

High-Voltage, High-Frequency Devices for Solid State Power Substation and Grid Power Converters


Allen R. Hefner

Semiconductor Electronics Division
National Institute of Standards and Technology
Gaithersburg, MD 20899
hefner@nist.gov

The devices discussed in this paper were produced by Cree/Powerex.
NIST does not necessarily recommend or endorse the devices as the best
available for the purpose.



Outline

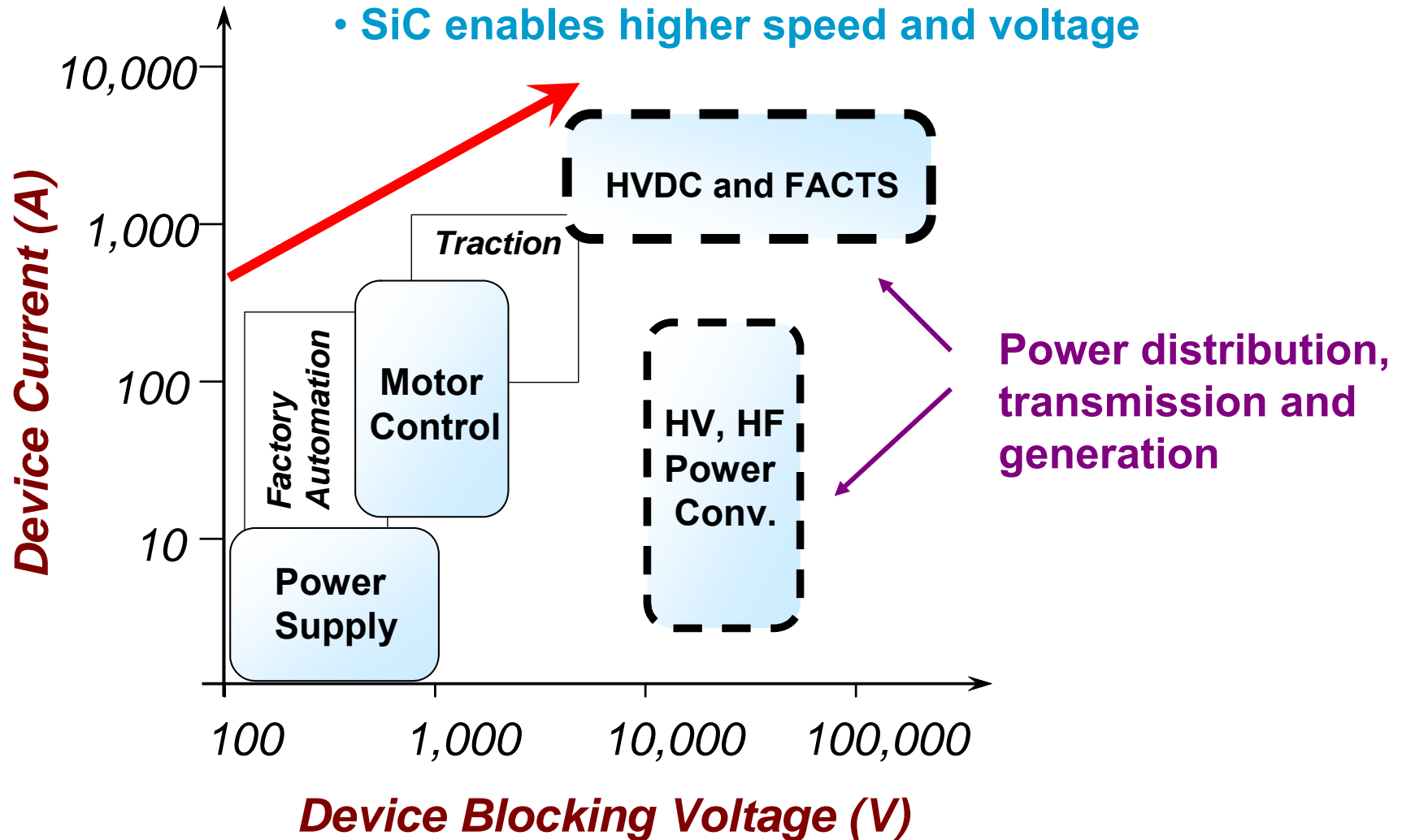
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- **HV-HF SiC Power Devices**
 - **DARPA HPE Program Overview**
 - **Goal: Solid State Power Substation (SSPS)**
 - **Status: 10 kV, 100 A, 20 kHz power modules**
 - **Component Modeling and Circuit Simulation**
 - **Impact on Grid-Connected Power Converters**

HV-HF Power Conversion

- **Switch-mode power conversion and conditioning:**
 - advantages: efficiency, control, functionality, size and weight
 - semiconductors from: 100 V, ~MHz to 6 kV, ~100 Hz
- **New semiconductor devices extend application range:**
 - **1990's: Silicon IGBTs**
 - higher power levels for motor control and traction
 - **Emerging: SiC Schottky diodes and MOSFETs**
 - higher speed for power supplies and motor control
 - **Future: HV-HF SiC MOSFET, PiN diode, Schottky, and IGBT**
 - enable 15-kV, 20-kHz switch-mode power conversion

Switch-Mode Power Applications

- Switching speed decreases with voltage
- SiC enables higher speed and voltage



SiC Power Devices

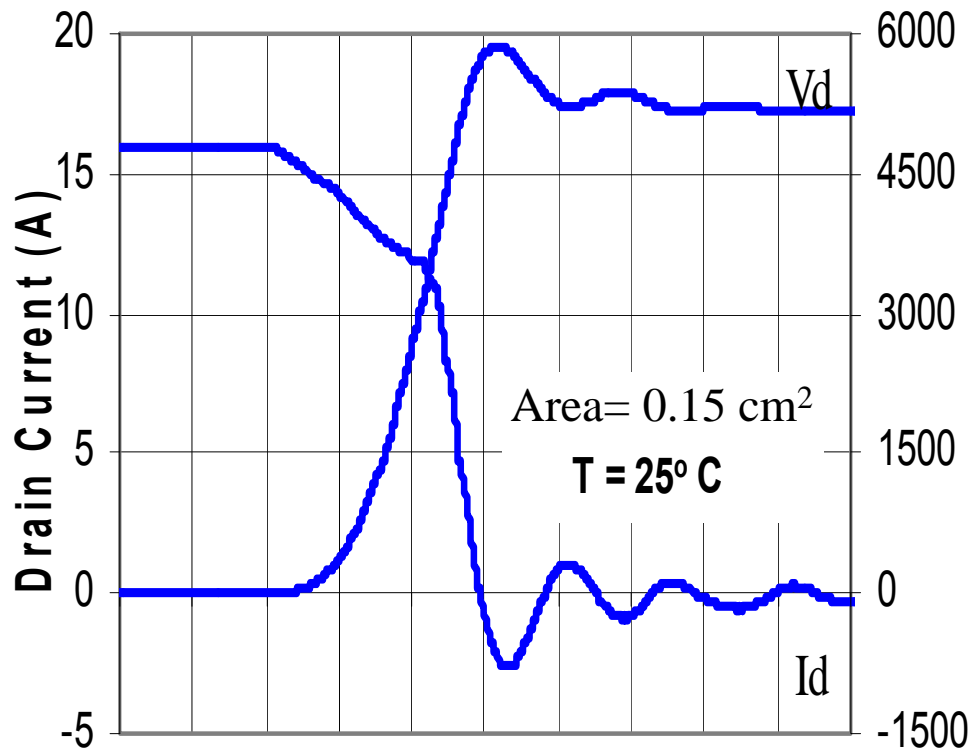
SiC wide bandgap material enables better electrical and thermal performance than Si power devices

Semi-Conductor Material	Energy Bandgap (eV)	Breakdown Electric Field (V/cm)	Thermal Conductivity (W/m·K)	Saturated Electron Drift Velocity (cm/sec)
4H-SiC	3.26	$2.2 \cdot 10^6$	380	$2.0 \cdot 10^7$
Si	1.12	$2.5 \cdot 10^5$	150	$1.0 \cdot 10^7$

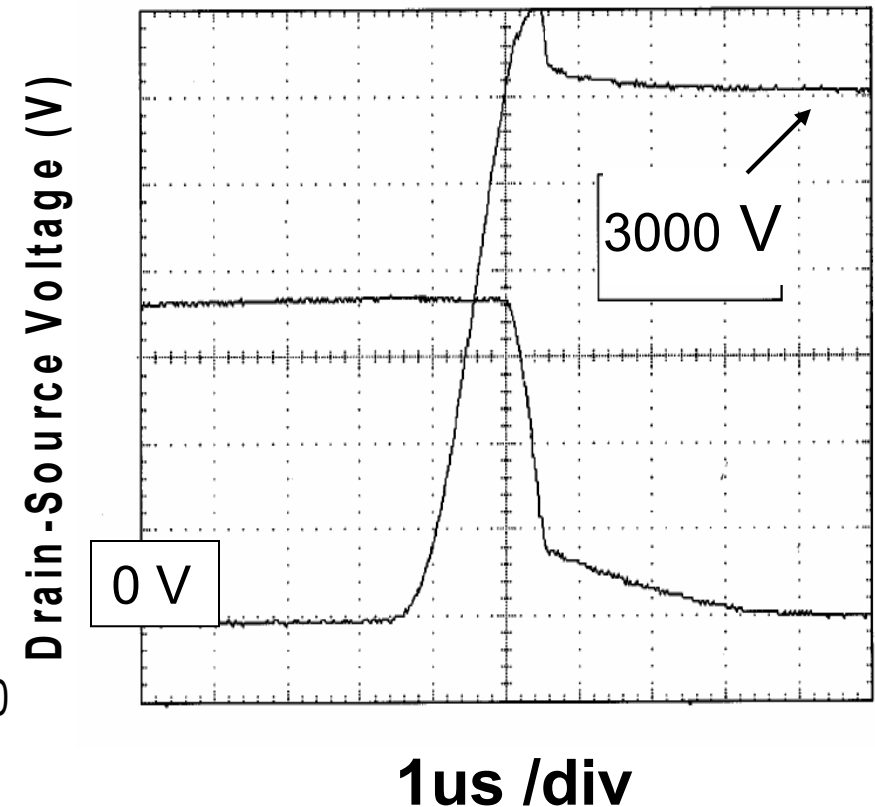
- Handles higher temperature: larger bandgap
- Higher voltage, current and speed: larger breakdown field
- Fault tolerance, Pulsed: intrinsic-temperature, saturation-velocity and thermal-conductivity

DARPA HPE MOSFET: High Speed at High Voltage

SiC MOSFET: 10 kV, 30 ns

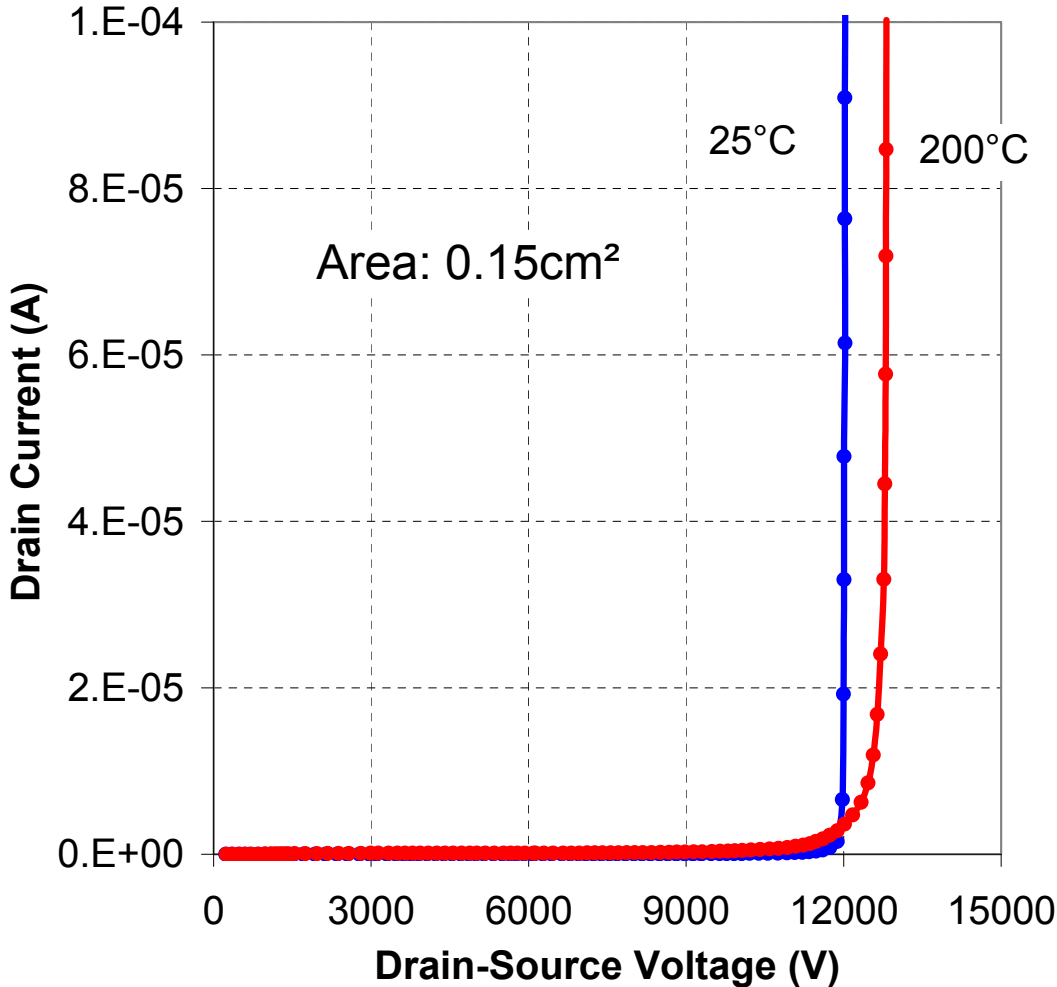


Silicon IGBT: 4.5 kV, 2us

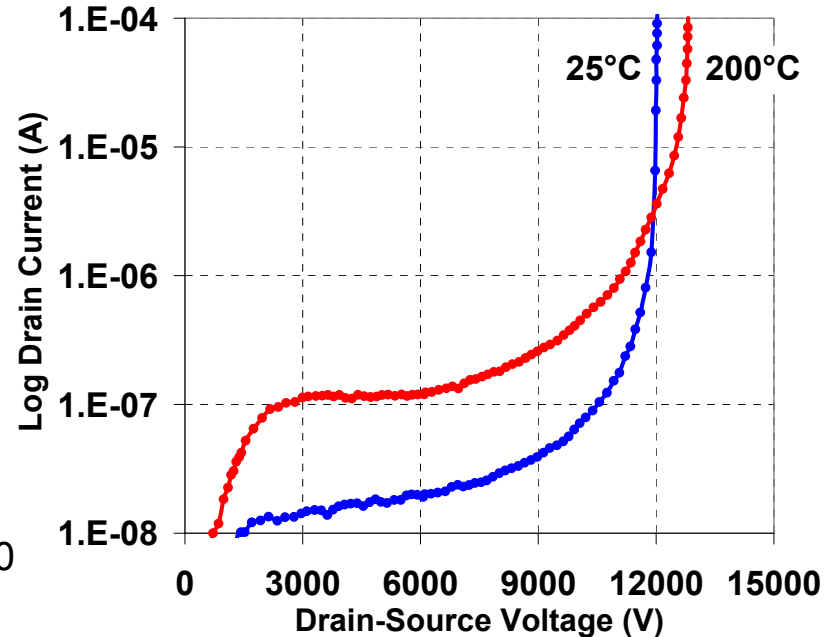


MOSFET Voltage Capability

Voltage Capability > 12 kV



Low Channel Leakage for $V_g \leq 0$, $T \leq 200^\circ\text{C}$
Increased Threshold Voltage



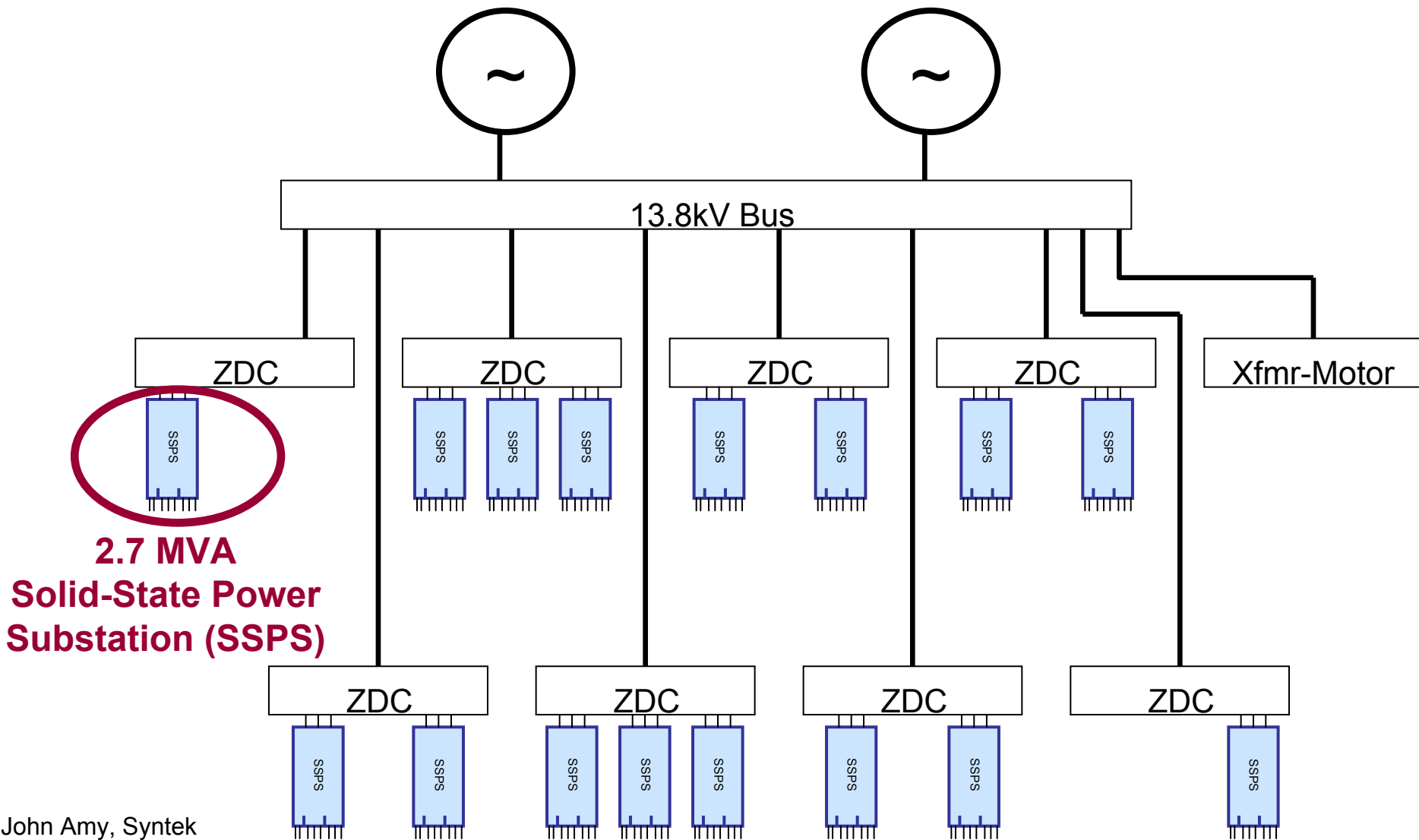
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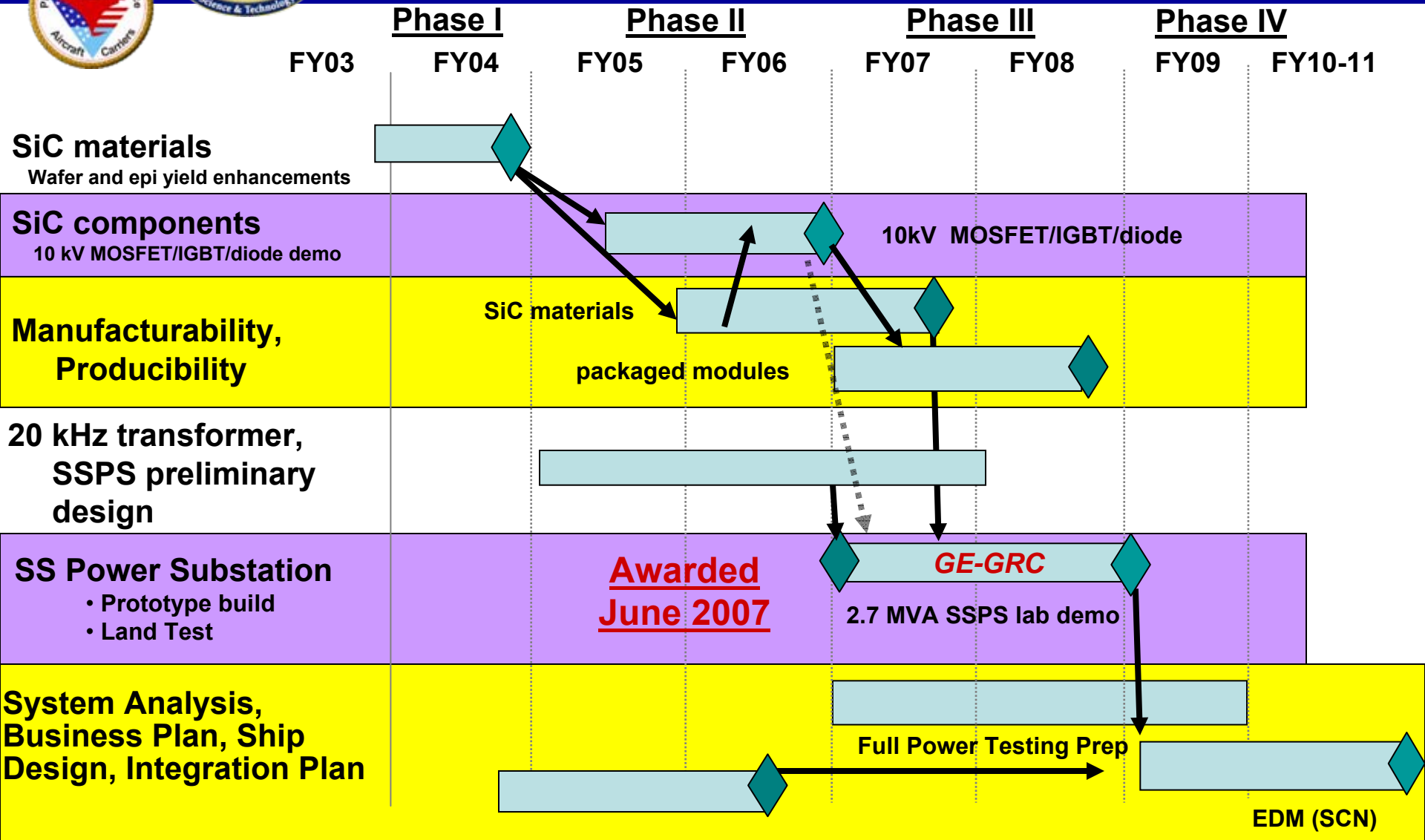
HPE Program Application

CVN21 Aircraft Carrier Zonal Distribution System





HPE Program Timeline



DARPA HPE SiC Devices

- HV-HF SiC power devices:

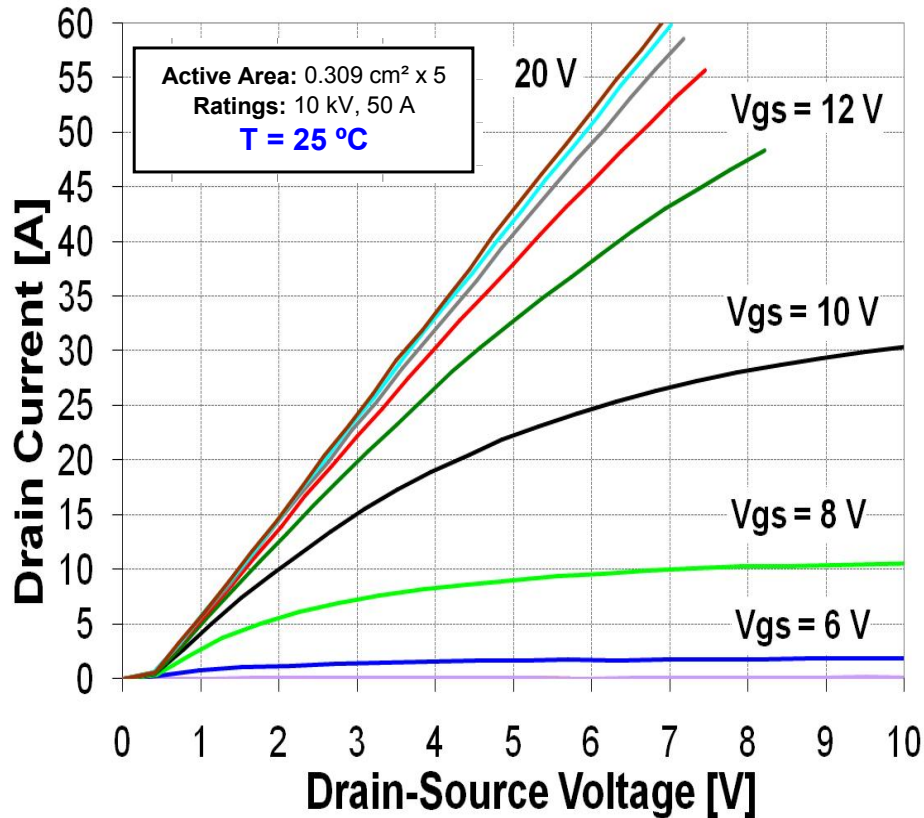
“game changer” enabling SSPS

- HPE Phase II device and module goals:

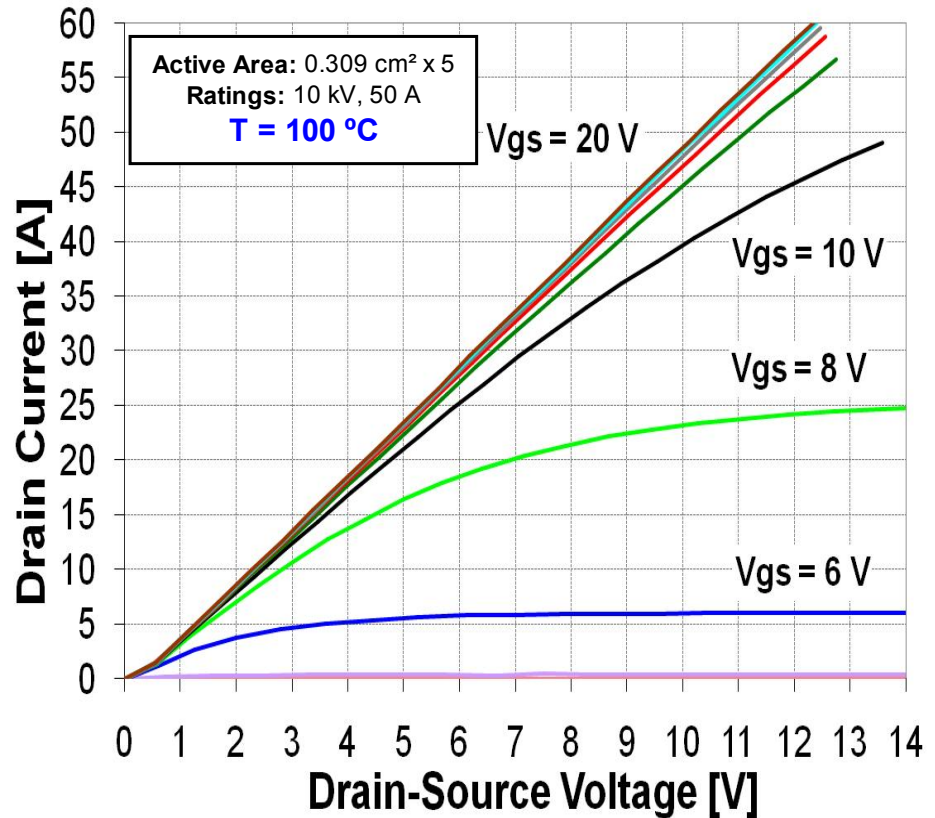
DARPA High Power Electronics Proposed Device Development				
	PiN, (JBS) (single die)	MOSFET (single die)	IGBT* (single die)	Half Bridge Module
BV (V)	10 kV	10 kV	15 kV*	10 – 15 kV
I _{on} (A)	45 A (18 A)	18 A	25 A	110 A
T _j (°C)	200 C	200 C	200 C	200 C
F _{sw} (Hz)	20 kHz	20 kHz	20 kHz	20 kHz

Measured Output Characteristics for 50 A, 10 kV SiC MOSFET Module

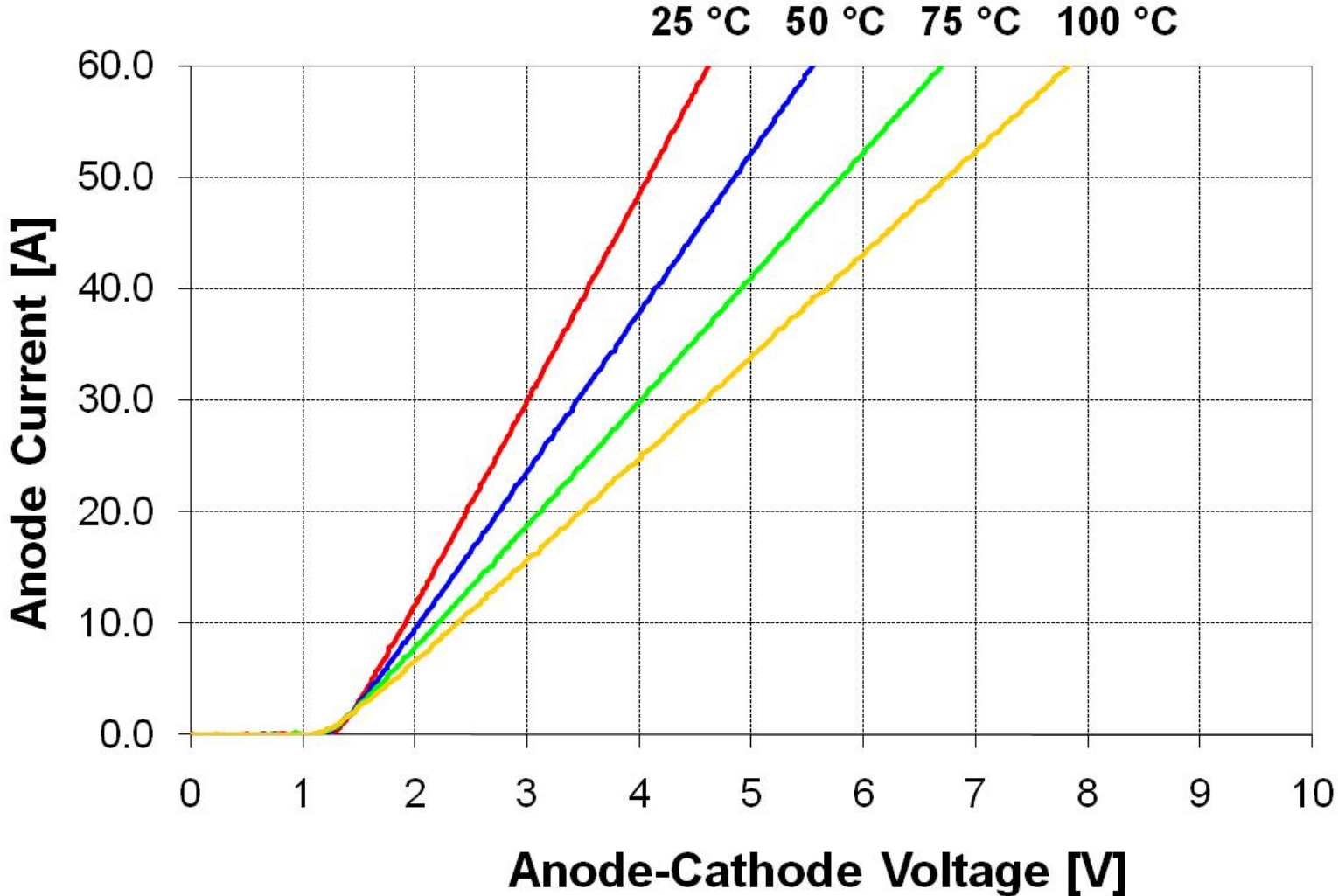
25 °C



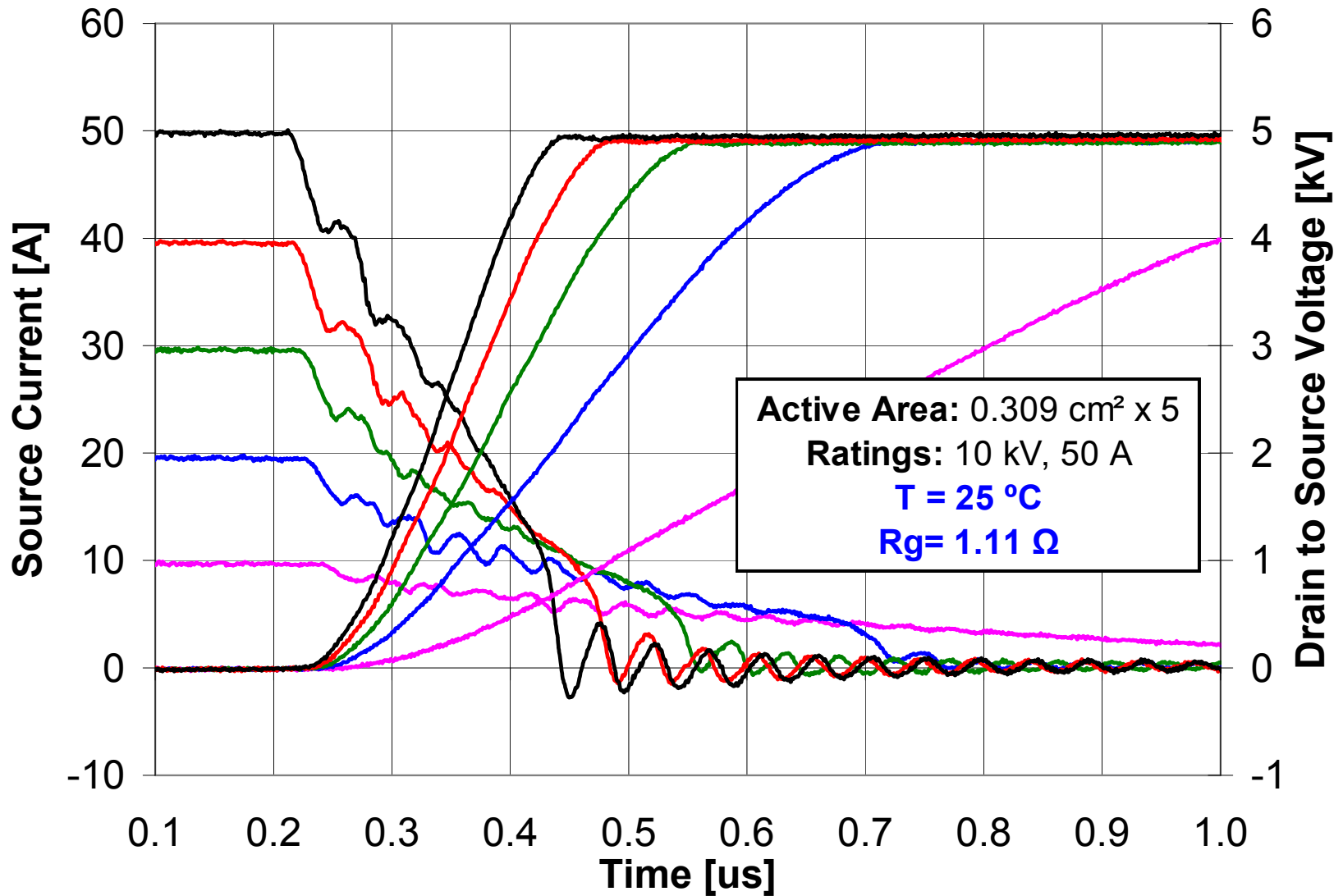
100 °C



Measured SiC JBS Diode Characteristics for 50 A, 10 kV Half-Bridge Module



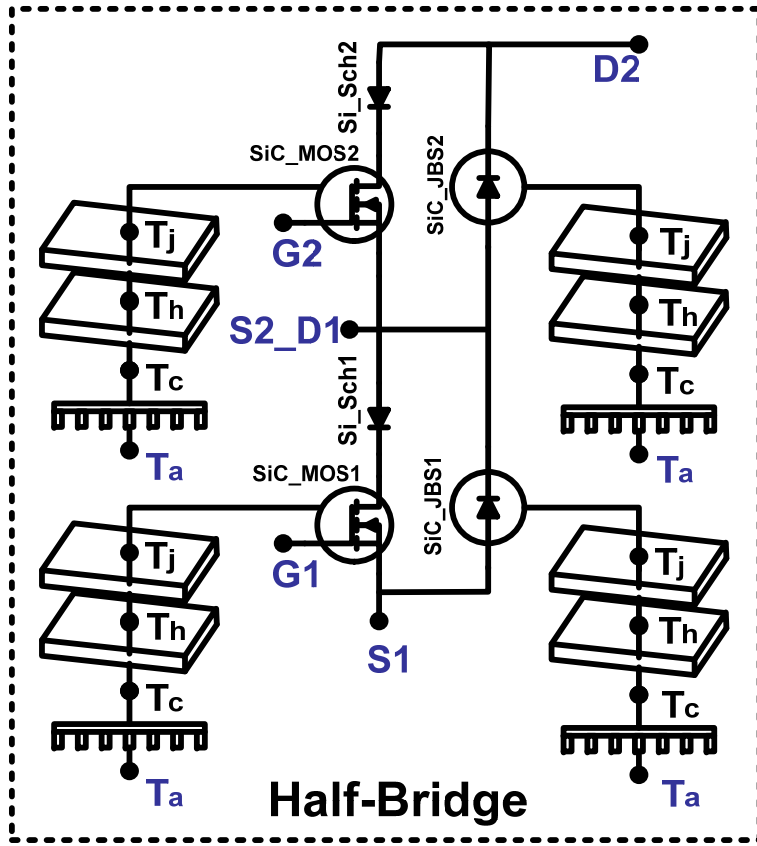
Inductive Load Turn-Off for 50 A, 10 kV Half-Bridge Module



Outline

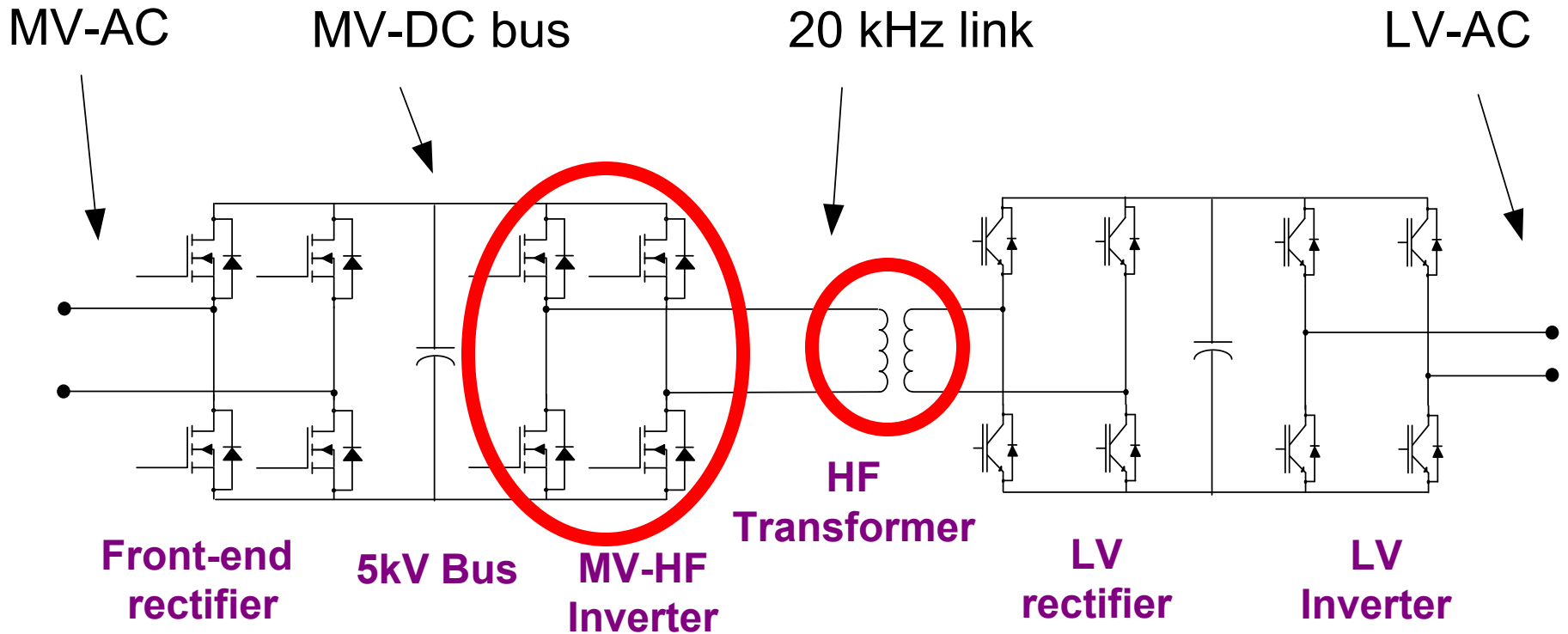
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SiC MOSFET/JBS Half-Bridge Module Model and Circuit Simulation



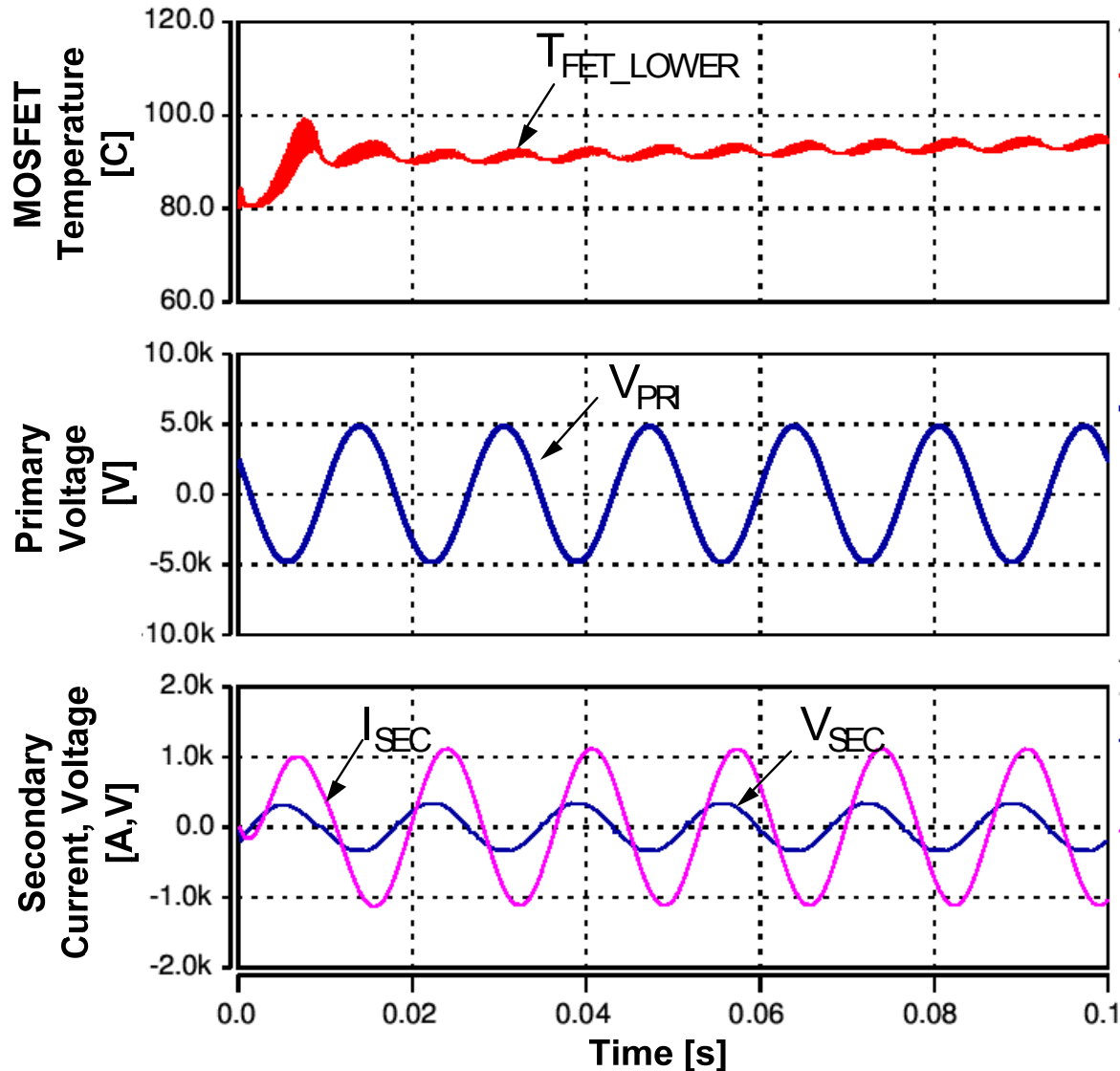
- **Model being used to perform simulations necessary to:**
 - optimize module parameters
 - determine gate drive requirements
 - SSPS system integration
 - impact on grid power converters
- **Half-bridge module model:**
 - 10 kV SiC power MOSFETs
 - 10 kV SiC JBS for anti-parallel diodes
 - low-voltage Si Schottky diodes
 - voltage isolation and cooling stack
- **Validated models scaled to 100 A, 10 kV half bridge module**

Representative SSPS Topology



This configuration would require twelve blocks to implement a three-phase 2.75 MVA, 13.8 kV to 465 V SSPS.

Electro-Thermal SSPS Simulation



- Optimized module with AMOSFET = 3 cm² and AJBS = 2 cm²
- Worst case coolant temperature of 80 °C
- Rated load at 0.8 power factor lagging
- MOSFET temperature rises by 20 °C to 100 °C at start-up

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Impact on Grid Power Converters

Objective:

- **High-Megawatt Power Conditioning Systems (PCS) are required to convert:**
 - from power produced by Fuel Cells (FC) in future power plants
 - to very high voltage and power required for delivery to the grid

Motivation:

- **DoE SECA cost goals:**
 - FC generator plant \$400/kW
 - including \$40-100/kW for PCS
- **Today's PCS cost (*Fuel Cell Energy Inc.*):**
 - FC generator plant \$3,000/kW
 - including \$260/kW for power converter (to 18 kV AC)



300 MW PCS

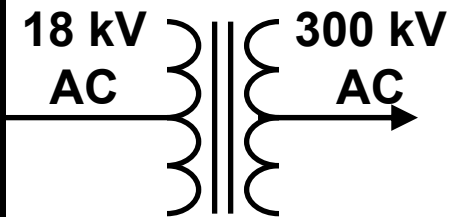
~700 V
DC



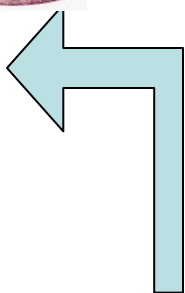
Approx.
500
Fuel
Cells



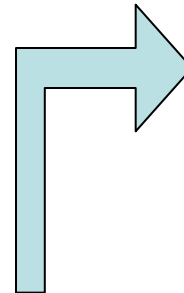
~700 V
DC



\$40-\$100 / kW



Ripple < 2%
Stack Voltage Range
~700 to 1000 V



IEEE – 519
IEEE – 1547
Harmonic Distortion

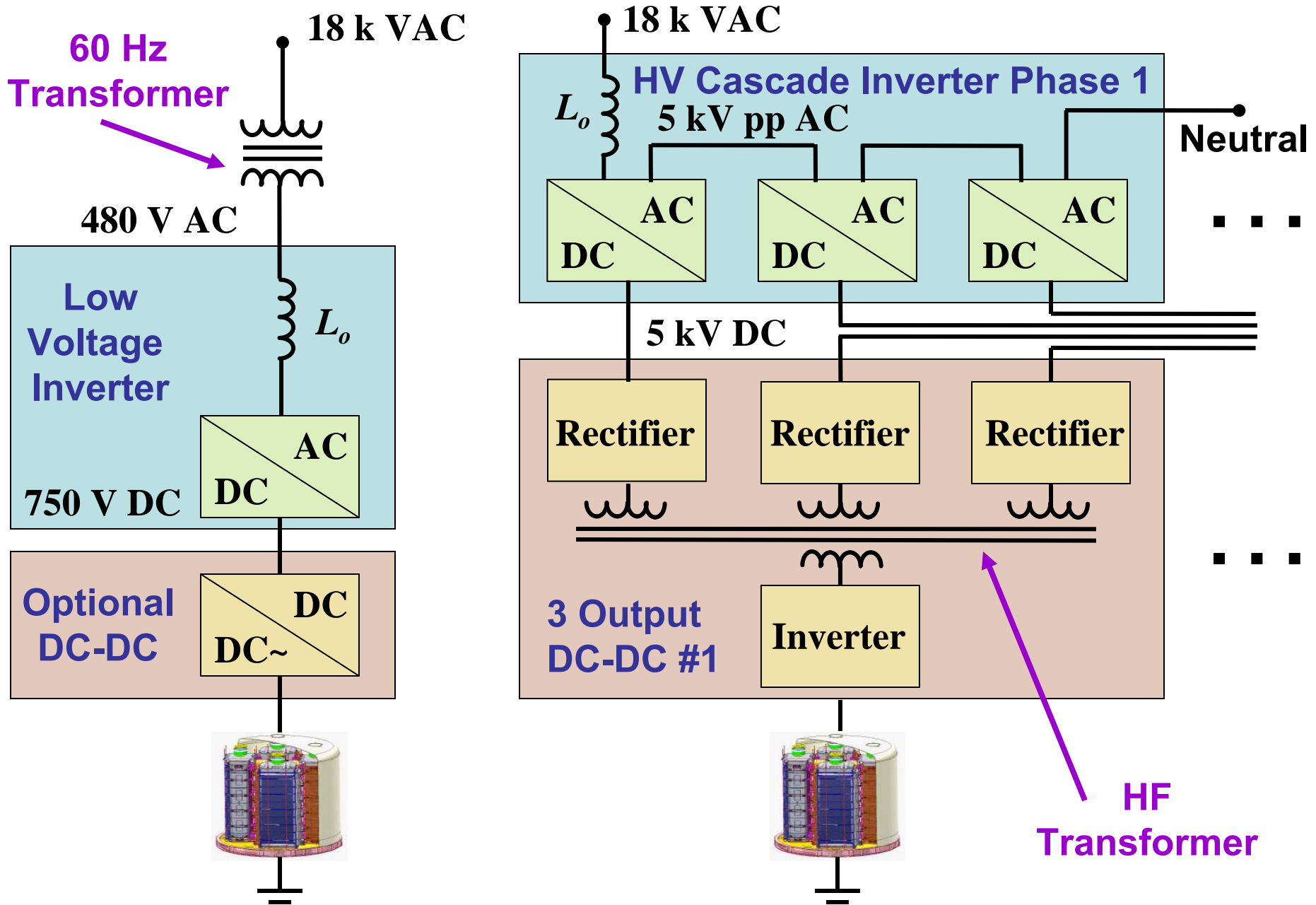
Advanced Technology Cost

- Future, high-volume costs: 5 to 10 years, 1 GW/yr
- **Advanced Technology Goals and Cost Break Points**
 - 1.2 kV Schottky diodes: **\$0.2/A**
 - 12 kV Schottky diodes: **\$1/A**
 - 12 kV Half-bridge SiC-MOSFET/SiC-Schottky: **\$10/A**
 - 15 kV SiC-PiN: **\$0.4/A**
 - 15 kV SiC-IGBT/SiC-PiN Module: **\$3.3/A**
 - Nano-crystalline transformer: **\$2/kW**
 - Power Electronics DC-DC, DC-AC: **150 % overhead**
 - 60Hz Transformer and Switchgear: **50 % overhead**

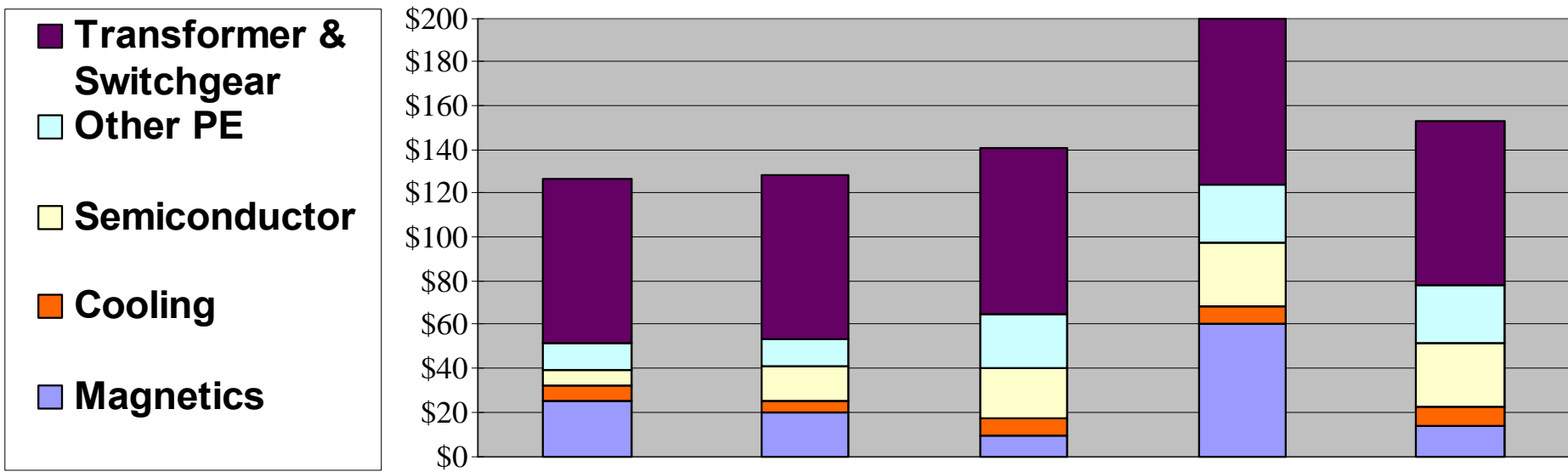
Power Converter Architectures

- **Low-Voltage Inverters (460 V AC):**
 - Require high inverter current for each FC module
 - and large number of Inverters for 300 MW Plant
- **Medium-Voltage Inverters (4160 V AC):**
 - Lower inverter current for each FC module
 - Combine multiple FCs with single high power inverter
- **High-Voltage Inverters (18 kV AC):**
 - Replaces 60 Hz transformer with isolation from HF transformer
 - Cascade enables: 18 kV AC inverter by series connection, and interleaved switching decreases losses and filter requirement

HF Transformer versus 60 Hz Transformer



Estimated \$/kW: LV Inverter

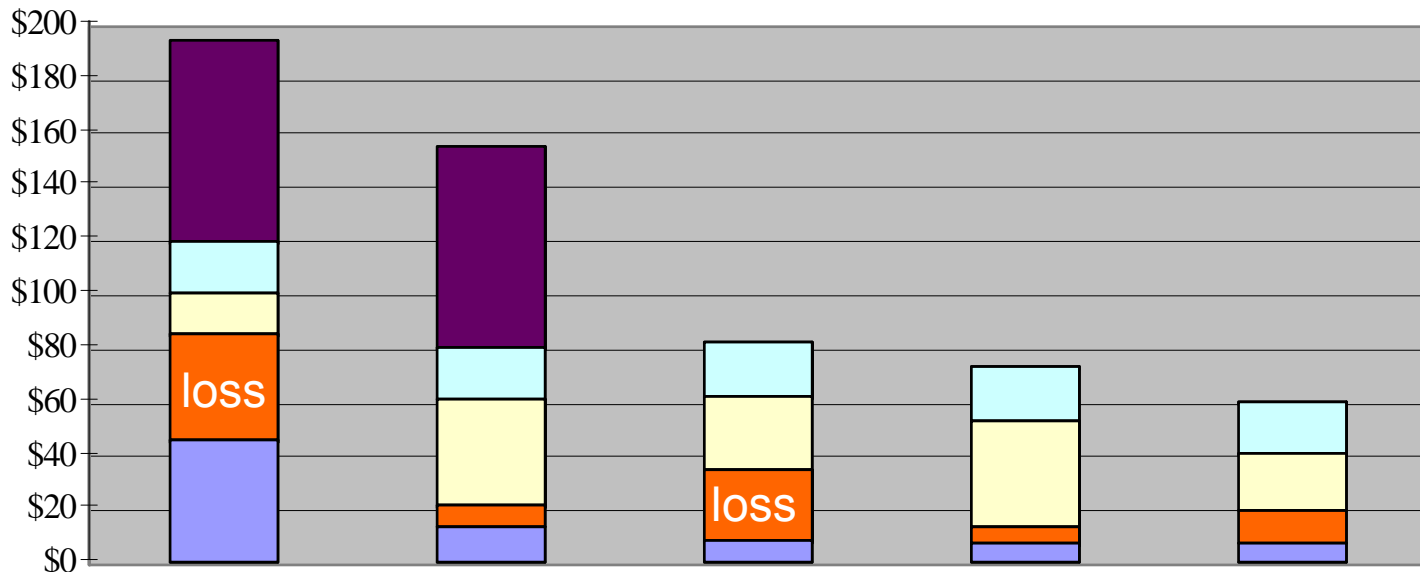


Inverter Voltage	Low	Low	Low	Low	Low
Converter Stages	One	One	Two	Two	Two
LV-SiC Schottky		yes	yes	yes	yes
HF Transformer				Ferrite	Nano
60 Hz Transformer	yes	yes	yes	yes	yes

Risk Level: Low Moderate Considerable High

Estimated \$/kW: MV & HV Inverter

- Transformer & Switchgear
- Other PE
- Semiconductor
- Cooling
- Magnetics



Inverter Voltage	Medium	Medium	High	High	High
HV-SiC Diode		Schottky	Schottky	Schottky	PiN
HV-SiC Switch		MOSFET		MOSFET	IGBT
HF Transformer	Nano	Nano	Nano	Nano	Nano
60 Hz Transformer	yes	yes			

Risk Level:

Low

Moderate

Considerable

High

Conclusion

- **HV-HF switch-mode power conversion:**
 - SiC material enables HV-HF devices
 - efficiency, control, functionality, size and weight,... cost
- **DARPA HPE SiC devices reduce weight for CVN21**
 - Phase II is developing 100 A, 10 kV SiC power modules
 - Phase III goal is 13.8 kV 2.7 MVA Solid State Power Substation
- **Circuit simulation used to**
 - Optimize SiC module and system
 - Evaluate impact of new technology on grid power converters
- **SECA goal of \$40-\$100 / kW for the fuel cell plant**
 - High-Voltage grid-connected inverter may reduce cost
 - Requires HV-HF SiC devices and HF power transformer

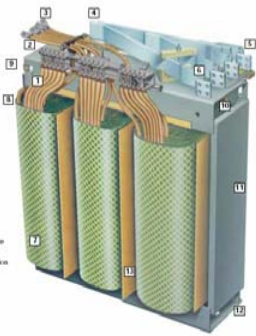
SiC Benefits and Requirements

Voltage and Current Range

BV (kV)	0.3 – 1.2 kV	2 – 6 kV	10 – 15 kV	20 – 40 kV
Ion (A)	1 - 500 A	50 – 3000 A	3 – 1000 A	200 A
Si Speed	20ns PiN	<1k - 15kHz	---	---
SiC Speed	0ns Schottky	> 20 kHz	50ns, 20 kHz	> 1 kHz
SiC Benefits	Efficiency *High Temp HT Coolant	Efficiency Control	Control Functionality Weight	Control Functionality Part Count
SiC Barrier	Cost *HT Package *MOS mobility/ oxide reliability	Cost Large Area/ Full-wafer- device	Vf degradation HV-HF package Yield High Volume	HV substrate Vf degradation Series Package

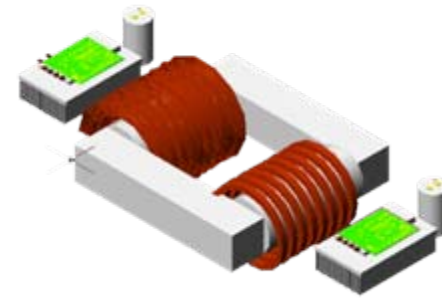


HPE Phase III Goal



Low Frequency Conventional Transformer (analog)

- 2.7MVA
- 13.8kV/450V (Δ/Y) 60Hz
- **6 tons/each**
- **10 m³/each**
- **fixed, single output**



Estimated SiC-based Solid State Power Substation (digital)

- 2.7 MVA
- 13.8kV/465V (Δ/Y) 20 kHz
- **1.7 tons/each**
- **2.7 m³/each**
- **multiple taps/outputs**

BENEFITS:

- **Reduction of weight and volume**
- **Precise voltage regulation to isolate voltage spikes, voltage dips**
- **Unity Power Factor (20% increase in power)**
- **Fast fault detection, protection, and potential removal of circuit breakers**