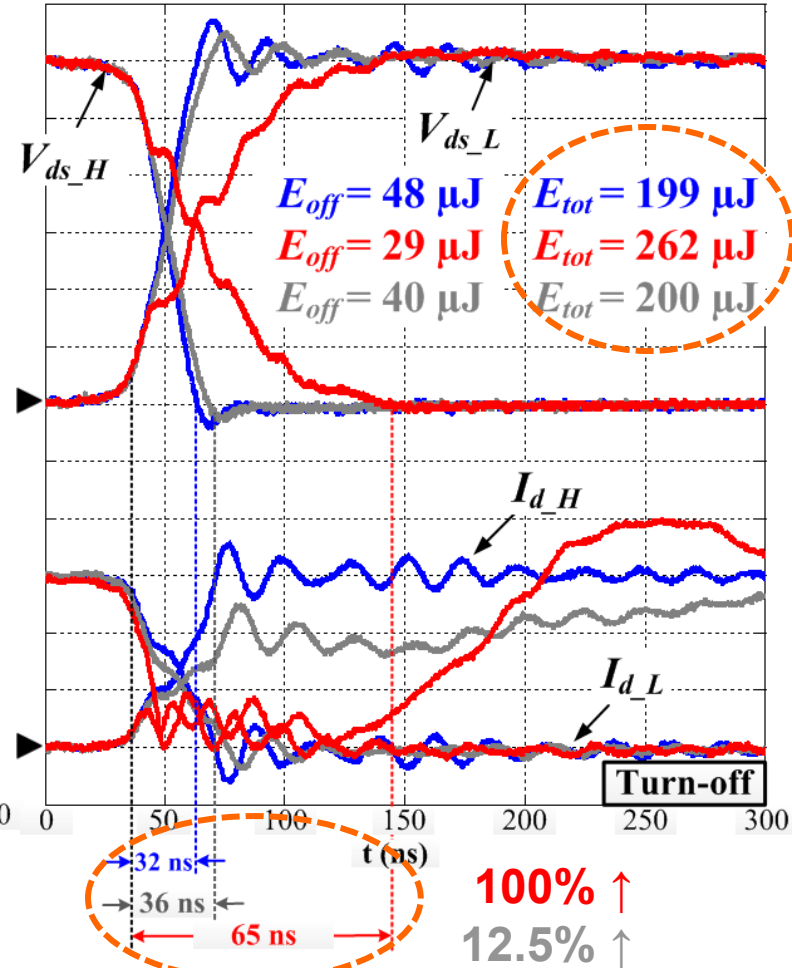
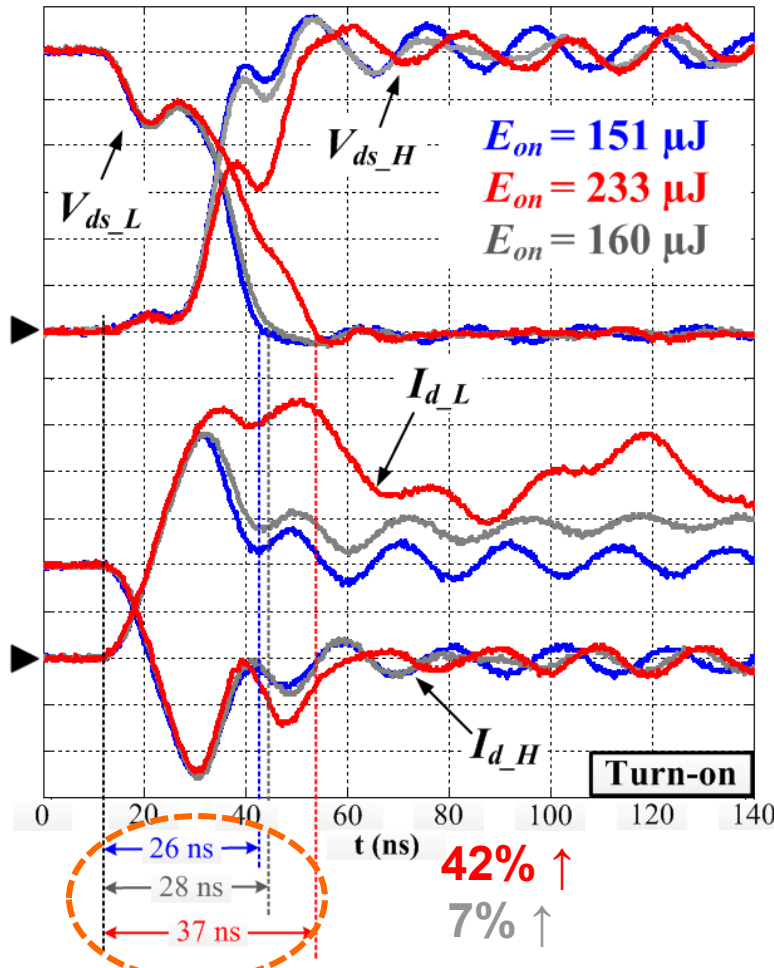
Switching Waveforms Comparisons

V_{ds_L} / V_{ds_H} : 100 V/div
 I_{d_L} / I_{d_H} : 5.0 A/div

$V_{DC} = 600\text{ V}, I_L = 10\text{ A}, R_g = 5\ \Omega$

— DPT¹ — IM-PC² — IM-PC-AN³

V_{ds_L} / V_{ds_H} : 100 V/div
 I_{d_L} / I_{d_H} : 3.33 A/div



1. DPT: double pulse tester with inductor load
2. IM-PC: pulse tester with induction motor + power cable
3. IM-PC-AN: pulse tester with IM + PC + auxiliary network



Summary

- ❑ **High switching-speed performance of WBG in motor drives**
 - **Interference between upper & lower switches (cross talk)**
 - Short-through current causes turn-on energy loss increase, tested up to 19% and dv/dt reduction by 10%
 - Spurious negative gate voltage beyond required range
 - **Interaction between PWM inverter & induction motor**
 - Switching energy loss increased by 32%
 - Switching time increased by 42% during turn-on and doubled during turn-off
- ❑ **Better utilization of WBG devices in PWM motor drives**
 - **Active gate driver circuitry for cross talk suppression**
 - **Consider motor load characteristics in the design and operation of PWM inverter**
 - **Integrated design/operation methodology**

Acknowledgements



This work made use of shared facility supported by the ERC Program of the National Science Foundation and DOE under NSF Award Number EEC-1041877 and the CURENT Industry Partnership Program.