

Real-Scale Upholstered Furniture Flammability and Effect of Silicone-Based Backcoating

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Introduction

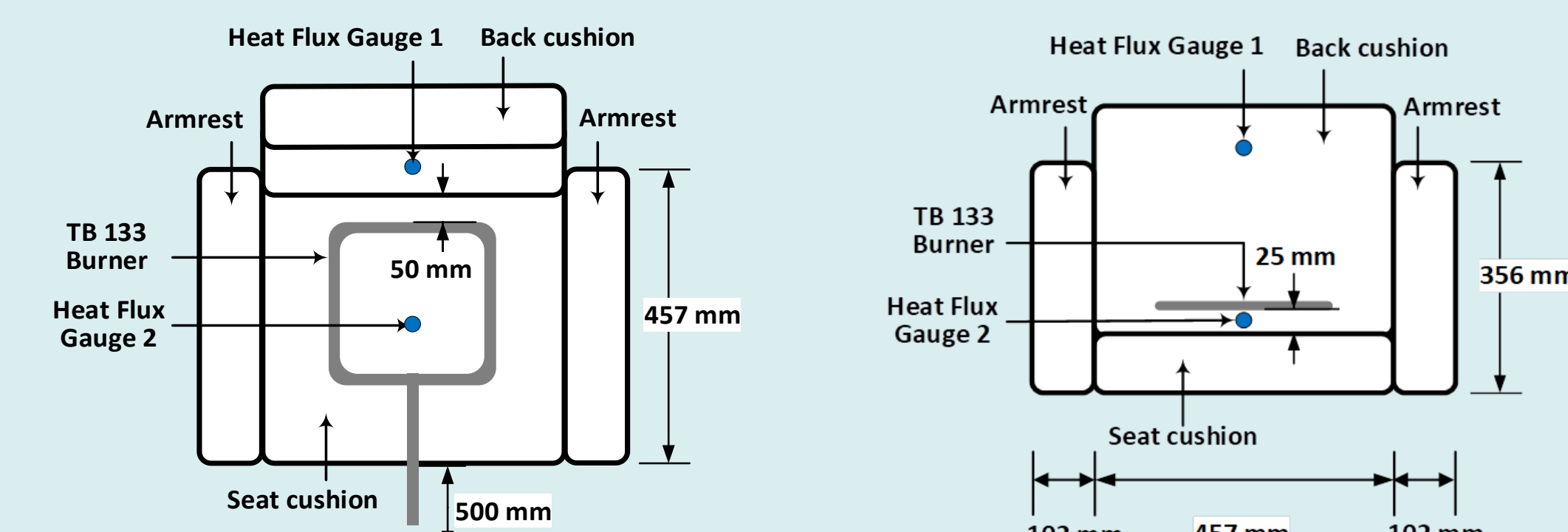
In this study, the effectiveness of a NIST developed silicone backcoating as flame-retardant in upholstered furniture has been demonstrated by full-scale smoldering and flaming tests. [1] A silicone-based elastomer filled with vinyl-silane modified aluminum-hydroxide is applied to the back of the upholstery fabric to generate an effective fire barrier with an expected benign toxicological and environmental profile. The flammability of the chair mock-ups with pristine uncoated upholstery fabric (UC) and backcoated upholstery fabric (BC) have been compared by using Cal. TB 133 [2] as flaming ignition source and NIST SRM 1196 as smoldering ignition source. Abrasion resistance and flexibility of UC and BC fabrics were also tested.

Silicone-based Back-Coated Mockup



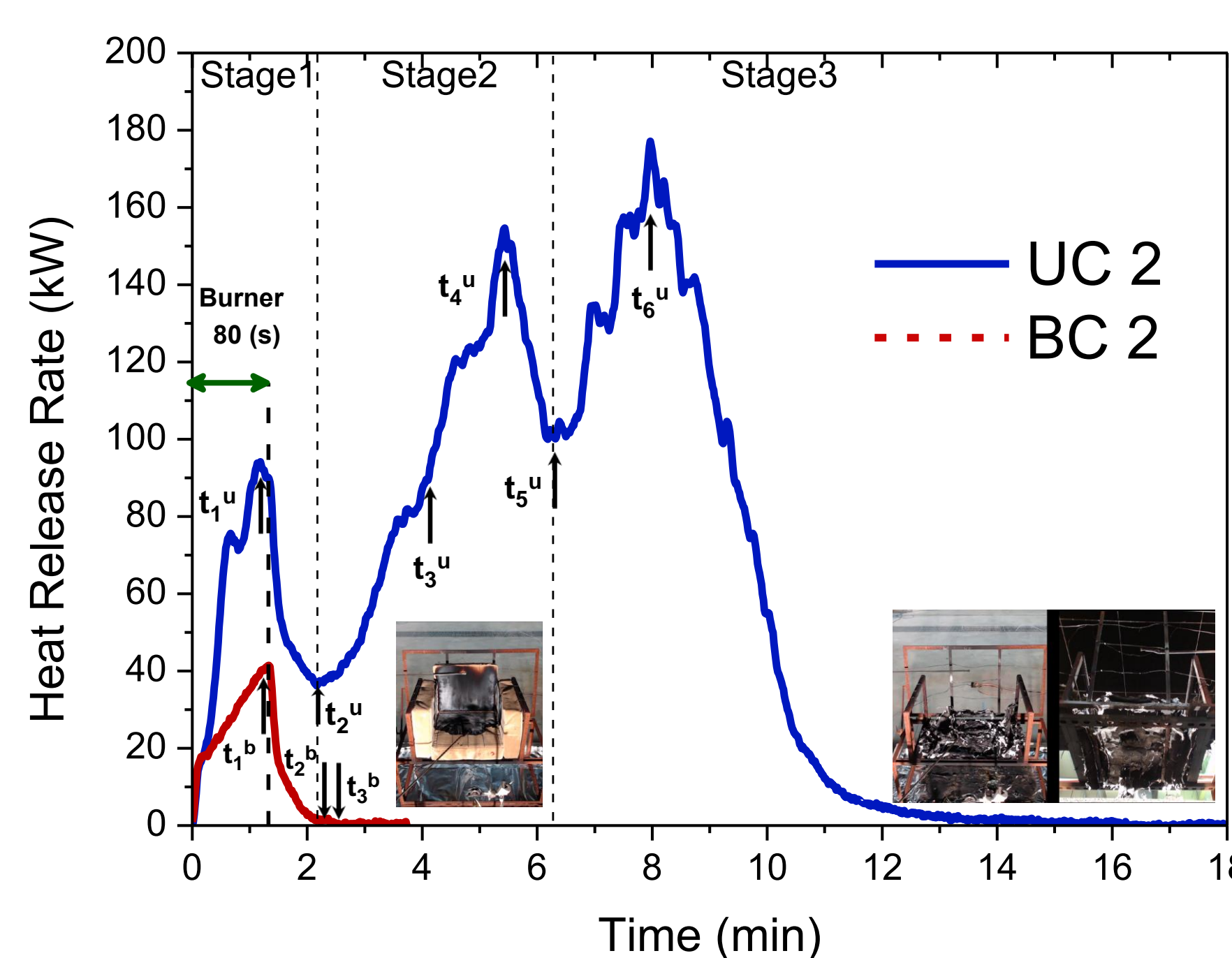
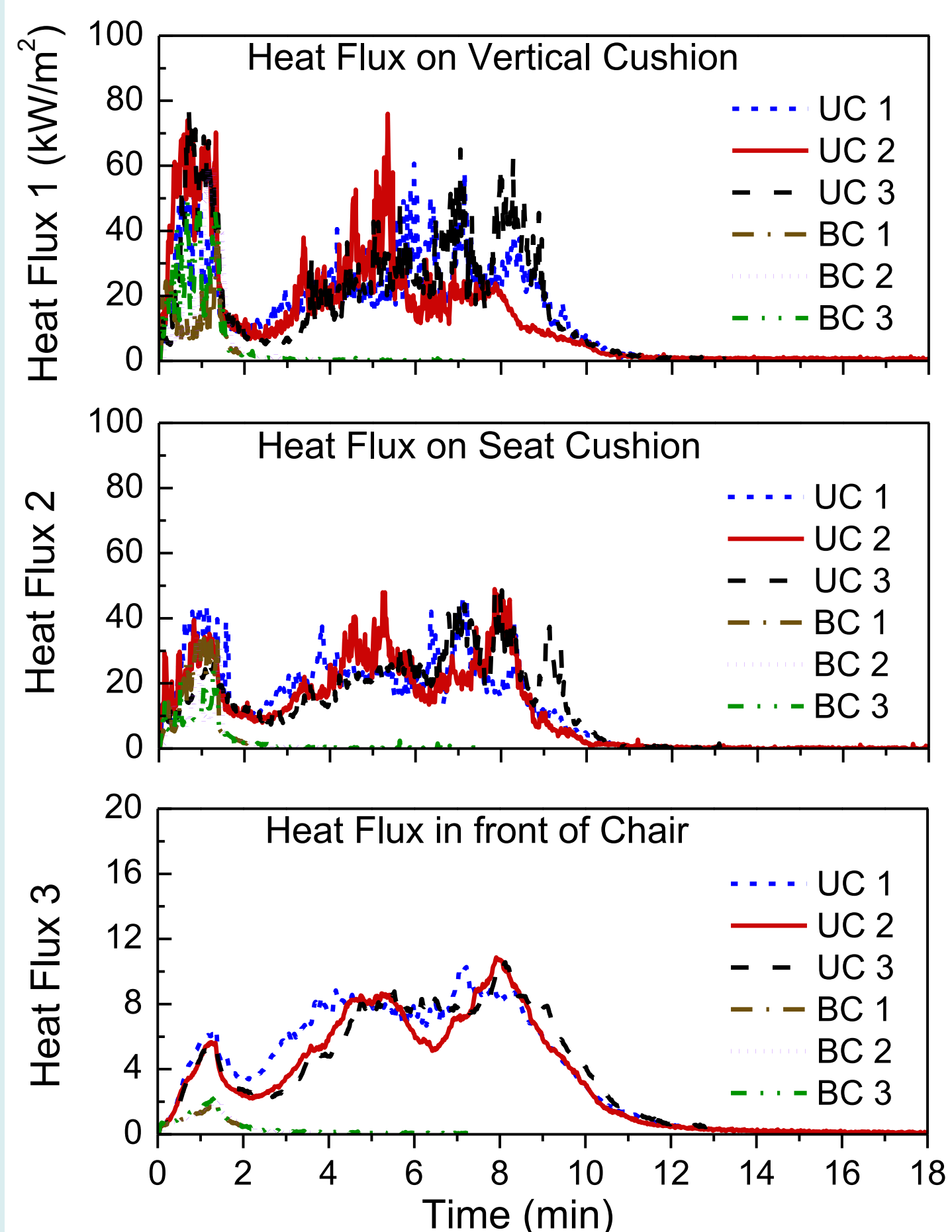
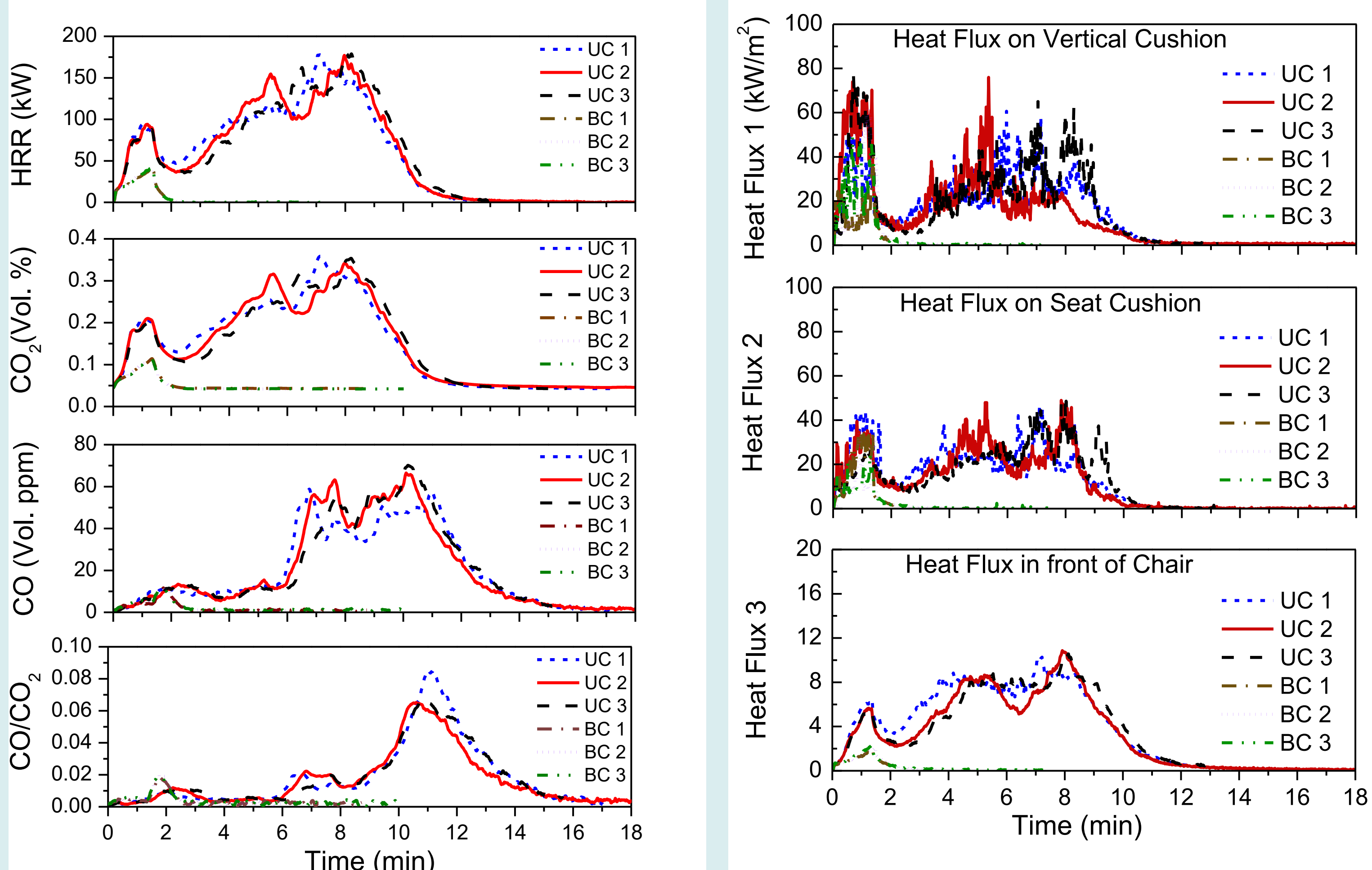
Sample	Backcoating formulation	Area density [g/m ²]	Thickness [mm]	Flexural rigidity [μJ]
UC fabric	no backcoating	447.3 ± 2.7	1.3 ± 0.2	81 ± 4
BC fabric	vinyl-silane modified aluminum hydroxide	813.3 ± 15.9	1.5 ± 0.3	287 ± 57

- Foam: Cal TB 117-2013 polyurethane
- Fabrics: 100% cotton velvet (UC)
- Backcoating (BC) [1] : halogen-free silicone-based elastomer with 65% by mass of vinyl modified ATH (VSAIOH)
- Ignition method:
Propane burner by Cal TB 133 with 18kW for 80 s, 1 inch above seat



Experimental and Results

Open Flame Test on UC and BC Chair Mock-ups



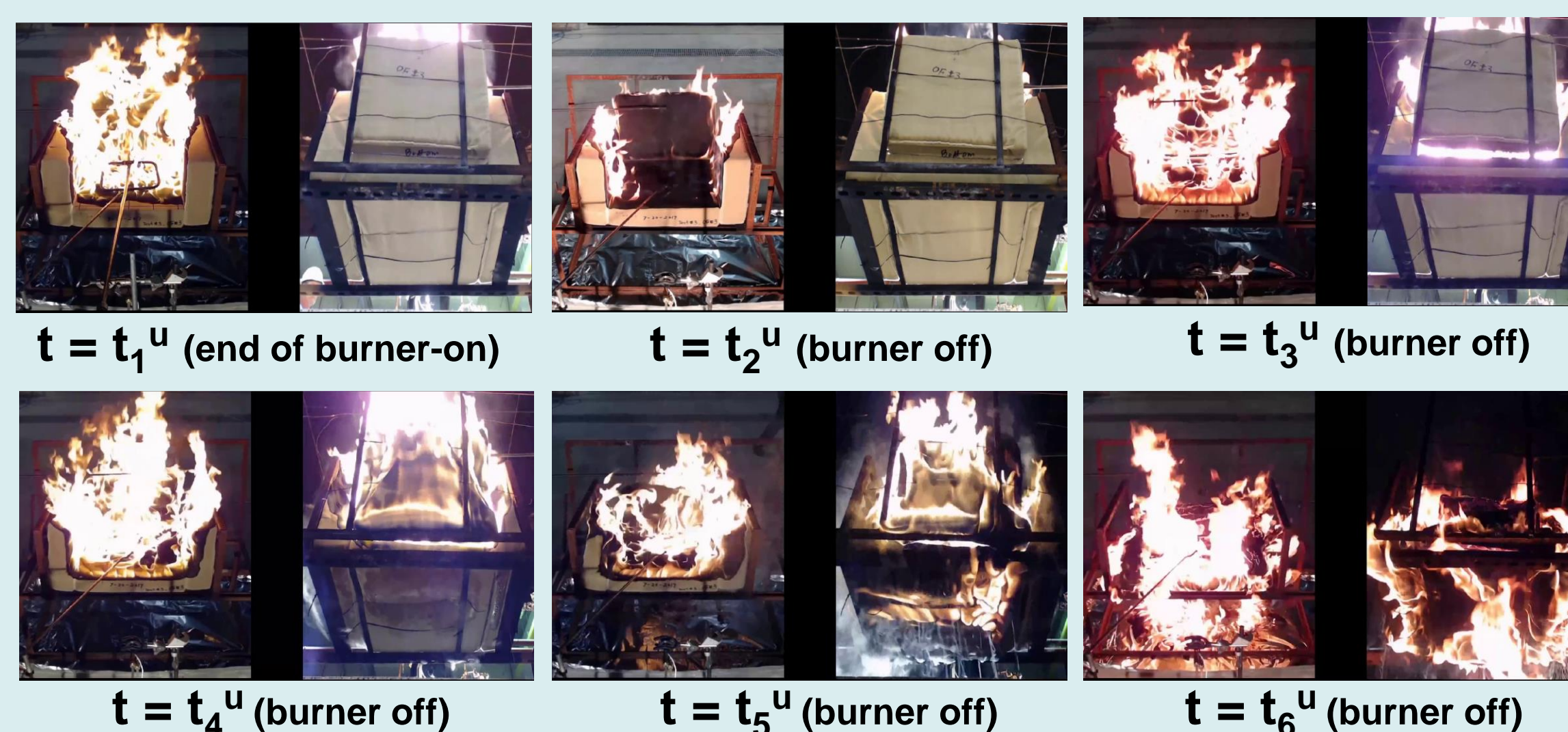
Classified stages with HRR plots of uncoated fabric chair

- Stage 1:** Gas-burner causes combustion of fabrics and TDI of polyurethane (for 80 s)
- Stage 2:** Flame spreads and more polyol occurs
- Stage 3:** Mockup has collapsed into a pool of flaming pyrolysis products

BC technology results in extraordinary reduction of flammability. BC chairs have PHRR and THR as low as 13.5 % and 2.2 % of UC chairs, respectively. Heat flux values up to about 70 kW/m² are measured.

Chair Fabric	Stage I				Stage II				Stage III				Total		
	PHRR _i [kW]	THR _i [MJ]	ML _i [Kg]	eff H _{c,i} [kJ/g]	PHRR _{ii} [kW]	THR _{ii} [MJ]	ML _{ii} [Kg]	eff H _{c,ii} [kJ/g]	PHRR _{iii} [kW]	THR _{iii} [MJ]	ML _{iii} [Kg]	eff H _{c,iii} [kJ/g]	THR [MJ]	TML [Kg]	eff H _{c,tot} [kJ/g]
UC Fabric	73.8 ± 3.5	6.2 ± 0.3	0.41 ± 0.00	15.3 ± 0.7	145 ± 24.0	24.1 ± 3.5	1.17 ± 0.18	20.6 ± 0.2	178.8 ± 2.4	28.9 ± 2.9	1.11 ± 0.15	26.1 ± 1.0	59.2 ± 0.7	2.69 ± 0.03	22.6 ± 0.1
BC Fabric	24.2 ± 0.8	1.3 ± 0.1	0.15 ± 0.00	8.3 ± 0.5									1.3 ± 0.1	0.15 ± 0.00	8.3 ± 0.5

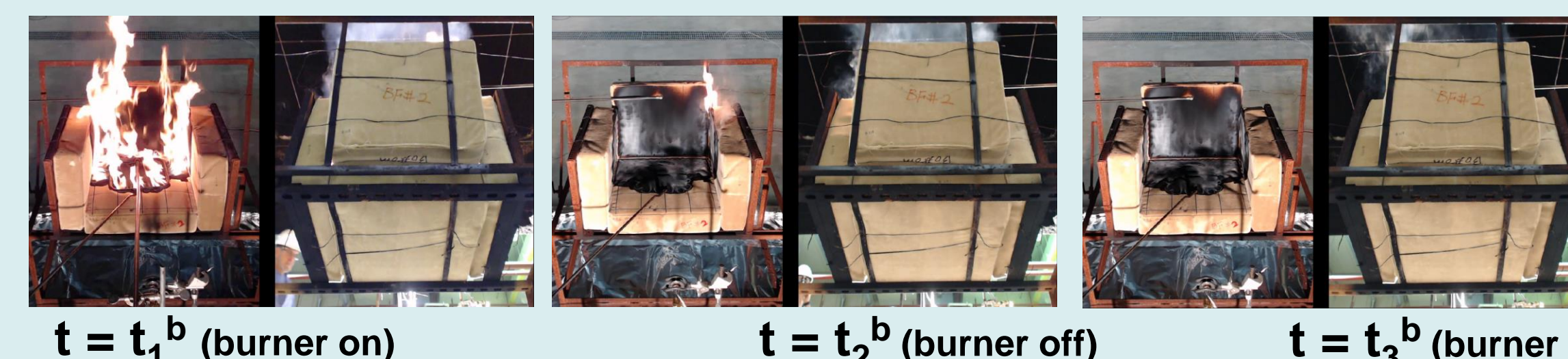
Uncoated (UC) fabric Chair



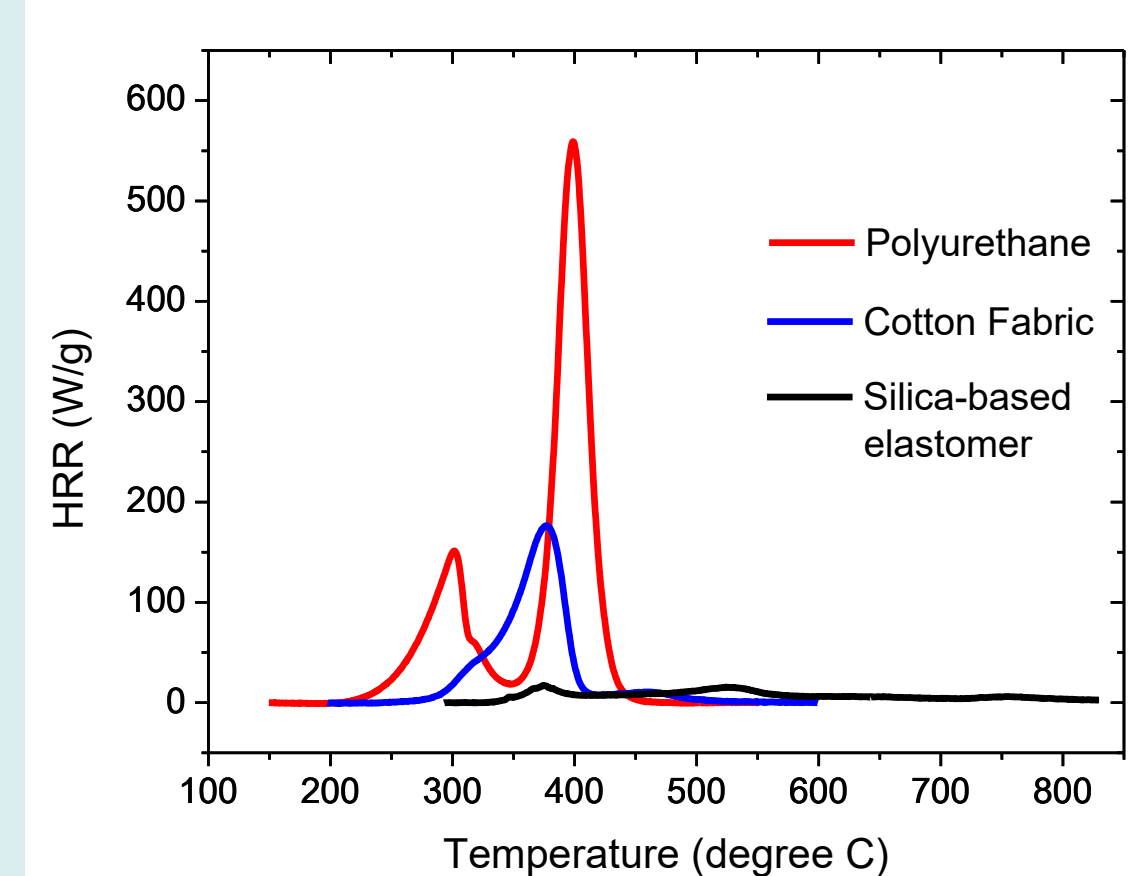
UC mock-ups were fully burn by the end of test. (Left)

On the contrary, in BC mock-ups foam combustion was negligible (see below).

Back-Coated (BC) fabric Chair



Micro-Scale Combustion Calorimetry and Abrasion Resistance Tests



Sample	THR [kJ/g]	PHRR [W/g]
Polyurethane foam	26.1 ± 0.06	555.9 ± 5.65
Velvet (100% cotton) fabric	10.3 ± 0.08	178.0 ± 2.82
Sylgard 65% VSAIOH	3.6 ± 0.44	17.0 ± 0.92

$$k \cdot \text{THR}_{\text{Full-Test}} = \text{THR}_{\text{Cal.}} \quad (\text{Eq. 1})$$

$$\text{eff H}_{c, \text{Full-test}} = \text{THR}_{\text{Full-Test}} / \text{ML}_{\text{Full-Test}} \quad (\text{Eq. 2})$$

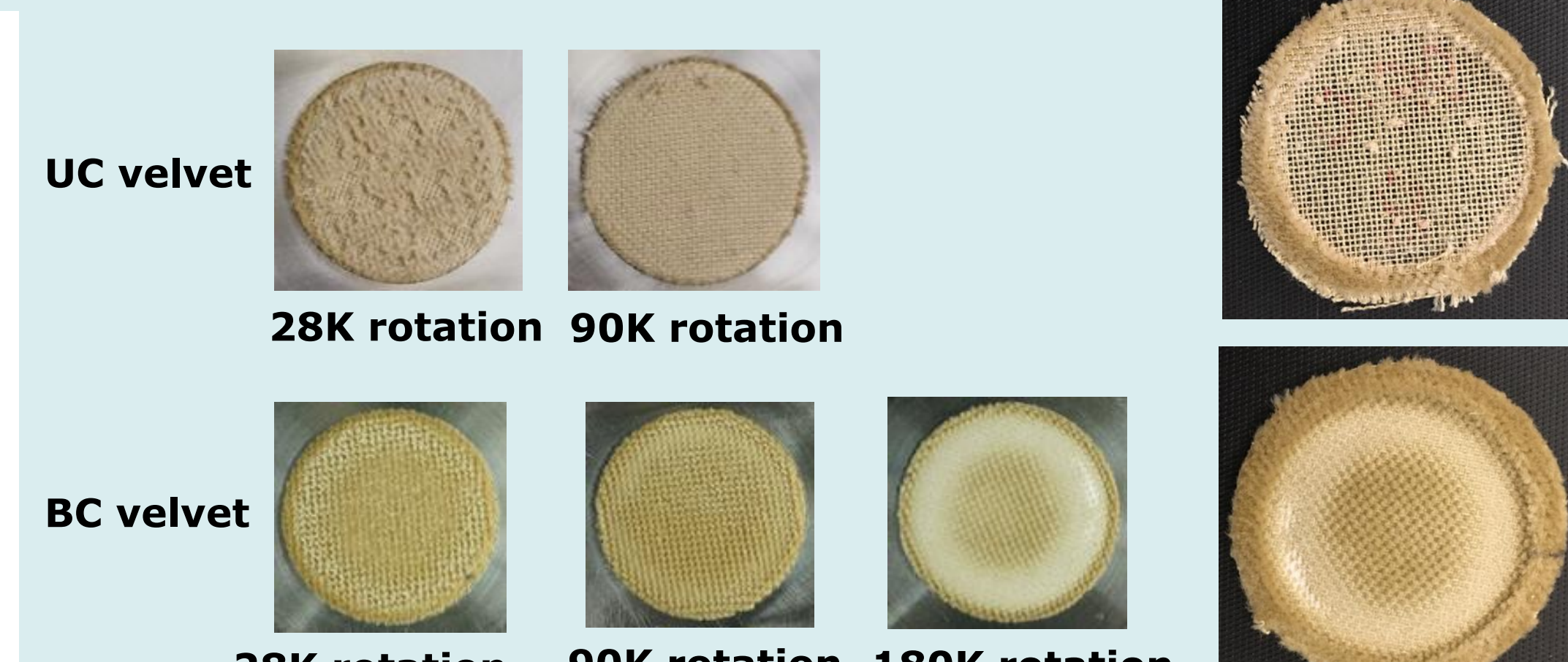
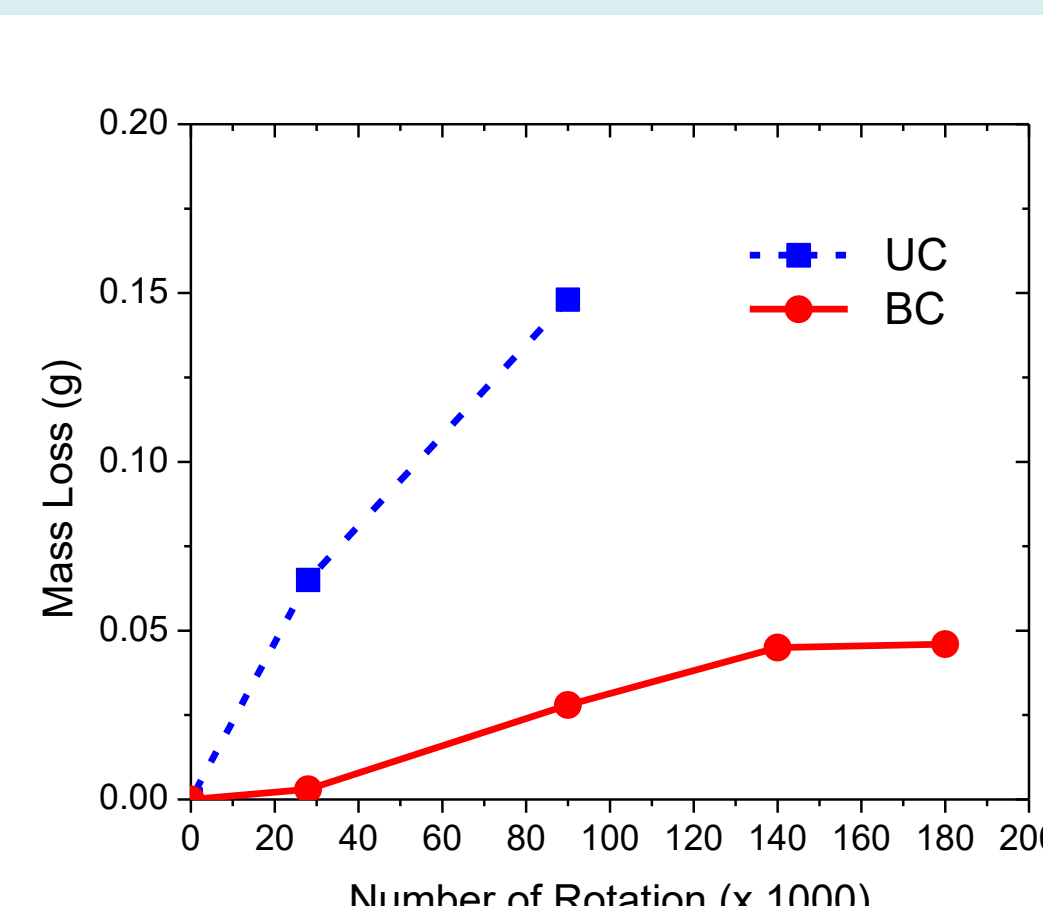
$$\text{THR}_{\text{Cal.}} = \text{ML}_{\text{PUF,Full-Test}} \cdot \text{H}_{c, \text{PUF,MCC}} + \text{ML}_{\text{Fabric,Full-Test}} \cdot \text{H}_{c, \text{Fabric,MCC}} \quad (\text{Eq. 3})$$

Factor $k \approx 0.999 \pm 0.006$ for UC fabric chair

References

- [1] M. Zammarano et al., Adv Mater Interfaces 3(23) (2016).
- [2] California TB 133 Flammability Test Procedure, Department of Consumer Affairs, Bureau of Home Furnishings and Thermal Insulation, North Highlands, CA, 1991.

Abrasion resistance test by Martindale abrasion tester



Conclusion

The results show that the BC fabric allows to achieve an unusual all-in-one solution for flaming and smoldering combustion that improves durability without affecting the aesthetics or the comfort of the chair.