



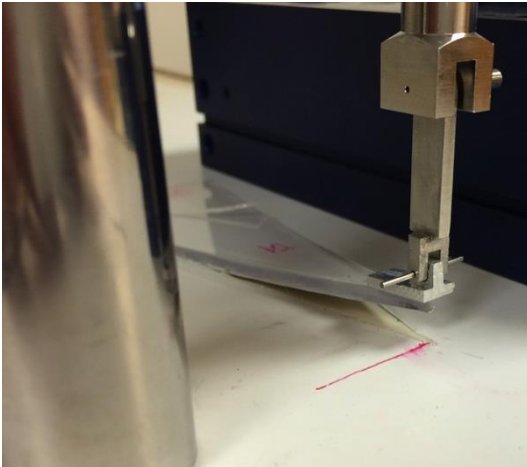
# Quantifying Adhesion in PV modules: A Historical Survey and Degradation Processes

Nick Bosco  
*NREL*

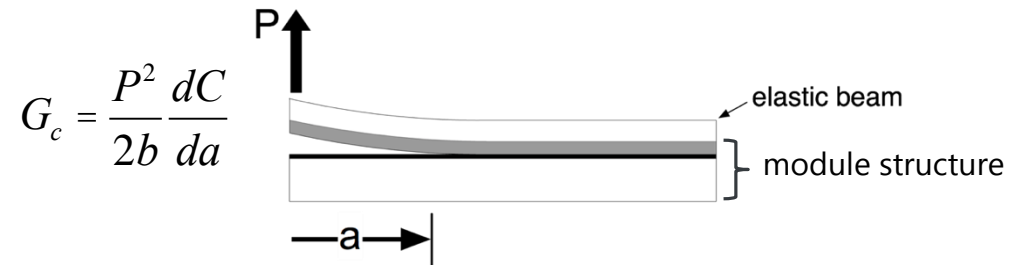
# Quantifying Adhesion

## width-tapered cantilever beam method

backsheet



- Only the strain energy temporarily stored in the beam is available to drive delamination
- Measurements of beam compliance allow us to quantify this energy very accurately

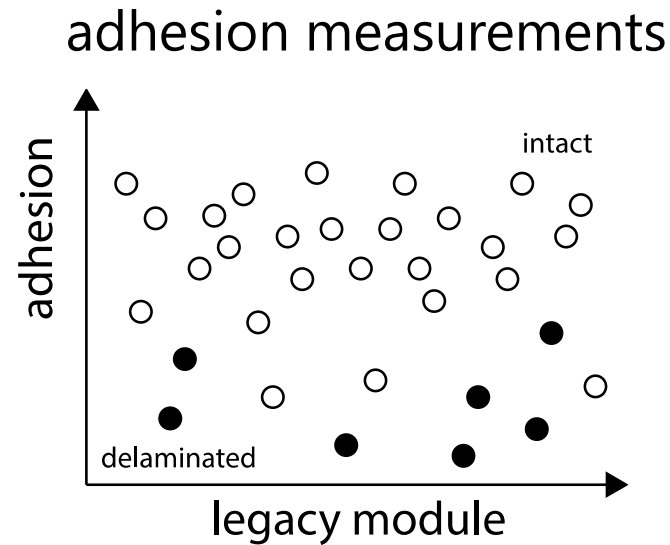


front encapsulant



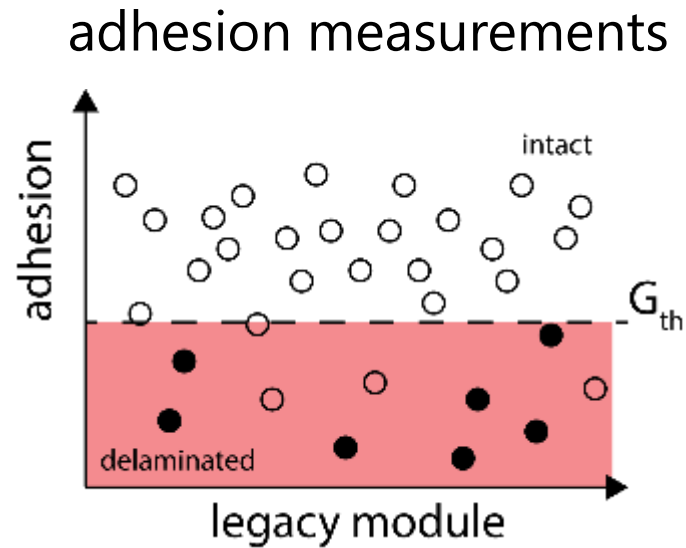
- The measurement is identical at the coupon and module level
- Every interface within the PV module laminate may be measured
- The result is the quantification of a material property

# Threshold Adhesion Values



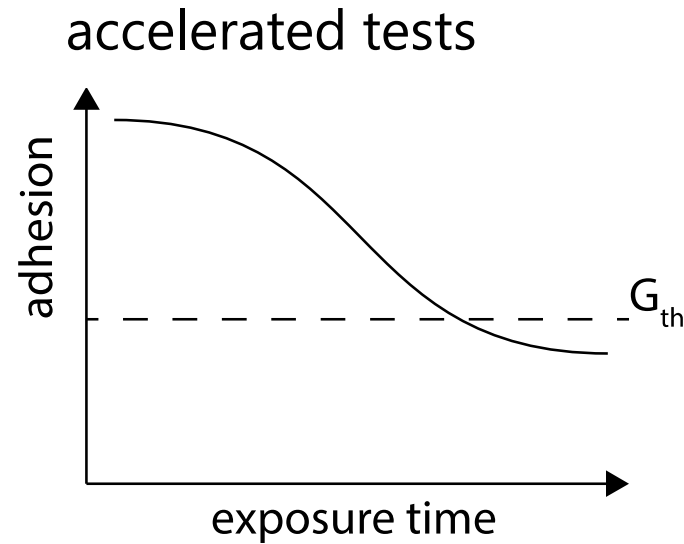
- an adhesion value above which a module should remain intact throughout its lifetime

# Threshold Adhesion Values



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# Threshold Adhesion Values



- an adhesion value above which a module should remain intact throughout its lifetime

# Module Population

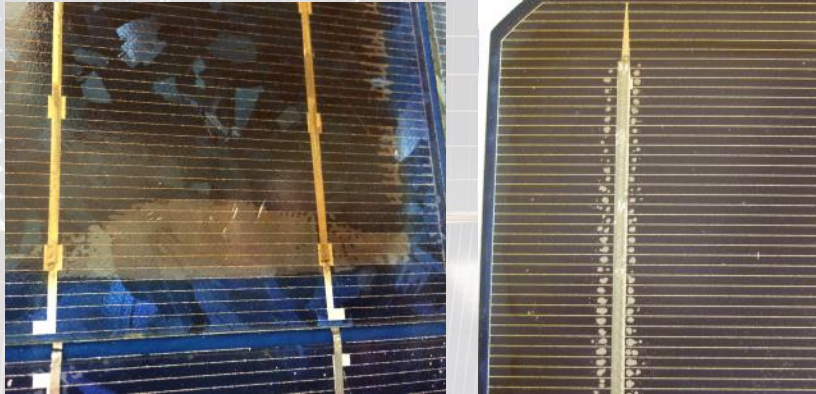
- 32 crystalline silicon modules
- 11 manufactures
- Deployed or stored from two – 27 years
- 16 locations world wide
- Include pre-existing delamination

N. Bosco, J. Eafanti, S. Kurtz, J. Tracy and R. Dauskardt, "Defining Threshold Values of Encapsulant and Backsheet Adhesion for PV Module Reliability," in *IEEE Journal of Photovoltaics*, vol. 7, no. 6, pp. 1536-1540, Nov. 2017.



# Module Population

## examples of pre-existing front encapsulant delamination



- measurements primarily made away from debonded area
- likely results in a more conservative estimate of  $G_{th}$

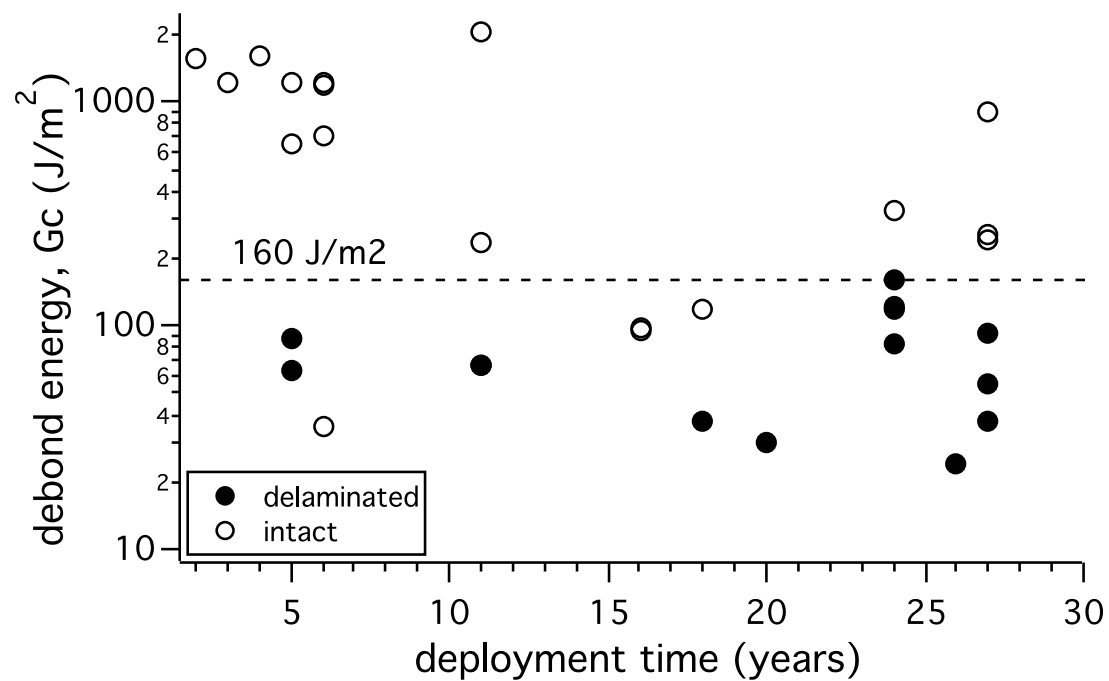
## examples of pre-existing backsheet delamination



Photo: John Wohlgemuth

- measurements made at delamination front
- results in a more accurate estimate of  $G_{th}$

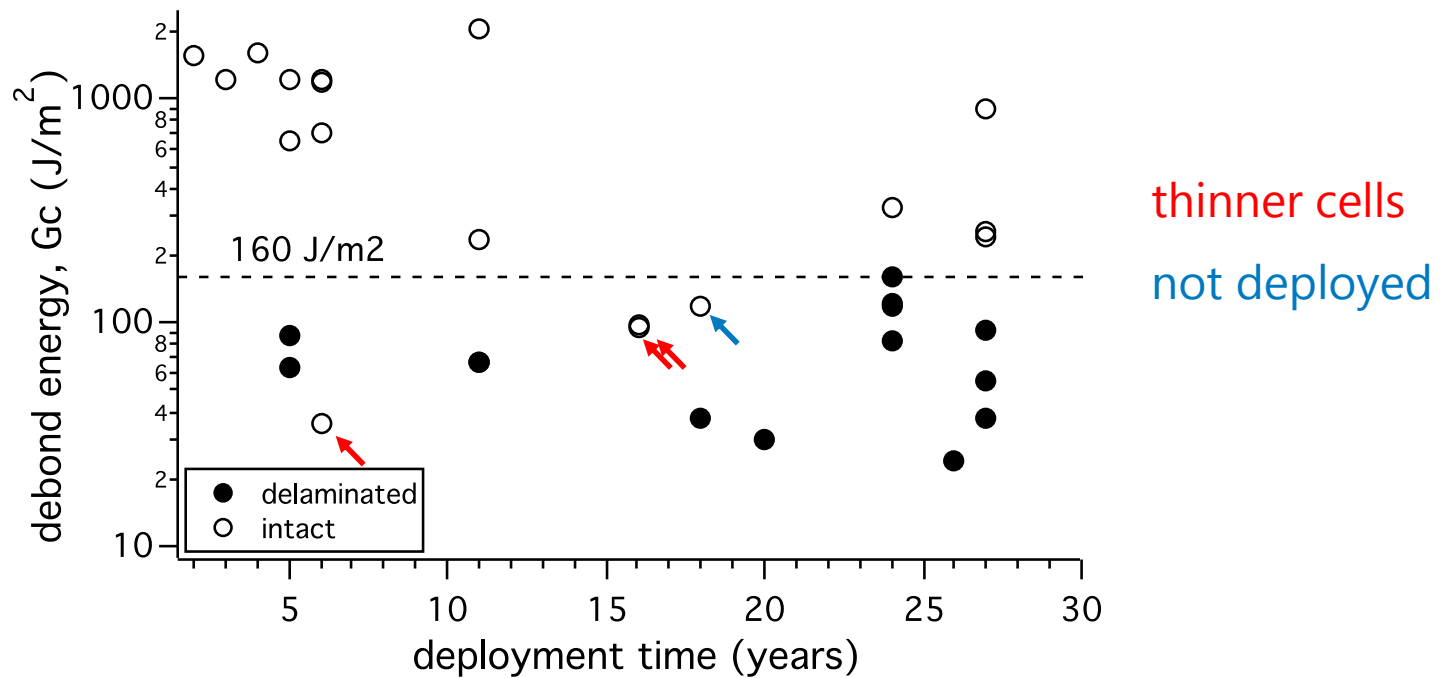
## Encapsulant Adhesion Survey



- Front encapsulant adhesion threshold is ~ **160  $J/m^2$**

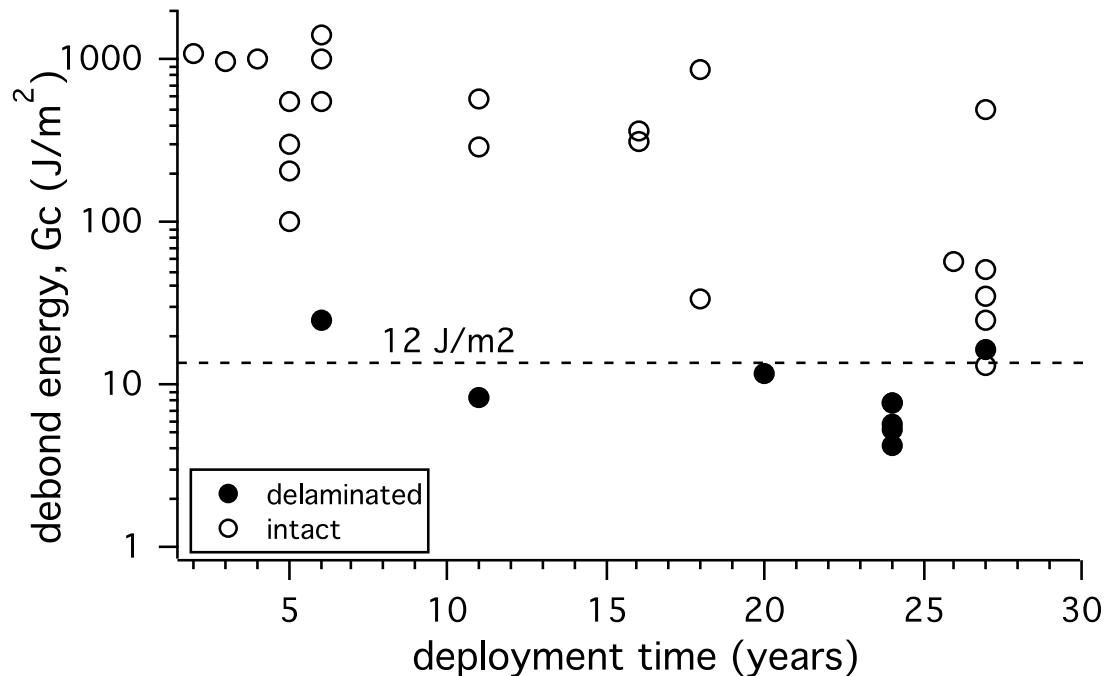


## Encapsulant Adhesion Survey



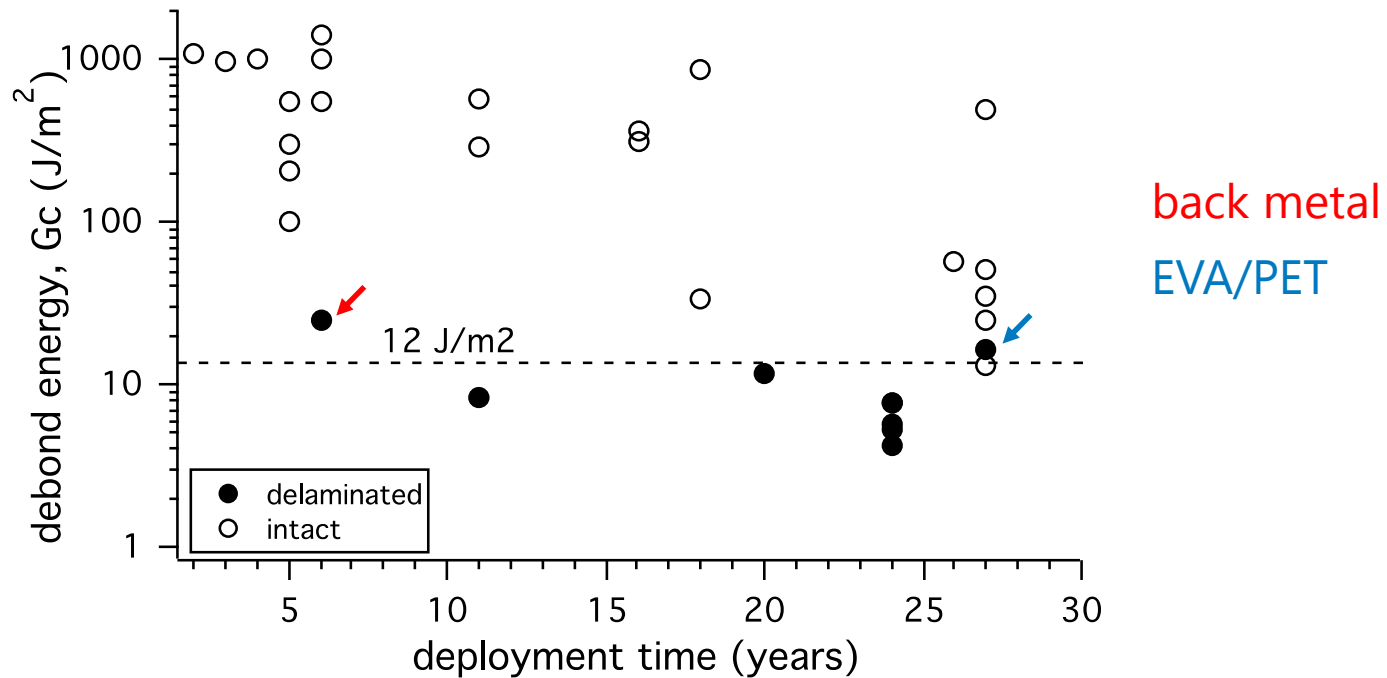
- Front encapsulant adhesion threshold is ~ **160  $\text{J/m}^2$**
- Newer modules with thinner cells can accommodate lower debond energies without delaminating

## Backsheet Adhesion Survey



- backsheet adhesion threshold is ~ **12 J/m<sup>2</sup>**
- Most delamination occurred at the outer PET/ PVF interface
- Only a lower limit (>300 J/m<sup>2</sup>) of adhesion was measurable on some modules

## Backsheet Adhesion Survey



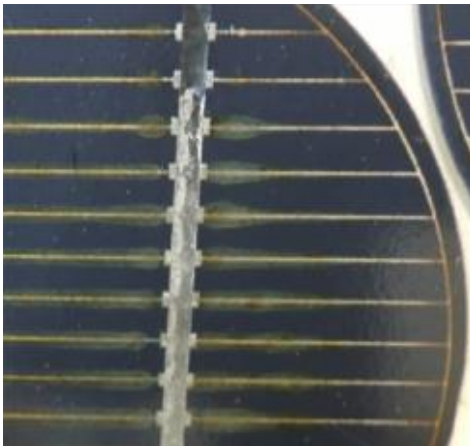
- backsheet adhesion threshold is ~ **12  $J/m^2$**
- Most delamination occurred at the outer PET/ PVF interface
- Only a lower limit ( $>300 J/m^2$ ) of adhesion was measurable on some modules

# Conclusions

- Front encapsulant adhesion threshold is:  $\sim \mathbf{160 \text{ J/m}^2}$
- Backsheet adhesion threshold is:  $\sim \mathbf{12 \text{ J/m}^2}$
- These values should evolve as the sample population increases
- A safety factor should be assigned when developing and evaluating materials
- Some aspects of module design will influence  $G_{th}$

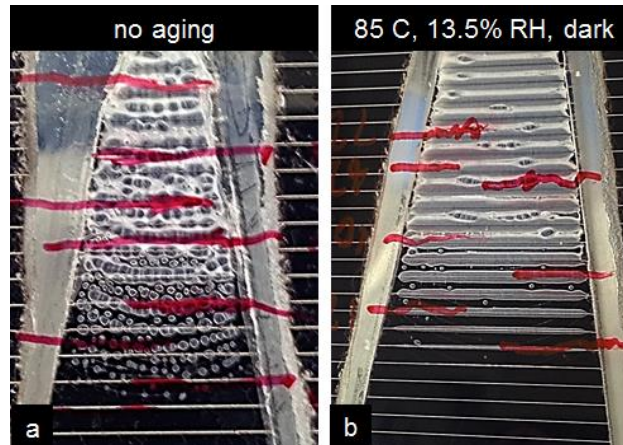
# motivating observations

## field observation



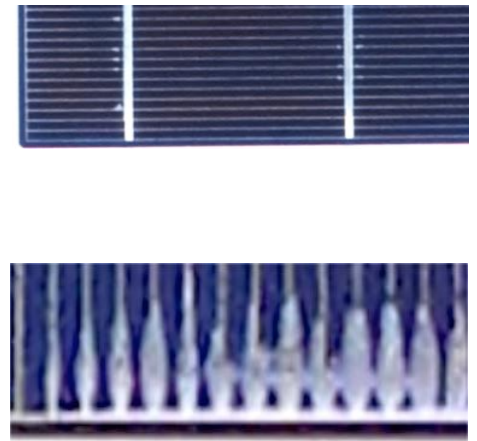
Arco Solar

## adhesion measurement



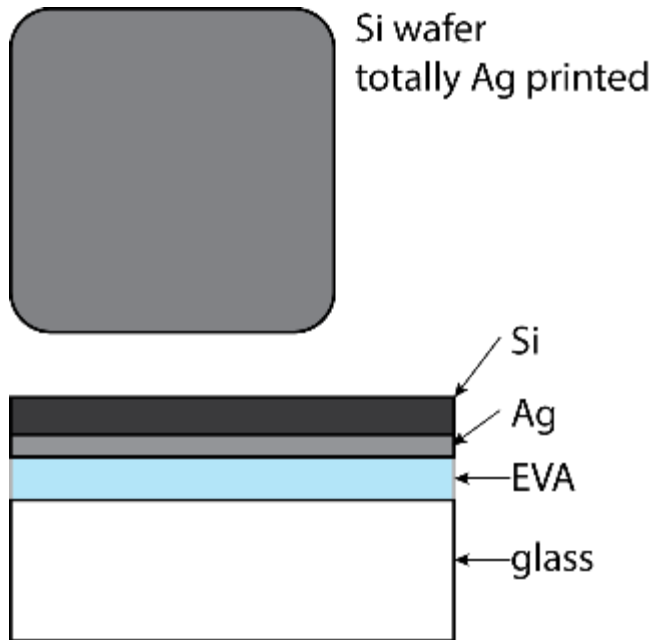
85°C, 13.5% RH

## accelerated stress



85°C, 85% RH: 1000 h  
followed by  
72°C, 95%, -1000 V :156h

# experimental design

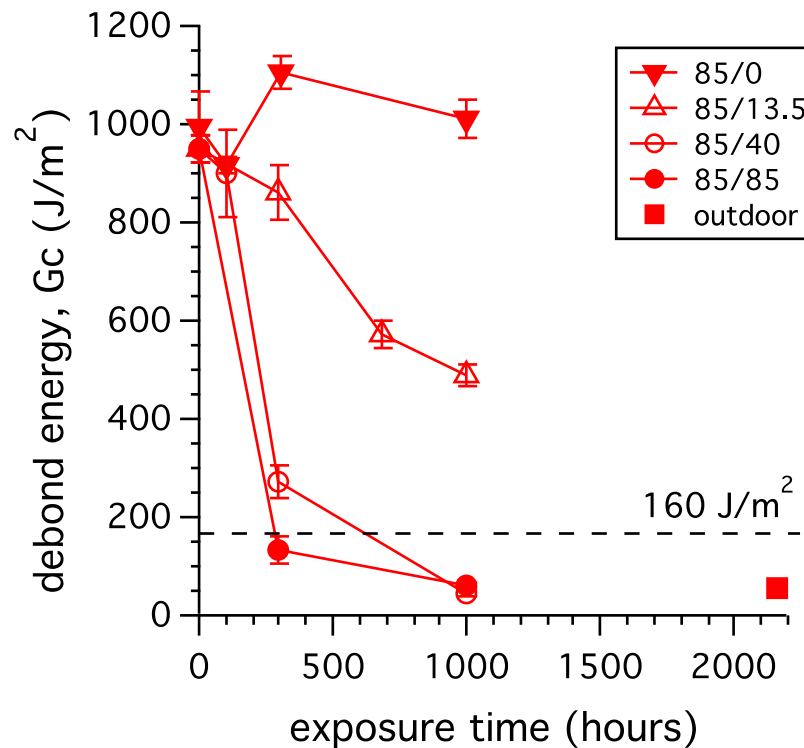


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Photovoltaics Center of Excellence (UCEP)  
Georgia Tech University, USA

sample	temp $^{\circ}$ C	RH%	bias $^{\circ}$ V
Ag/EVA1	85	0	0
Ag/EVA2	85	13.5	0
Ag/EVA3	85	40	0
Ag/EVA4	85	85	0
Ag/EVA5	on-sun		
Ag/EVA6	85	85	0
	85	85	-1000
Ag/EVA7	85	85	-1000
Ag/EVA8	85	0	-1000
Cell/EVA1	85	85	0
Cell/EVA2	85	0	0
	85	0	-1000
Cell/EVA3	85	85	0
	85	85	-1000
Cell/EVA4	85	0	0
	85	0	-2000
Cell/EVA5	85	85	0
	85	85	-2000

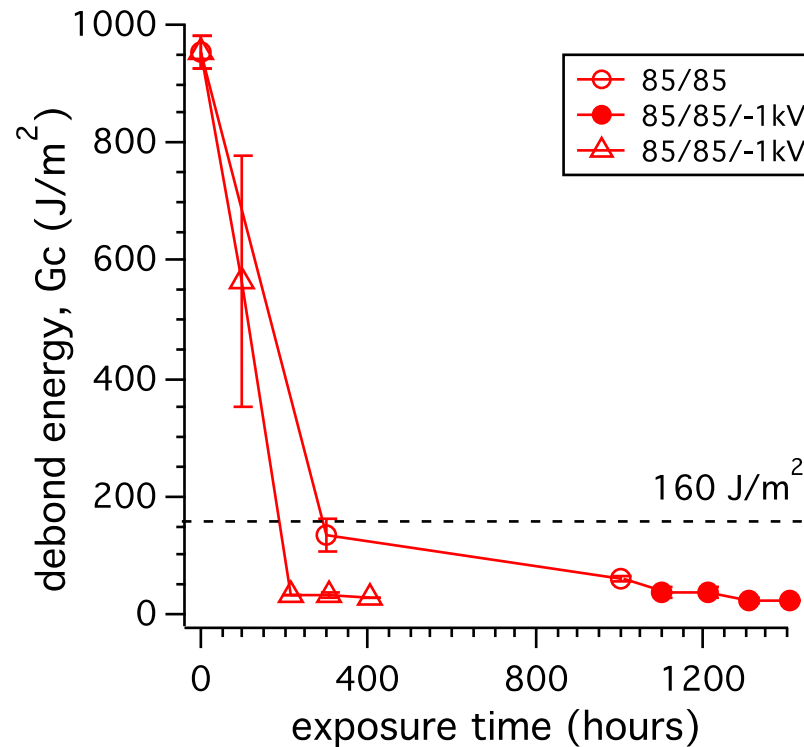


## Ag/ EVA humidity series



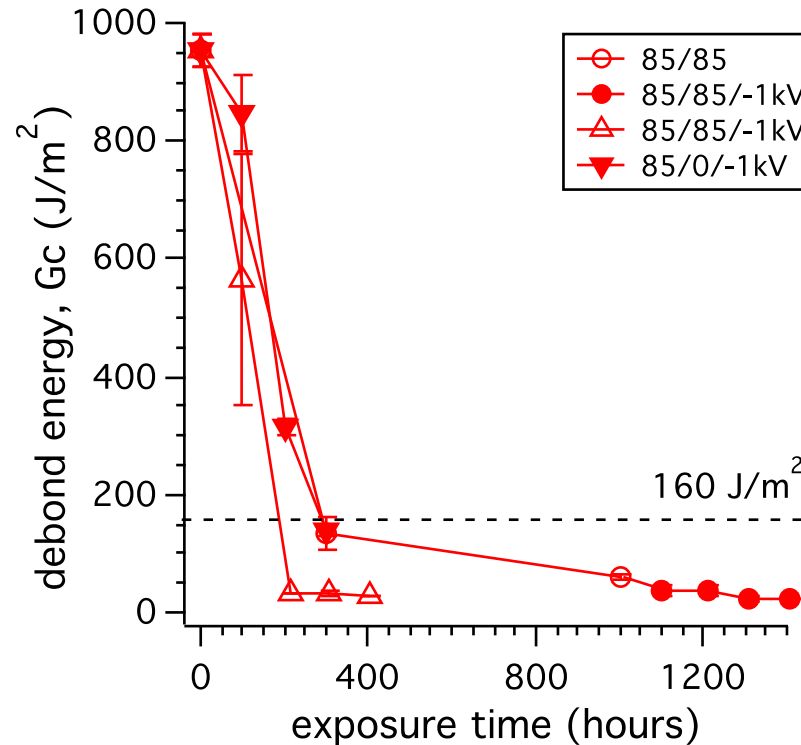
- adhesion rapidly degrades in the presence of humidity
- accelerated conditions are representative of a short on-sun exposure

## Ag/ EVA bias series



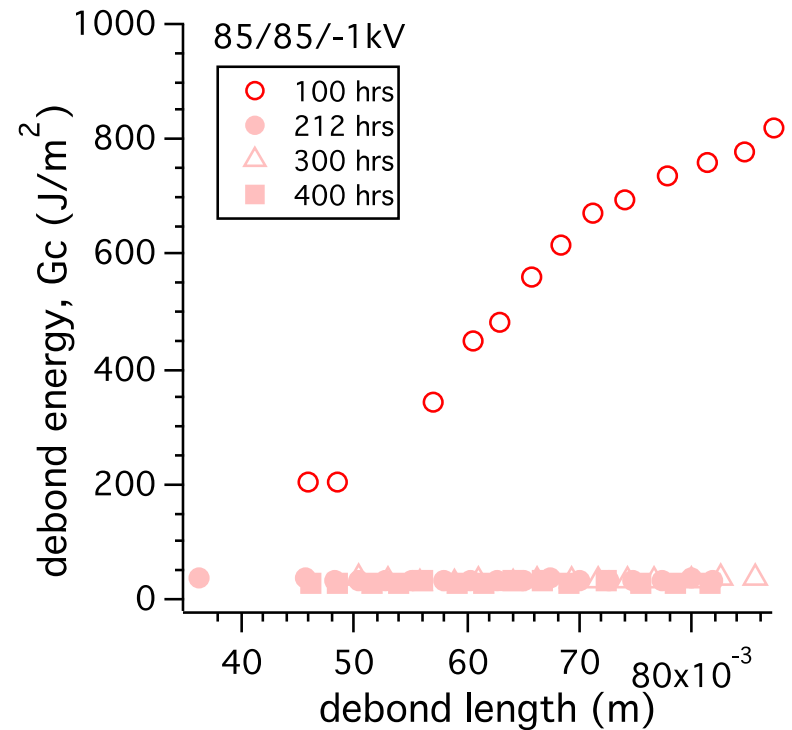
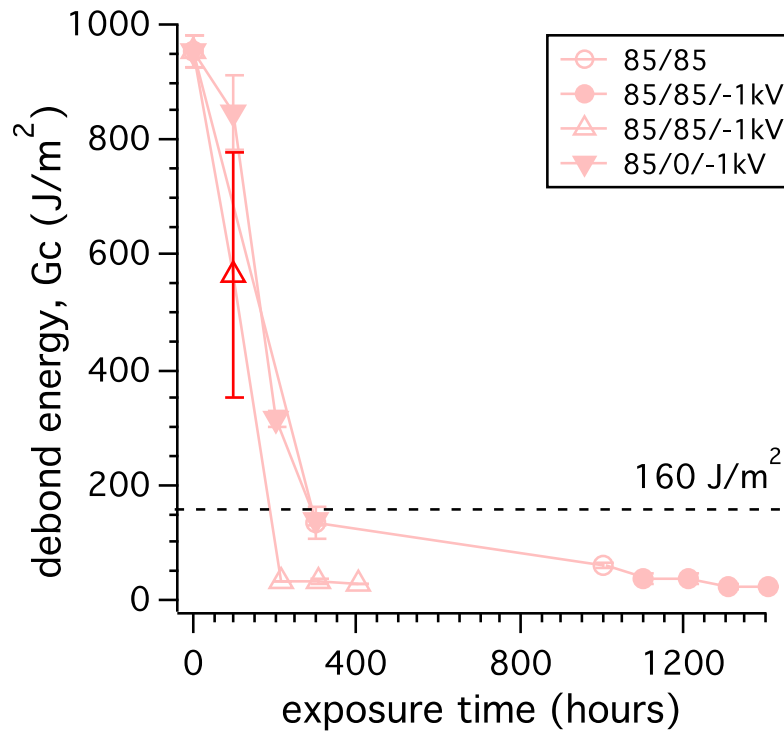
- parallel damp heat and bias exposure is more effective than a serial exposure

## Ag/ EVA bias series



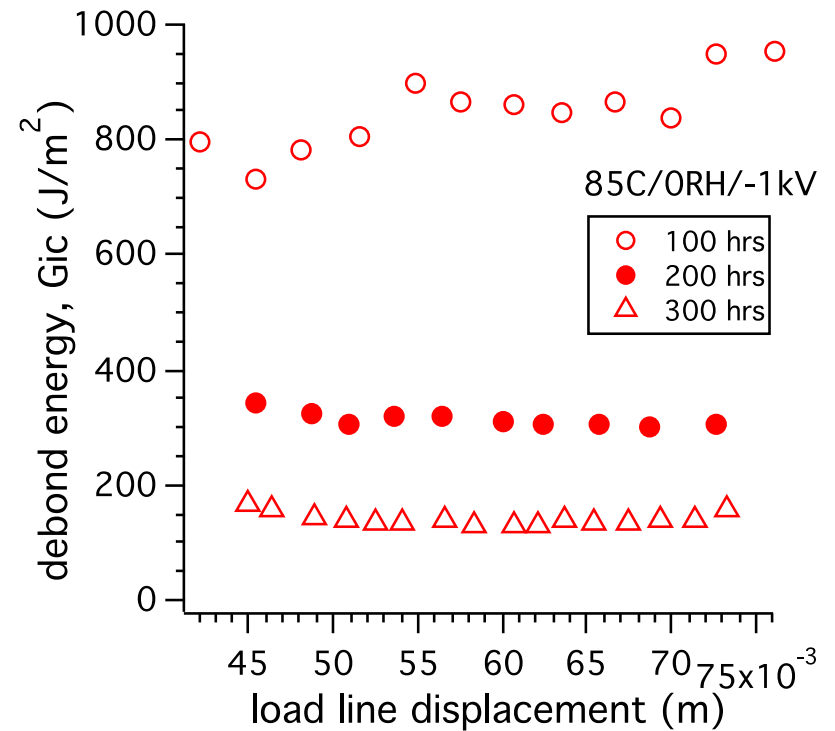
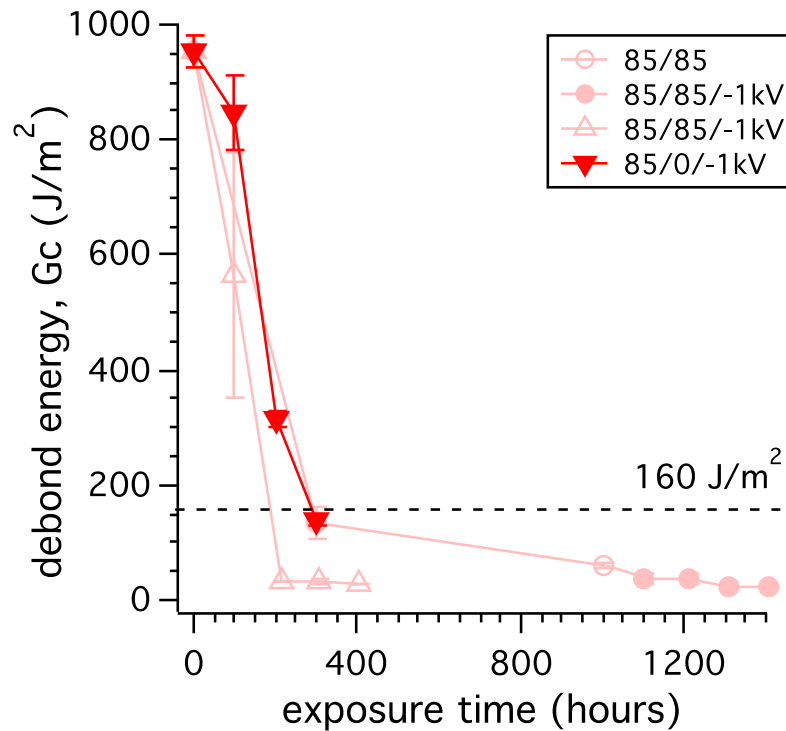
- damp heat and bias exposure is more effective than a serial exposure
- independent voltage mechanism observed
- bias mechanism accelerated in the presence of moisture

## Ag/ EVA bias series



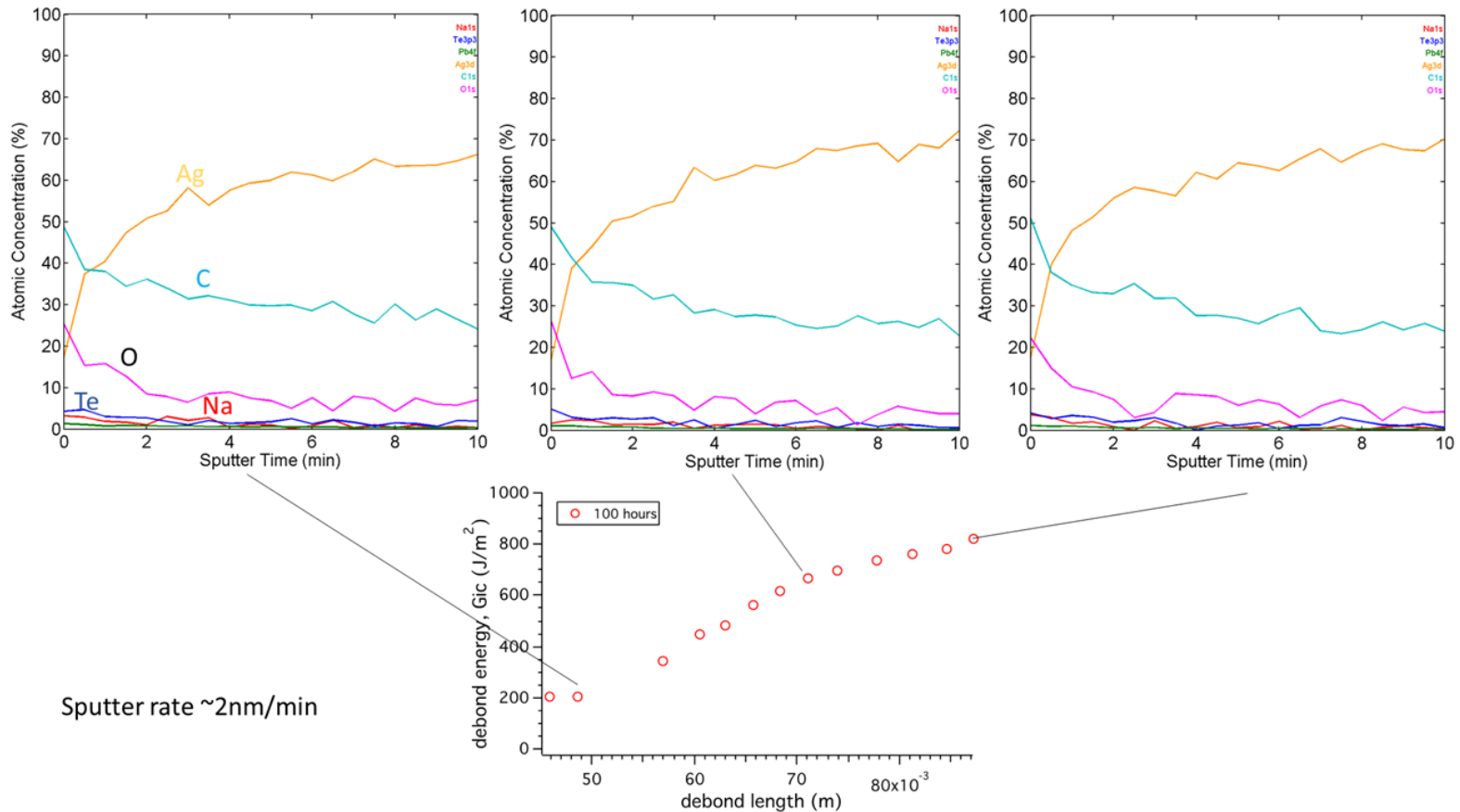
- adhesion gradient observed for short exposure times
- suggests moisture diffusion is the limiting mechanism

## Ag/ EVA bias series



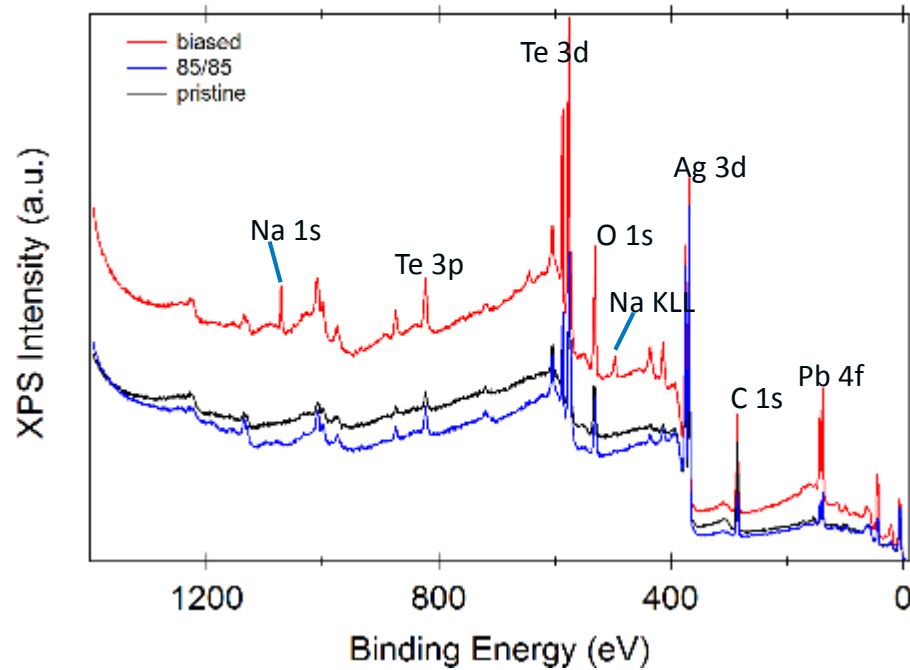
- uniform adhesion consistent with bias mechanism

# results



- XPS depth profiling does NOT show oxide formation responsible for decreased level of adhesion.

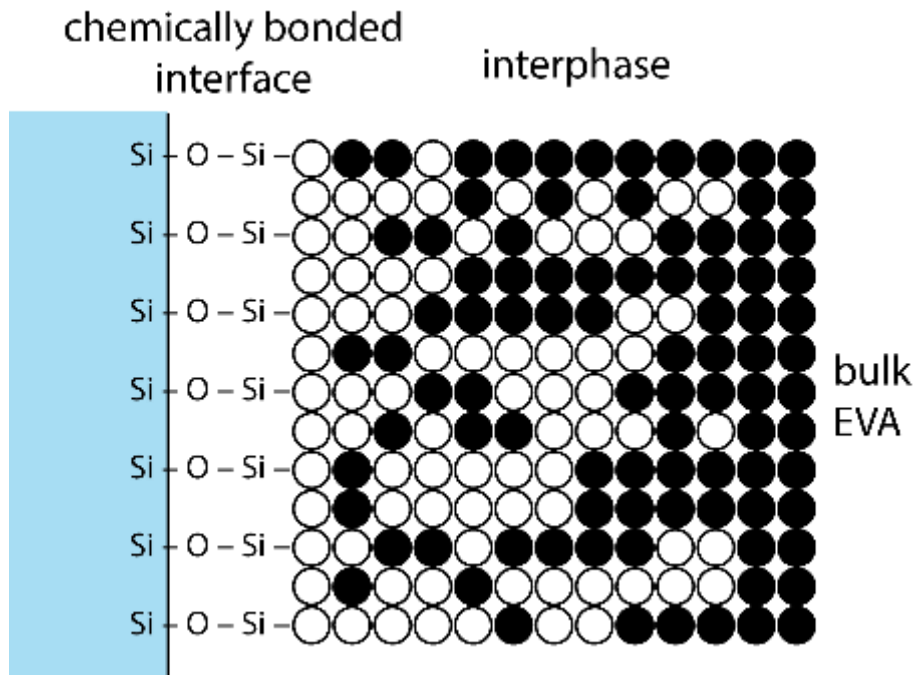




Sample	XPS file	Atomic Concentration (%)						
		C	O	Si	Ag	Te	Pb	Na
pristine	x170811_1	60	22	3.9	11	2.3	0.8	---
85/85	x170807_4	37	27	5.0	23	5.4	1.9	---
Biased	x170907_6	49	27	1.0	11	4	3.0	4.0

- Evidence of change in failure mode: cohesive to adhesive
- Na<sup>+</sup> is detected, but what is it doing?

# analysis



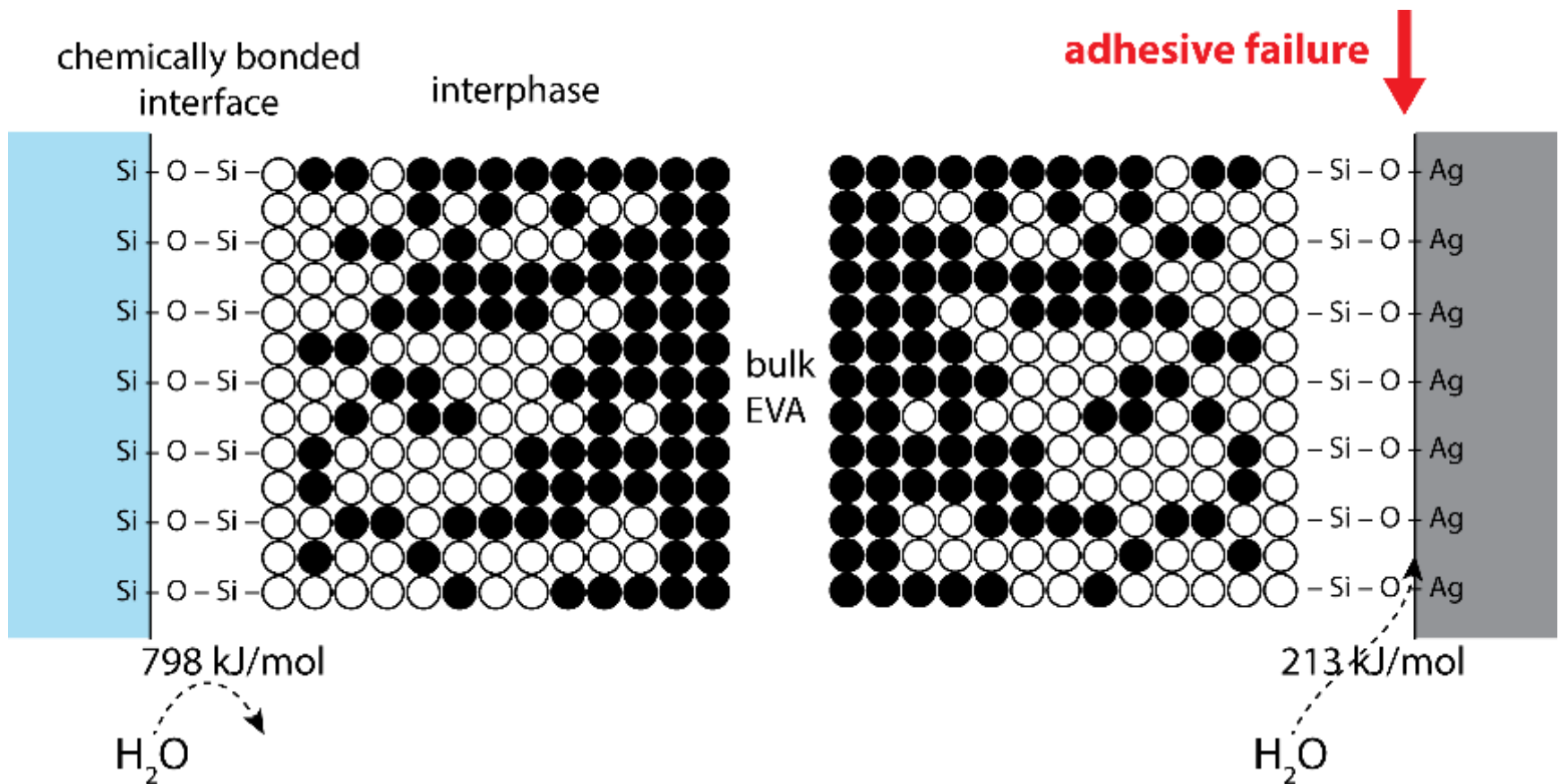
$$G_{c,siloxane} > G_{c,EVA}$$

- cohesive failure in the EVA occurs when siloxane bonded interface is intact.
- failure mode switches to adhesive when chemically bonded interface is degraded

↑  
cohesive failure

D.R. Coulter, E.F. Cuddihy, and E.P. Plueddemann, "Chemical Bonding Technology for Terrestrial Photovoltaic Modules," DOE/JPL-1012-91) JPL Publication 83-86, Nov. 15, 1983.

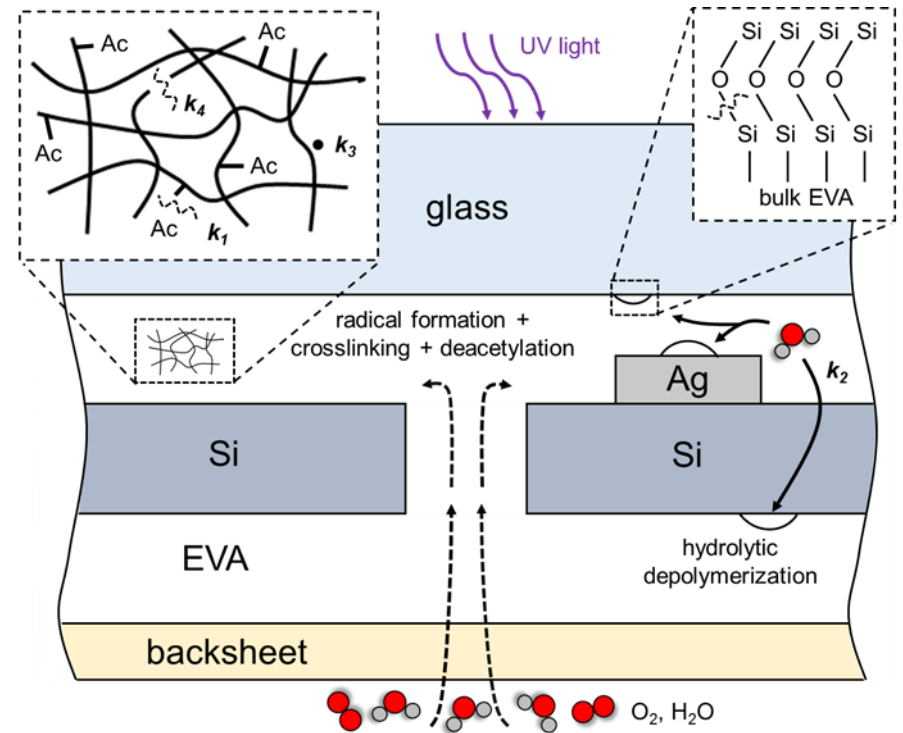
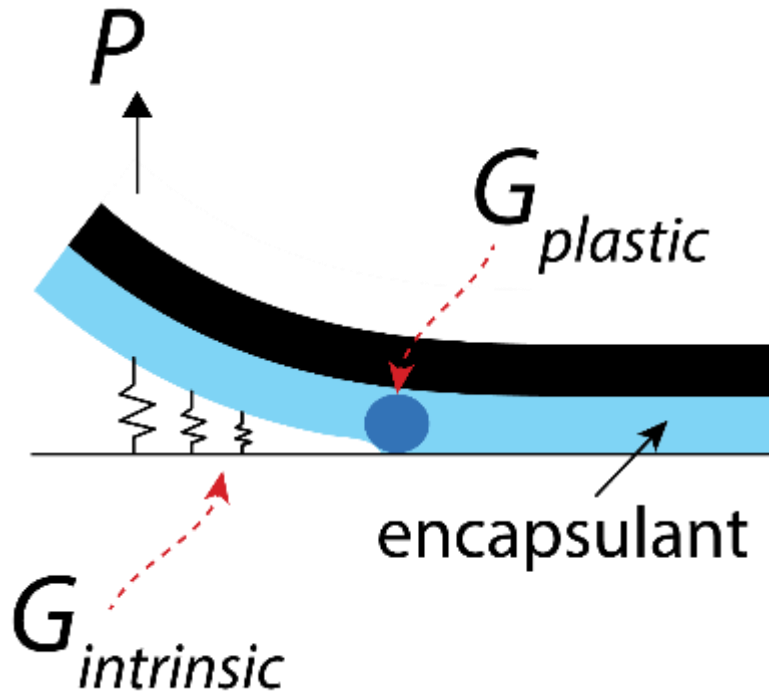
# analysis



- dissociation via moisture ingress
- changes failure mode from cohesive to adhesive failure at the Ag interface

D.R. Coulter, E.F. Cuddihy, and E.P. Plueddemann, "Chemical Bonding Technology for Terrestrial Photovoltaic Modules," DOE/JPL-1012-91) JPL Publication 83-86, Nov. 15, 1983.

# analysis



$$G_c(t) = \mathring{a} \sum_i^n G_{c,int,i}(t) + G_{c,PL}(t)$$

- Analytical model development: modular and extendable

Prof. Dagmar D'Hooge, Ghent University

## Analytical model development: modular and extendable

Prof. Dagmar Hooge, Ghent University, Belgium

$$G_c(t) = \sum_i G_{c,intr,i}(t) + G_{c,PL}(t)$$

Intrinsic Contribution

$$G_{c,intr,i}(t) = G_{c,intr,i}(0) f_i(t)$$

# bonds after rupture

$$f_i(t) = \exp\left(-a_i \left(1 - \frac{b_i(t)}{b_i(0)}\right)\right)$$

intensity factor of intrinsic process

# bonds initially

Non-linear Contribution

$$G_{c,PL}(t) = \sum_i^n G_{c,intr,i}(t) d(t)$$

$$d(t) = d(0) \left(1 - \frac{t}{t_\infty}\right)$$

proportionality factor

$$d(0) = \frac{G_c(0)}{\sum_i^n G_{c,intr,i}(0)} - 1$$

## Analytical model development: governing equations and functional form

$$f_i(t) = \exp\left(-a_i\left(1 - \frac{b_i(t)}{b_i(0)}\right)\right)$$

$$(\ ) = \sum \ , \ , (\ ) + \ , \ (\ ) \quad \text{?}$$

$$\frac{dc_{VAc}(t)}{dt} = -k_1 c_{VAc}(t) \quad \text{deacetylation (I)}$$

$$\frac{b_1(t)}{b_1(0)} = \exp(-k_1 t)$$

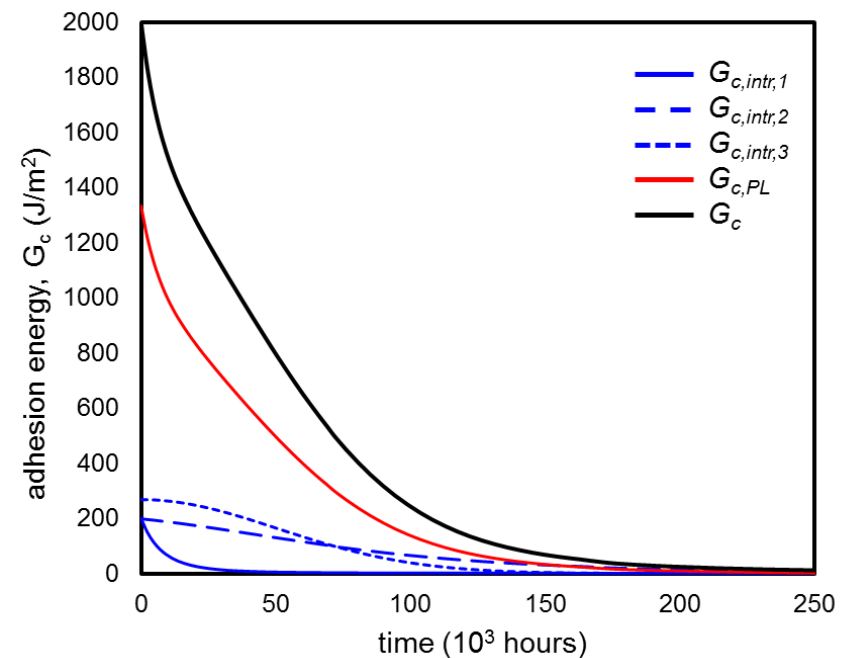
$$\frac{dc_{SiOSi}(t)}{dt} = -k_2 c_{SiOSi}(t) c_w(t) \quad \text{hydr. depolym. (III)}$$

$$\frac{b_2(t)}{b_2(0)} = \exp(-k_2 c_{w,eq} t)$$

$$\frac{dc_{MCR}(t)}{dt} = k_3 \mu_1 - k_4 c_{MCR}(t) \quad \text{radical formation and scission (II)}$$

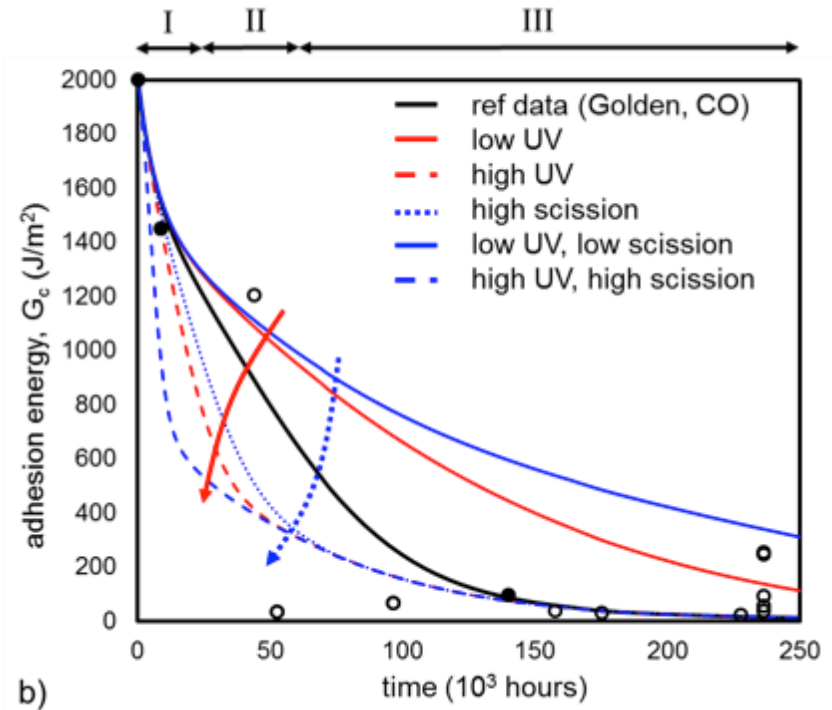
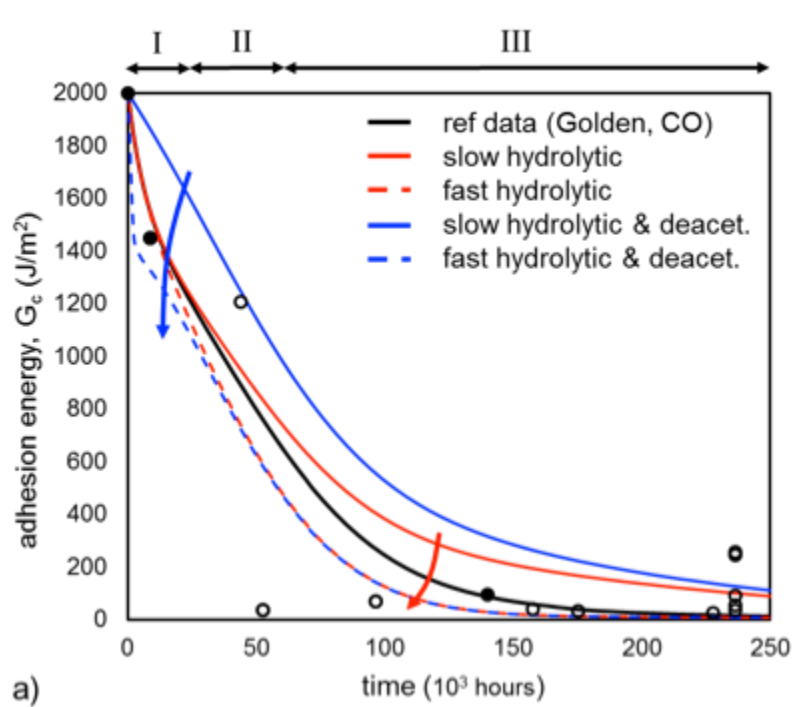
$$\frac{dc_{MM}(t)}{dt} = k_4 c_{MCR}(t)$$

$$\frac{b_3(t)}{b_3(0)} = \frac{c_{CL}(t)}{c_{CL}(0)} = \frac{k_3 \mu_1}{c_{CL}(0)} \left( t - \left( \frac{1}{k_4} + c_{MCR}(0) \right) (1 - \exp(-k_4 t)) \right)$$





## Analytical model development: parameter tuning



I. deacetylation

II. UV radicals + scission

III. hydrolytic depolymerization

- Quantifying the material property of adhesion
- Developing a modular and extendable model for adhesion degradation
- Current experiments to define degradation mechanisms and refine rate equations
- Work will enable accelerated tests to predict long-term adhesion performance
- A similar approach may be applied to all adhesive systems

[www.nrel.gov](http://www.nrel.gov)



# Quantifying Adhesion

## instructional videos

YouTube Search

Nick Bosco  
National Renewable Energy Laboratory

Width-Tapered Cantilever Beam Technique  
NREL Learning • 1/5 videos

- 1 Introduction NREL Learning
- 2 Coupon-Level Backsheet Adhesion Measurement NREL Learning
- 3 Module-Level Backsheet Adhesion Measurement NREL Learning
- 4 Coupon-Level Encapsulant Adhesion Measurement NREL Learning
- 5 Module-Level Encapsulant Adhesion Measurement NREL Learning

0:02 / 0:23

<https://youtu.be/q19li68J60c?list=PLmIn8Hncs7bFpFFBpUQnKXzzx54wucPp1>

- Tracy, J., Bosco, N., Novoa, F., Dauskardt, R., "Encapsulant and backsheet Adhesion Metrology for Photovoltaic Modules", ***Progress in Photovoltaics***, 25:87-96, Sept 2016
- Bosco, N., Kurtz, S., Tracy, J., Dauskardt, R. "Development and First Results of the Tapered Width Beam Method for Adhesion Testing of Photovoltaic Material Systems", ***IEEE Journal of Photovoltaics***, 2016
- N. Bosco, J. Eafanti, S. Kurtz, J. Tracy and R. Dauskardt, "Defining Threshold Values of Encapsulant and Backsheet Adhesion for PV Module Reliability," in ***IEEE Journal of Photovoltaics***, vol. 7, no. 6, pp. 1536-1540, Nov. 2017.
- J. Tracy, N. Bosco and R. Dauskardt, "Encapsulant Adhesion to Surface Metallization on Photovoltaic Cells," in ***IEEE Journal of Photovoltaics***, vol. 7, no. 6, pp. 1635-1639, Nov. 2017.