

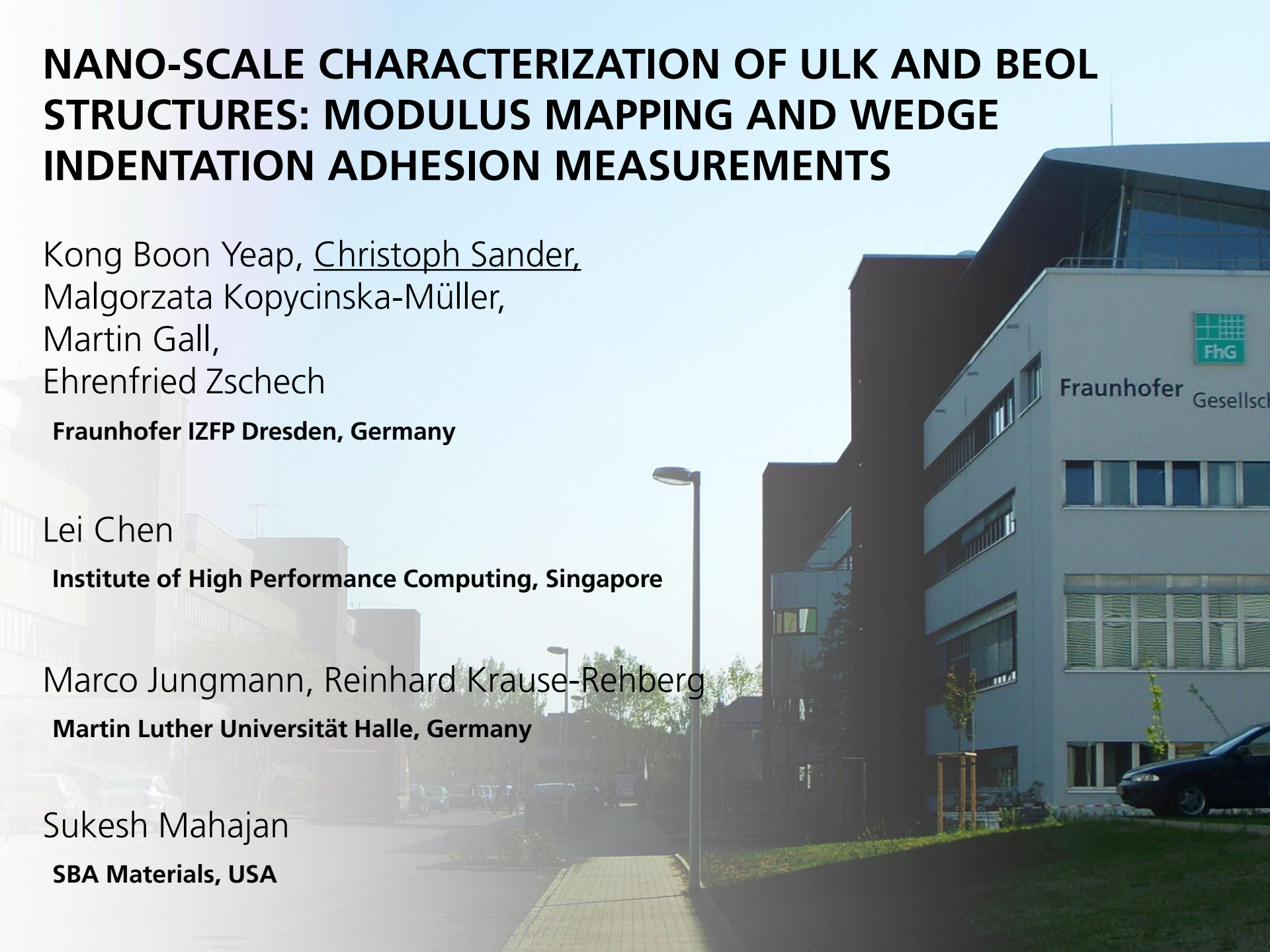
NANO-SCALE CHARACTERIZATION OF ULK AND BEOL STRUCTURES: MODULUS MAPPING AND WEDGE INDENTATION ADHESION MEASUREMENTS

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- Motivation
- Nanoindentation and FE simulation on **different pore topology** of OSG (organosilicate glass)
- Measurement of the effective **CTE** of BEoL structure
- Wedge-Indentation on **SA-OSG** (self-assembled OSG)
- Conclusion

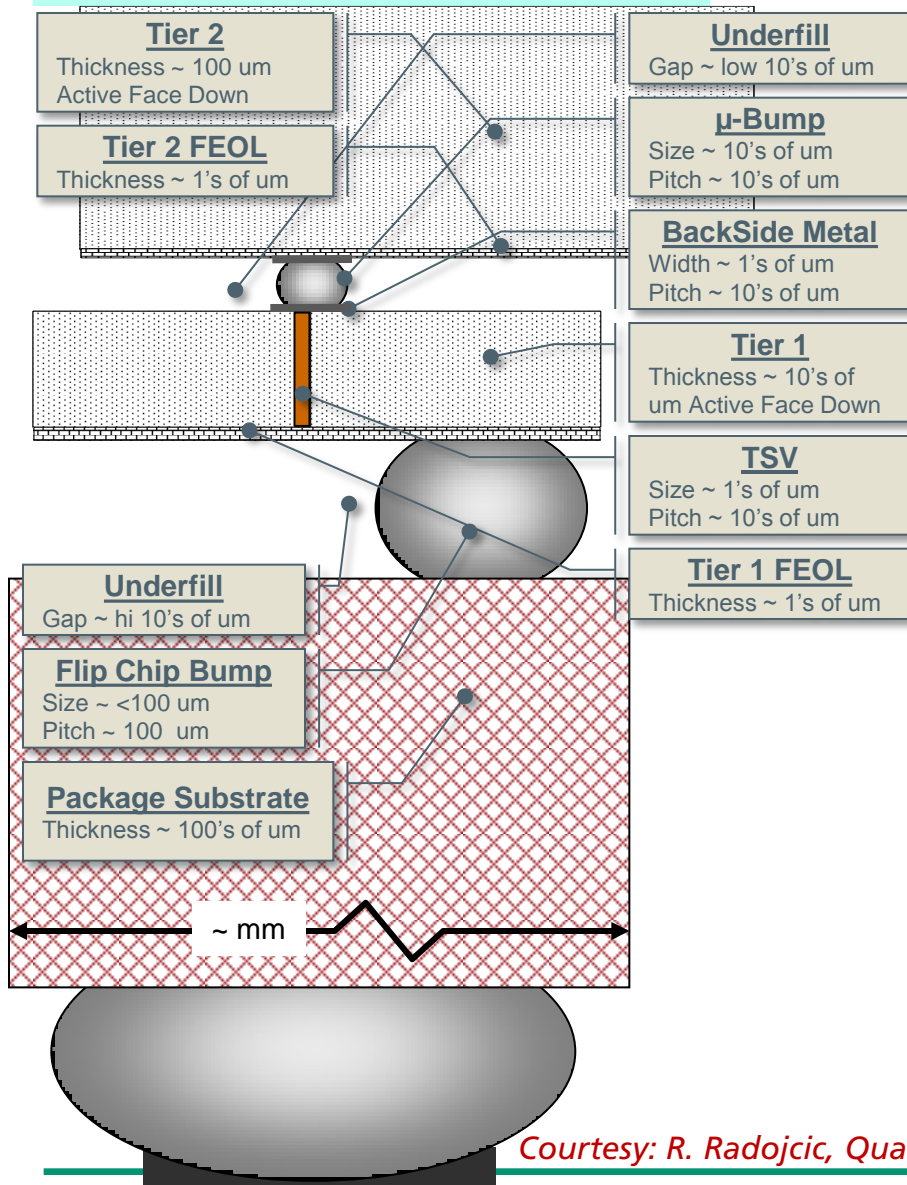


multi-scale database

MOTIVATION



3D TSV scheme



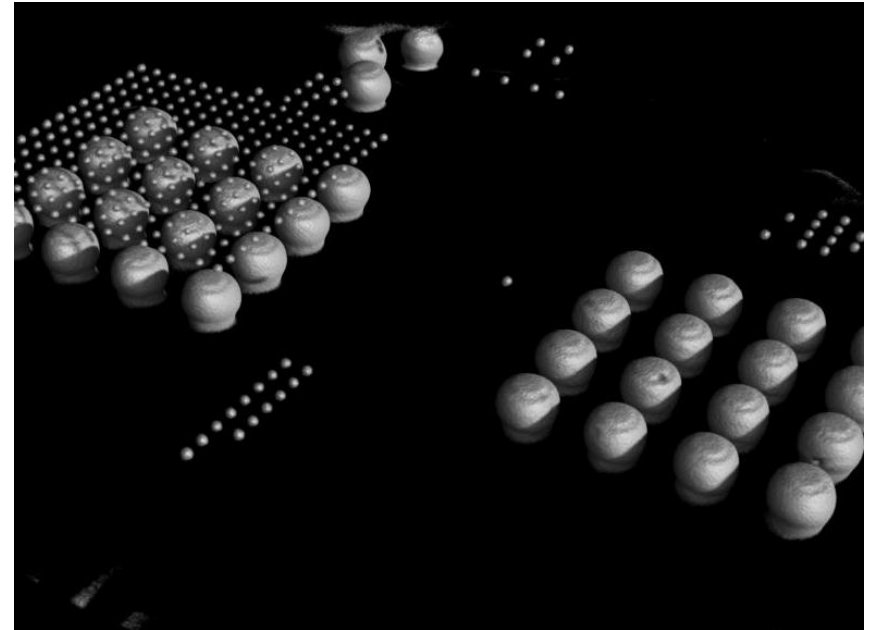
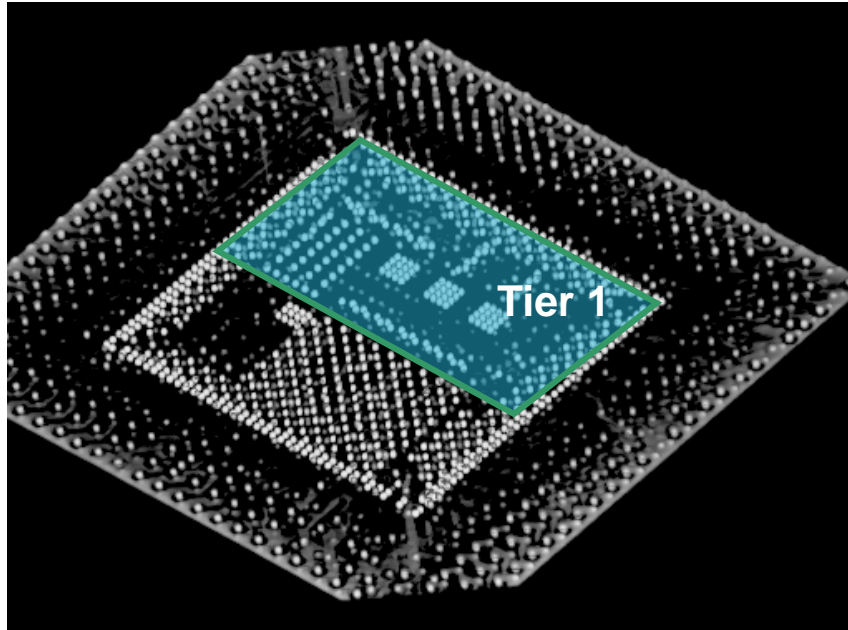
Courtesy: R. Radojic, Qualcomm

Integrated Heterogeneous 2-Die Stack

- Tier 1 : CMOS Logic SoC
 - TSV (connect frontside to backside)
 - Very thin Wafer (manage TSV aspect ratio)
 - Active face down incl. BEOl
- Interface μ-Bump
 - Backside RDL Metal (interface to μ-Bump and/or routing to allow offset of μ-Bump vs TSV)
 - μ-Bump (Tier to Tier interconnect)
 - Very thin underfill
- Tier 2 : Commercial Die
 - Memory or Analog die, or...
 - Frontside Metal (interface to μ-Bump)
 - Active face down & Pretty Thin
- Flip Chip (C4) Bump
 - Regular flip chip bump
 - Regular underfill
- Package
 - Regular PCB substrate
 - Regular plastic molding
 - Regular Package BGA Bump



Studied 3D IC



Micro-XCT Courtesy: Peter Krüger

- Young's modulus – Nanoindentation
- CTE – Coefficient of Thermal Expansion
- Adhesion of Ultra Low K on Silicon – Wedge Indentation



Stress engineering in 3D IC structures: Need of database and input for database: Multi-scale materials data

Stress-related phenomena caused by 3D TSV integration influence:

- chip performance (and variability),
- yield and reliability.

Stress management in complex systems requires:

- multi-scale modeling, including accurate MULTI-SCALE MATERIALS DATA
- Input data for simulation
- Model validation (and calibration)

→ **Multi-scale materials database concept** ¹

Multi-scale Materials Characterization needed

- Multi-scale (thermo-)mechanical materials data
-

Young's Modulus

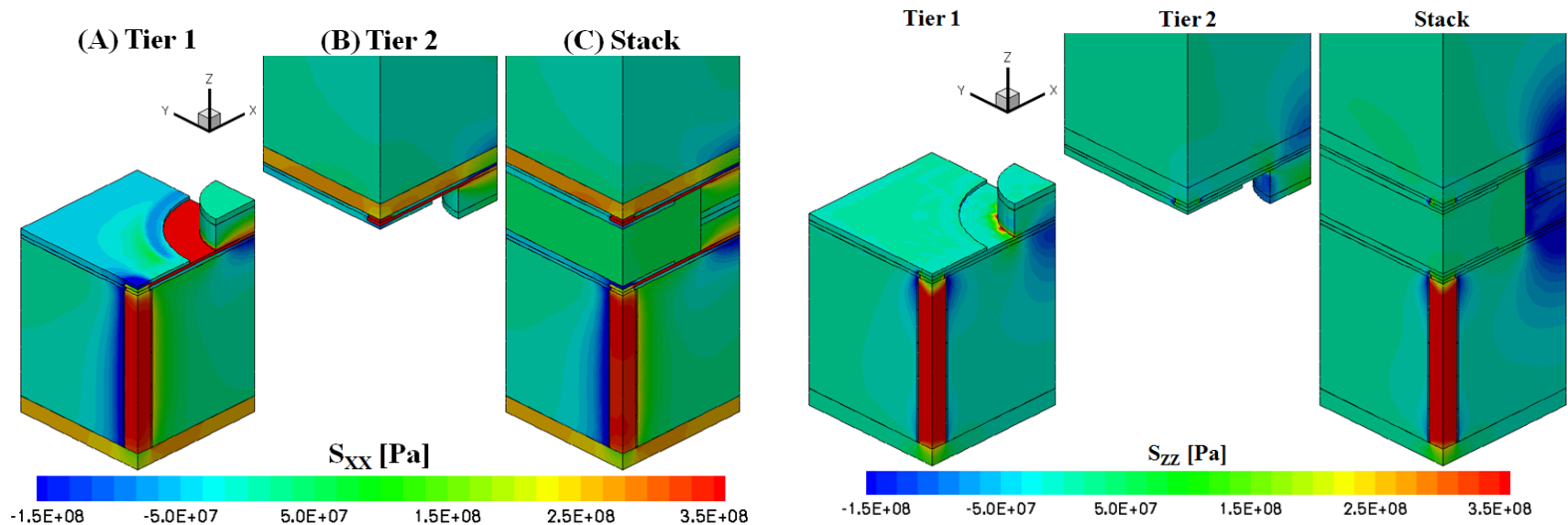
NANO-INDENTATION TECHNIQUE



Motivation

Relations between mechanical properties and structure at micro- and nano-scale:

- Optimum pore/molecular structure (CPI and dielectric reliability)
- Enable a physics-based IC design

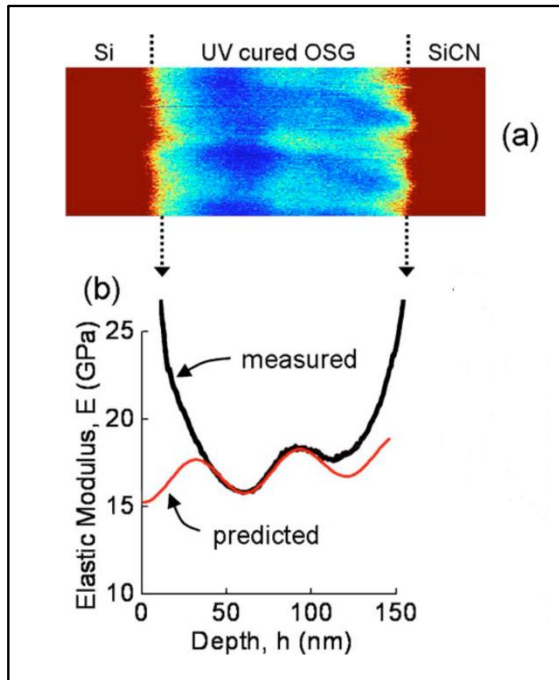


Courtesy of Xiaopeng Xu, Synopsys Inc.

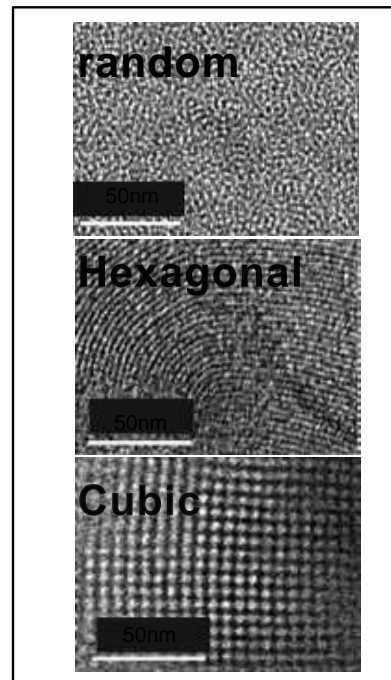


Introduction

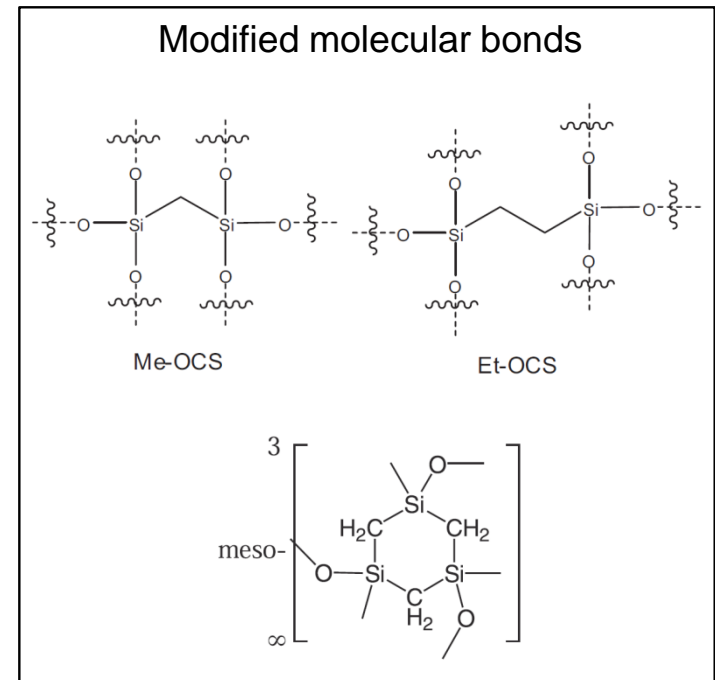
Dielectric constant below 2.0 and sufficient mechanical integrity:
-> ULK materials are tailored at multiple scales.



Scale: 100nm



10nm



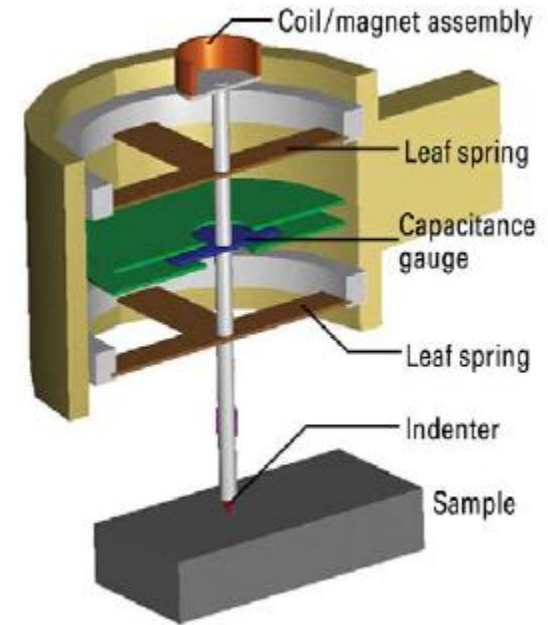
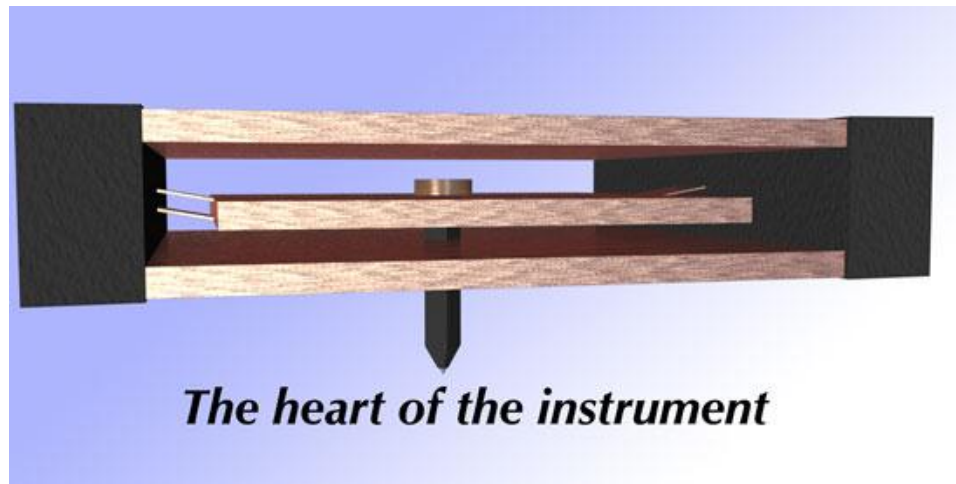
Molecular and atomic

Characterization of the multiscale properties – structure relationship

Kim et al. APL, Fan et al. Nat.Mater., Dubois et al. Adv.Mater., Landskorn et al. Science



Indenting at Micro/Nano-scale

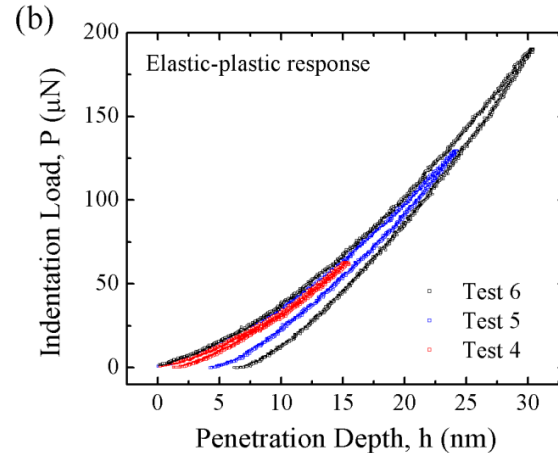
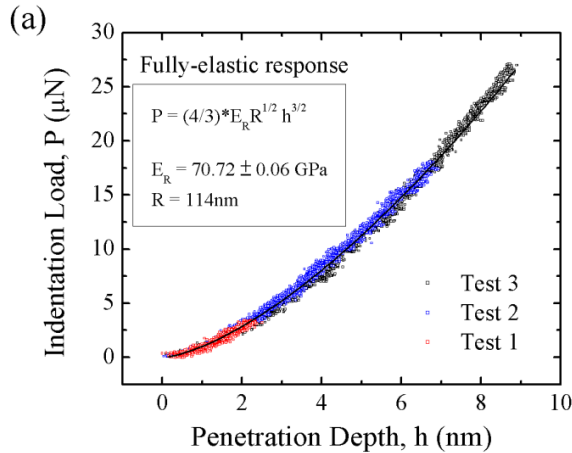


- The heart of a Nanoindentation system lies in the actuator and sensors mechanism
- Capacitive or Electrostatic Force Actuation and Depth Sensing
- Best machine performance: FORCE $\sim 30\text{nN}$, DISPLACEMENT $\sim 0.1\text{nm}$

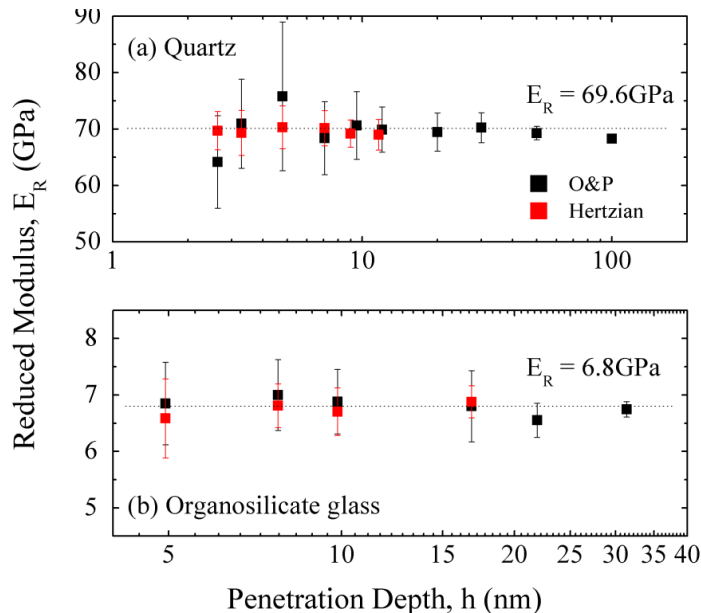
Courtesy of Hysitron Inc. and Agilent Technologies



High resolution nanomechanical testing



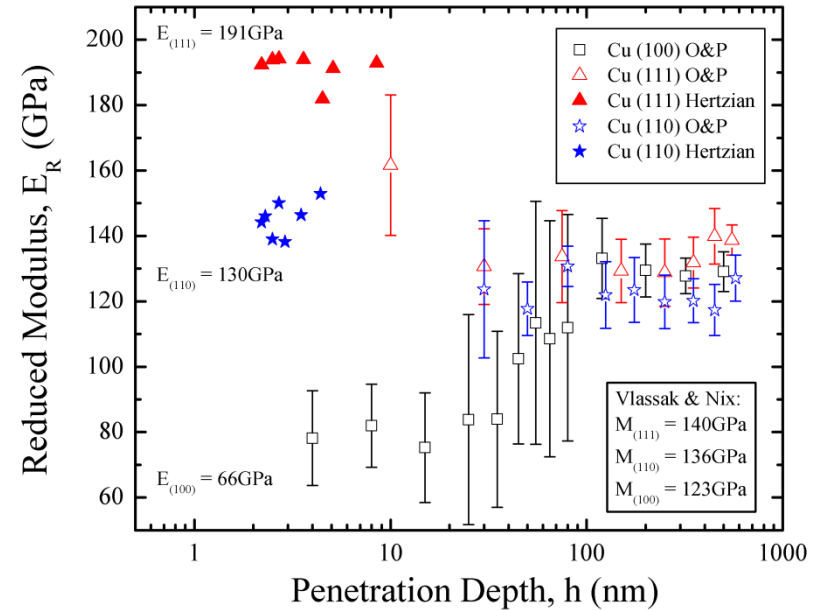
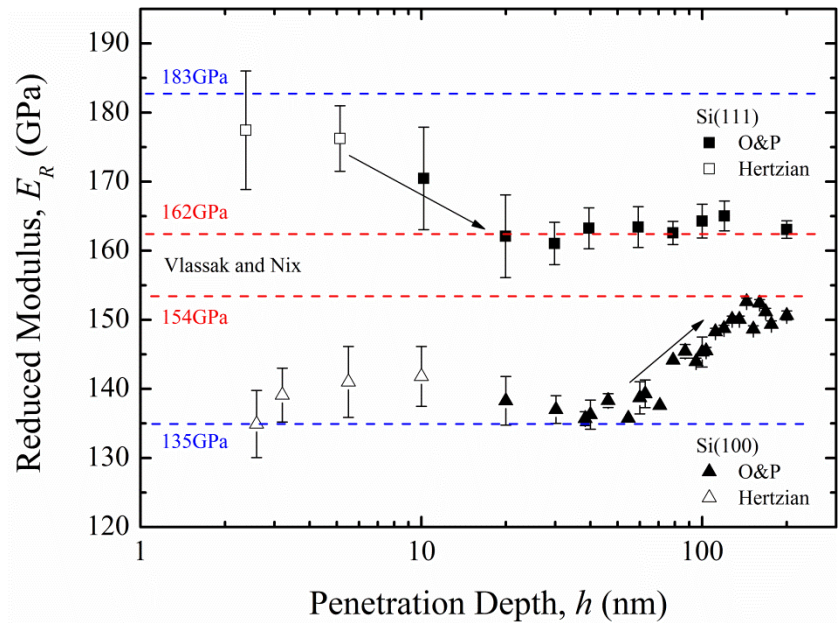
Load-displacement data at single nanometer scale



- Displacement length scale similar to the nanostructure of interest
- Nanoscale structure-property relation



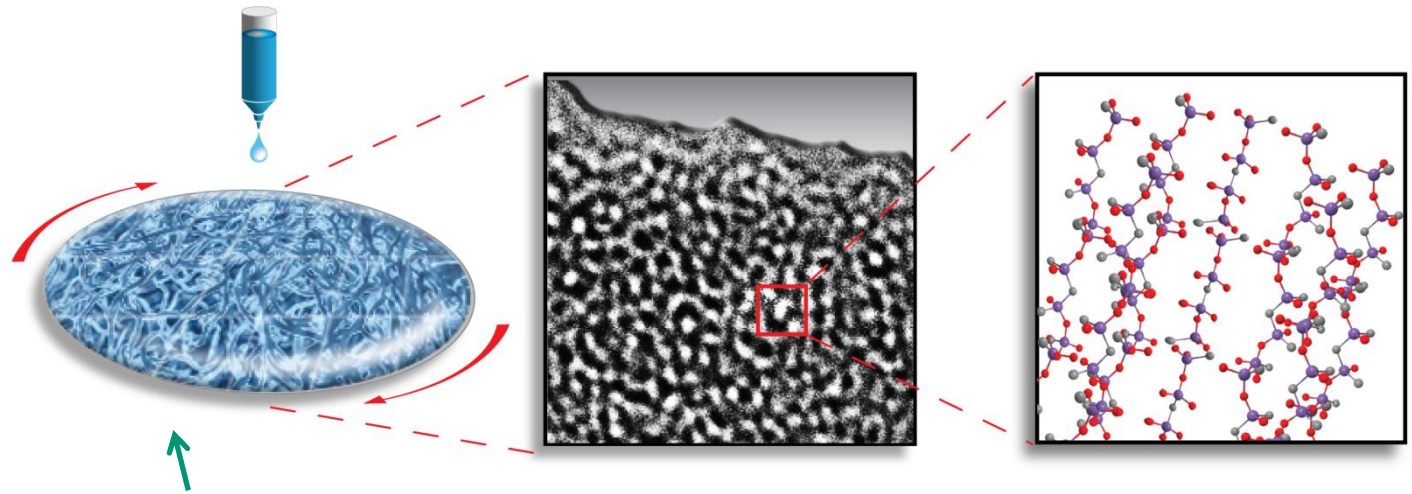
High resolution nanomechanical testing



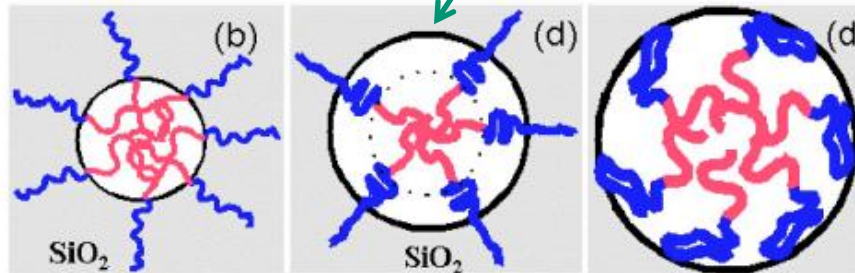
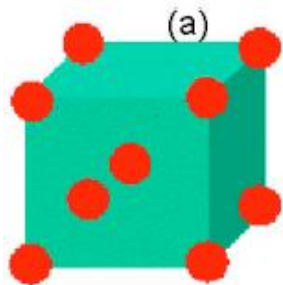
- Small indentation captures more of the structure-related properties
- Large indentation gives average properties
- Elastic-anisotropy is observed if $h < 10$ nm



Self assembly sol-gel template process



Spin coating + self assembly process



Triblock co-polymer, removed by thermal or UV curing

Evaporation and silanol condensation →

Courtesy: SBA Materials



OSG with different pore topology

Sample description and experimental results for SA-OSG and CVD-OSG films.

| Sample | Target k | Actual k | Porosity, p (%) | Thickness (nm) | Elastic Modulus, E (GPa) | Cure process |
|----------|---------------|---------------|----------------------|-------------------|----------------------------------|--------------|
| SA-OSG1 | 1.8 | 1.80 | 49 | 600 | 3.1 ± 0.1 | Thermal |
| SA-OSG2 | 2.0 | 2.08 | 42 | 650 | 3.8 ± 0.2 | Thermal |
| SA-OSG3 | 2.2 | 2.21 | 30 | 716 | 5.5 ± 0.3 | Thermal |
| SA-OSG4 | 2.2 | 2.25 | 31 | 620 | 6.5 ± 0.3 | Thermal |
| SA-OSG5 | 2.4 | 2.37 | 27 | 627 | 6.9 ± 0.4 | Thermal |
| SA-OSG6 | 2.4 | 2.41 | 24 | 693 | 7.3 ± 0.3 | Thermal |
| CVD-OSG1 | 2.4 | N.A. | 25 | 530 | 3.7 ± 0.3 | UV & Thermal |
| CVD-OSG2 | 2.7 | N.A. | 12 | 660 | 6.6 ± 0.7 | Thermal |
| CVD-OSG3 | 3.0 | N.A. | 0 | 520 | 13.0 ± 1.2 | Thermal |

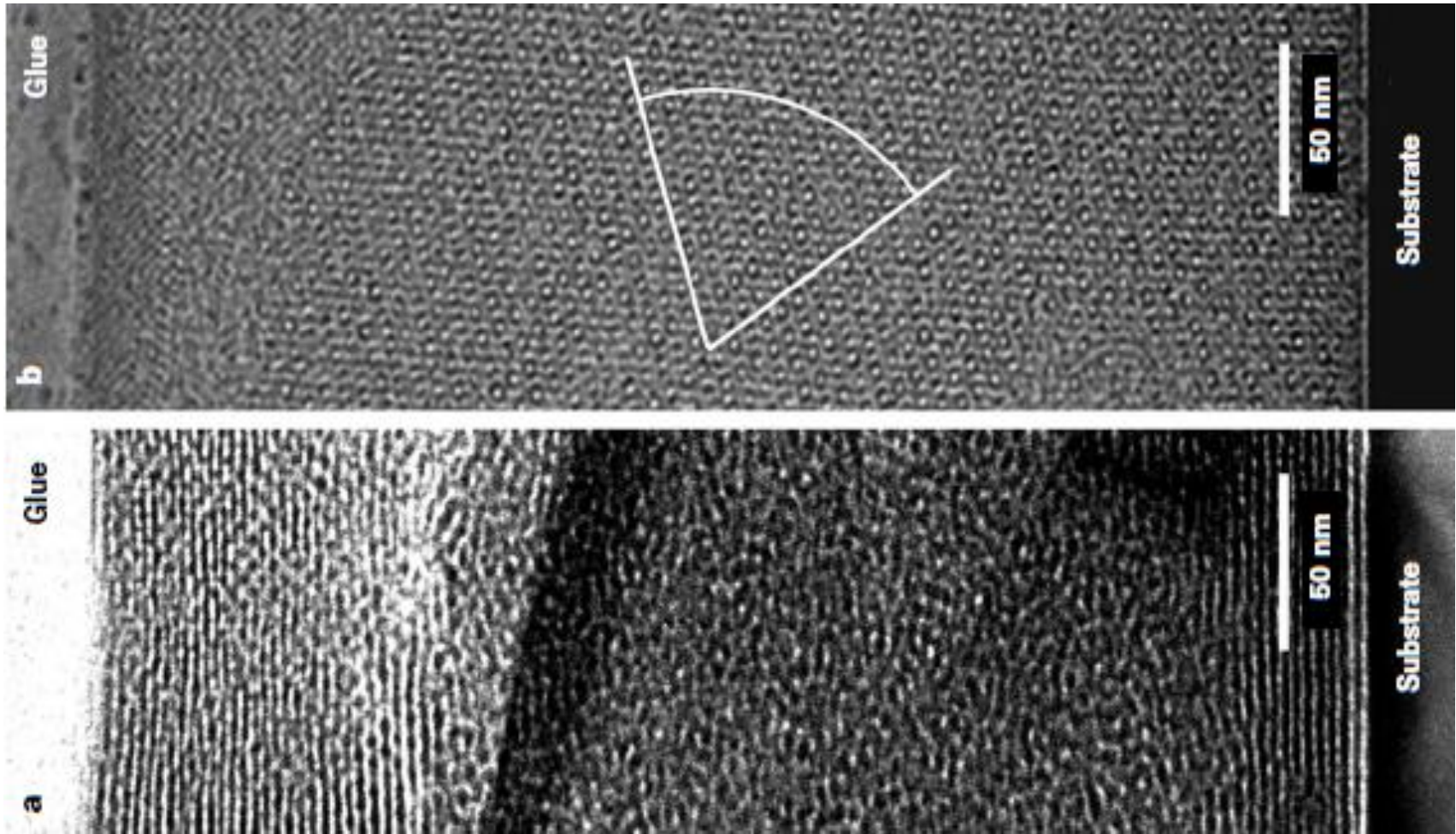
Self-assembled organosilicate glass (**SA-OSG**)

Chemical vapor deposited organosilicate glass (**CVD-OSG**)



OSG with different pore topology

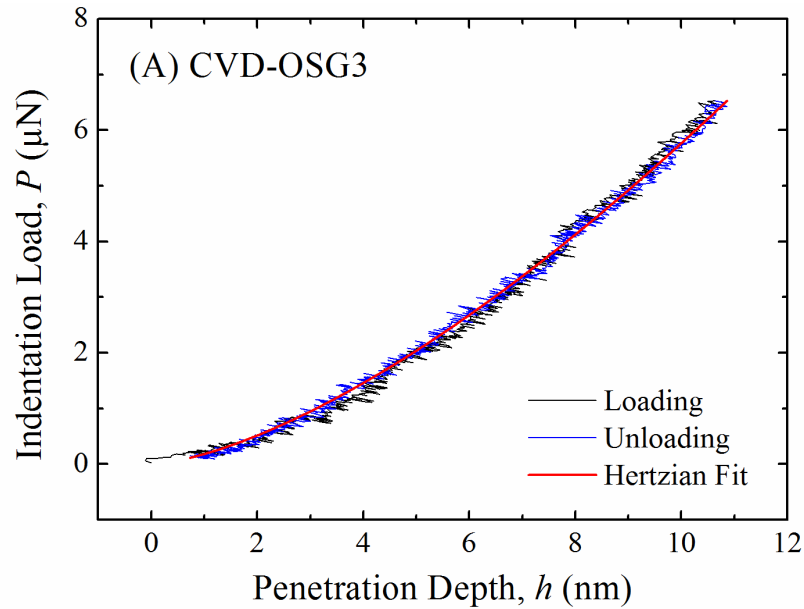
Pore arrangement: random vs. ordered domains



Lu et al. Nature, Maex et al. JAP, Smirnov et al. JJAP



Elastic deformation of CVD-OSG at nanoscale



CVD-OSG

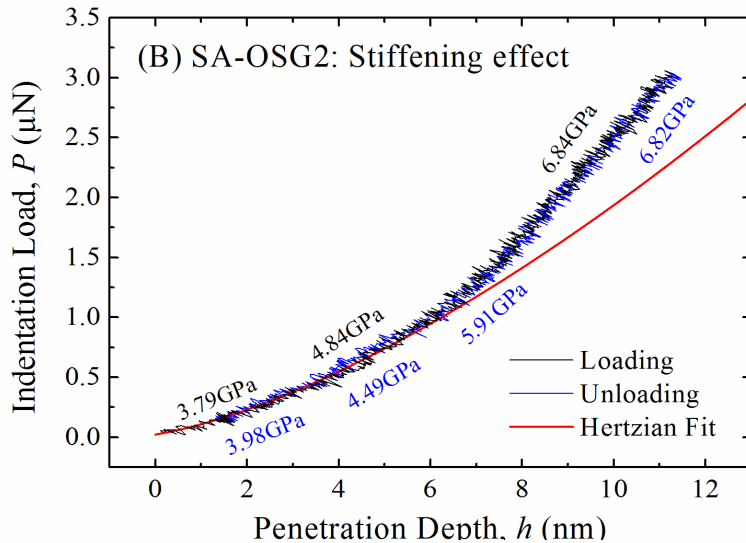
- Fully elastic
- Fit well with Hertz model

$$P = \left(\frac{4}{3\pi} \right) E_r R^{0.5} (h - h_0)^{1.5}$$

- Similar to isotropic material
- Consistent for dense or porous CVD-OSG

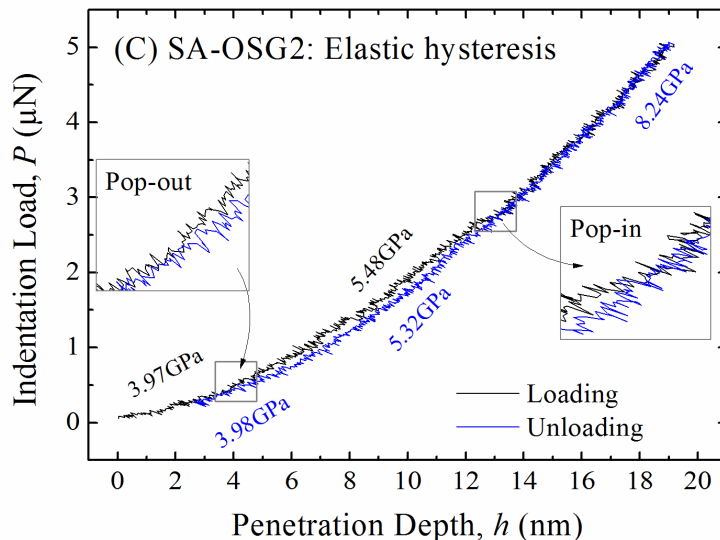


Elastic deformation of SA-OSG at nanoscale (42% porosity)

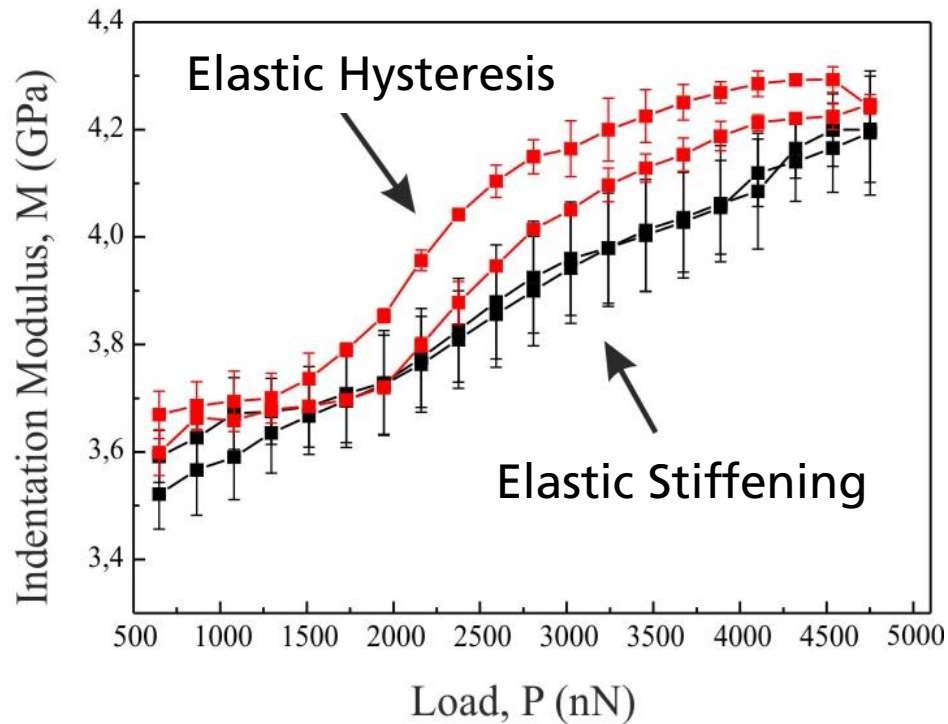


SA-OSG

- Stiffening effect, 4GPa to 7GPa
- Hertz model fits: Initial 3nm of the P-h curve
- 1 out of 4 indentation locations show “elastic hysteresis”
- Pop-in at 13nm of loading curve
- Pop-out at 4nm of unloading curve.
- Match again below 4nm



Elastic deformation of SA-OSG at nanoscale (42% porosity)



High-frequency dynamic mechanical test:

Atomic-force-acoustic-microscopy (AFAM)

Modulus values resolved at $P=1\mu\text{N}$ to $5\mu\text{N}$:

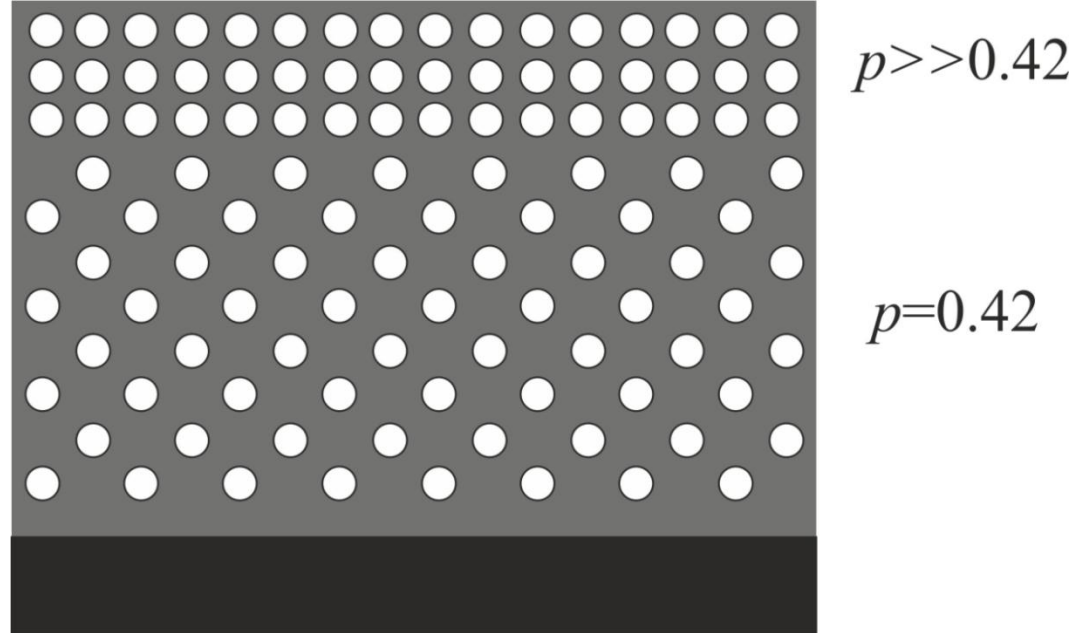
- Stiffening effect
- Elastic hysteresis

Deformation mechanism?

- **Elastic stiffening:** pore concentration gradient, topography, or nanocavity strengthening.
- **Hysteresis:** wall-bending or -buckling



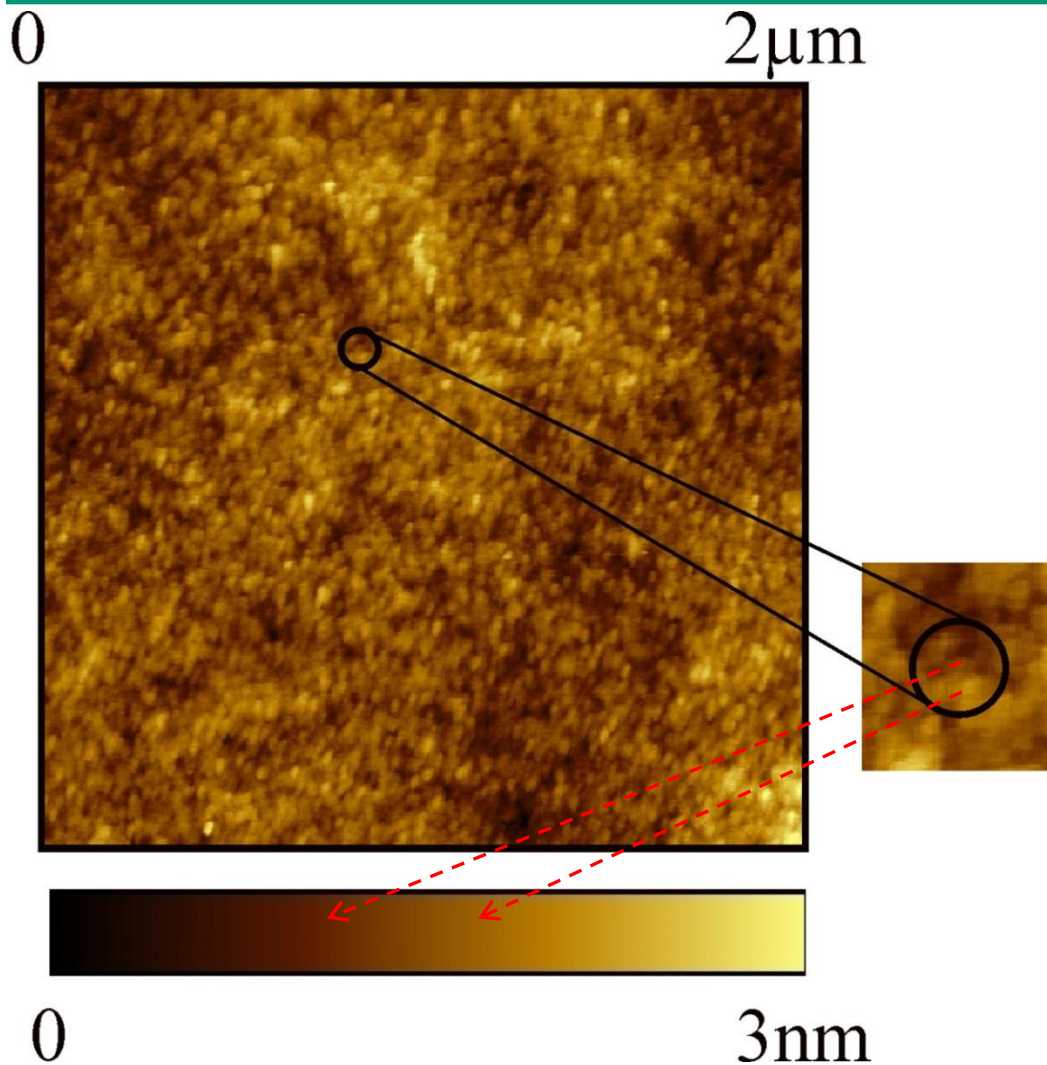
Elastic stiffening: Pore concentration gradient



- Pore concentration gradient
- Top layer: porosity $\gg 0.42$, thickness $\ll 3\text{nm}$ thick, $E \ll 1\text{GPa}$
- Bottom layer: porosity $= 0.42$, thickness $= 500\text{nm}$, $E > 10\text{GPa}$
- Porous structure exceeds the Hashin-Shtrikman upper bound
- Cannot fully account for the observed stiffening effect



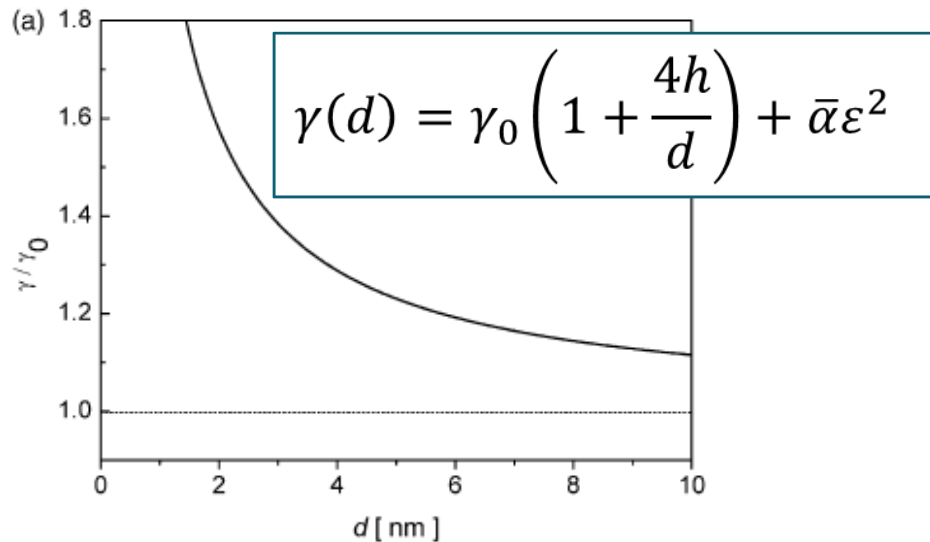
Elastic stiffening: Topography effect



- AFM topographic scan
- No obvious periodicity on the surface
- Indentation contact radius is about 50 nm
- Surface roughness within one indentation contact area < 1 nm
- **Effect** of topography on indentation data is **small**



Elastic stiffening: Nanocavity strengthening

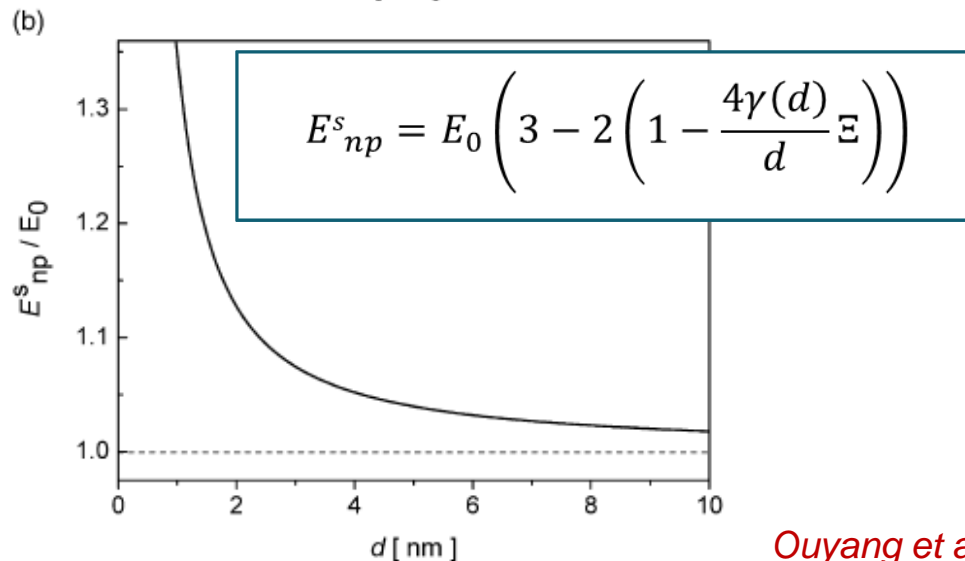


SA-OSG

- Constant pore size, $d=2\text{nm}$
- Elastic stiffening

CVD-OSG

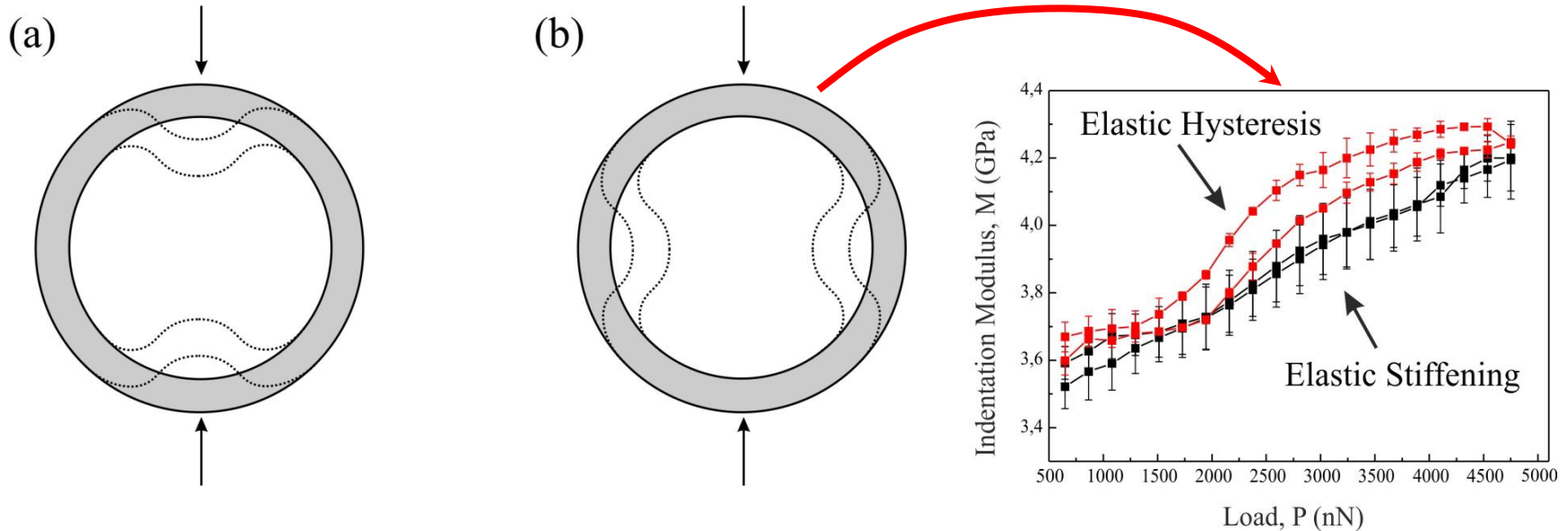
- Broad pore size distribution, 1nm to 10nm
- Constant E



Ouyang et al., Small, Ding et al. JAP.



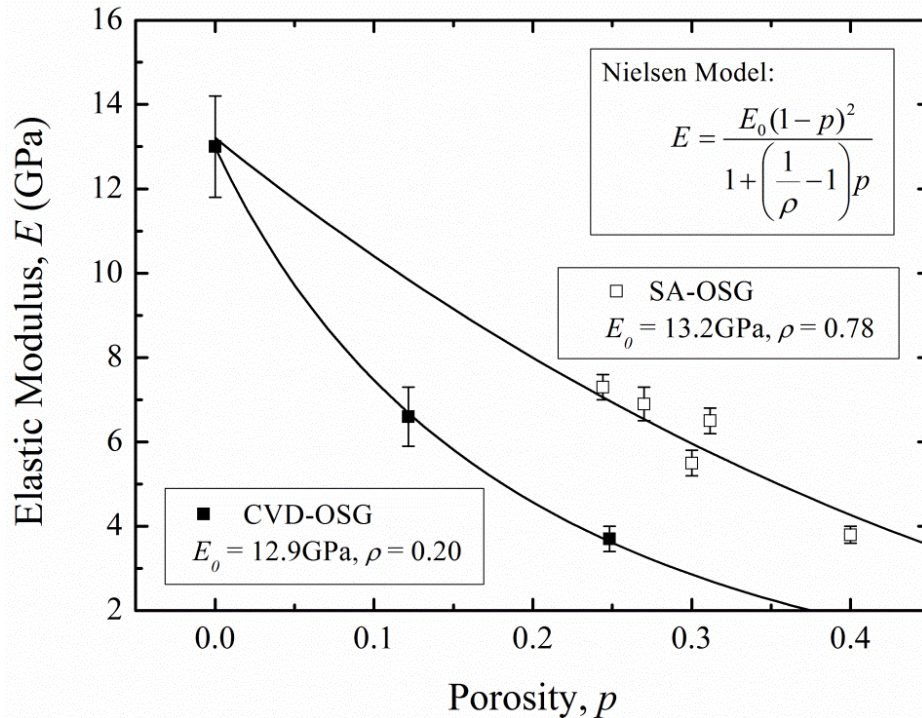
Hysteresis: Pore wall bending and buckling



- Under compressive load: bending or buckling dominated deformation
- Buckling of pore walls – structural instability at critical stress
- For ordered porous structures, buckling of pore walls is possible, depending on the structure orientation
- **Elastic hysteresis** may be related to pore buckling dominated deformation



Topology effect: elastic modulus vs. porosity model

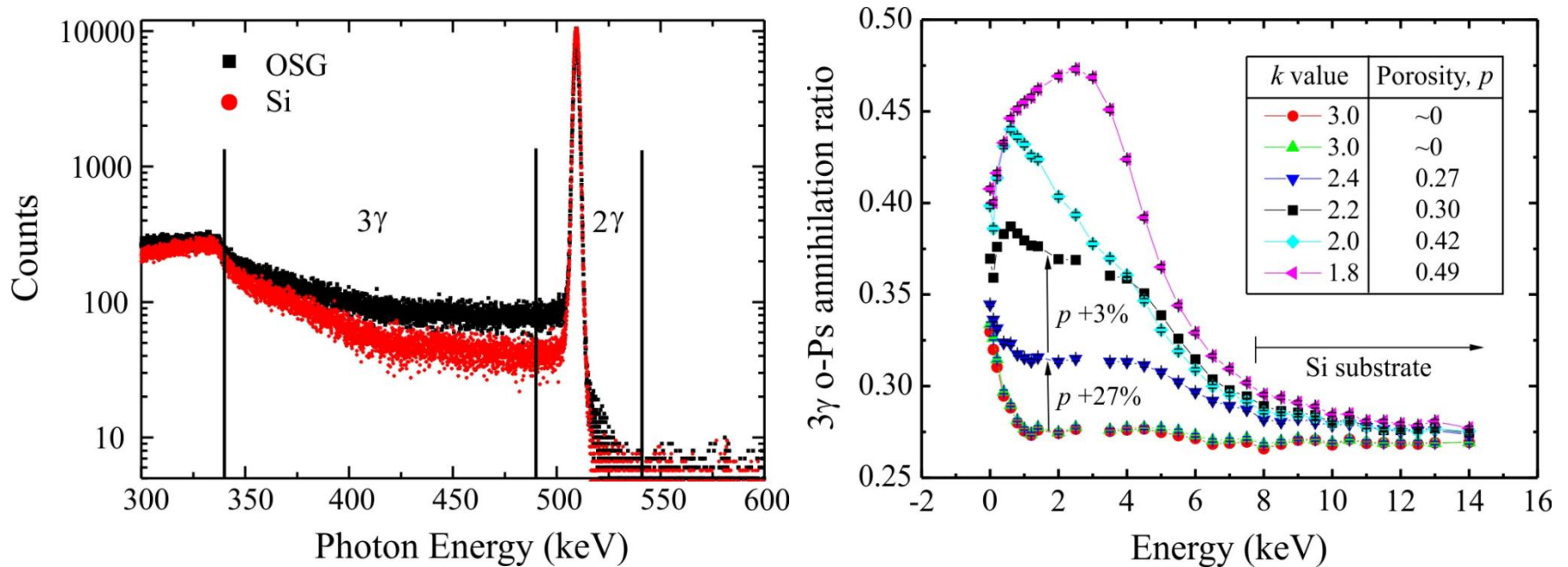


- Mathematical models of E-p relation with one or two variable parameters (n, C for foam model and ρ for Nielsen model)
- The variable parameters are indirectly correlated with the porous structure
- Assuming consistent porous structure

$\rho = 0 - 0.4$ – shell like pores
 $\rho = 0.3 - 0.7$ – dendrites, ribbons
 $\rho = 0.6 - 1.0$ – closed pores



PAS-positron annihilation spectroscopy

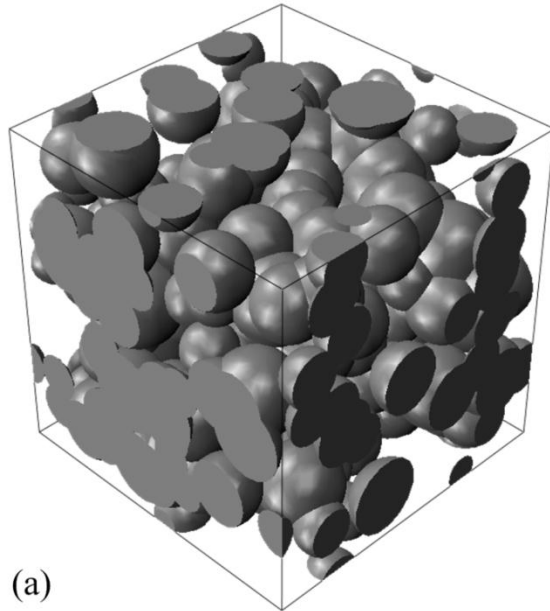


- 3γ o-Ps annihilation ratio is proportional to porosity and pore interconnectivity.
- A step increase of the 3γ ratio, when p is increased only by 3% is a clear indication of pore interconnectivity threshold at $p=0.3$.

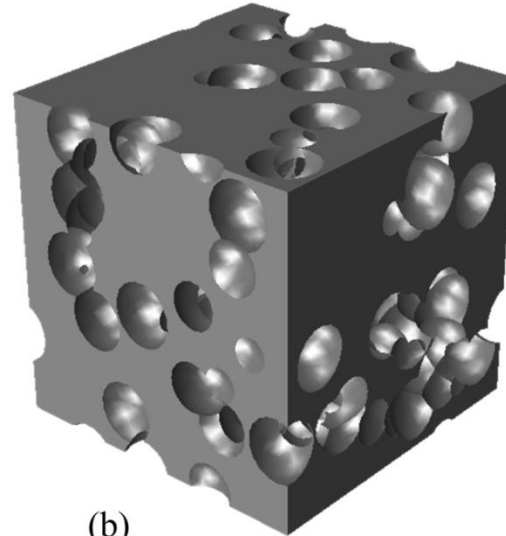


FE simulation of pore topology effect

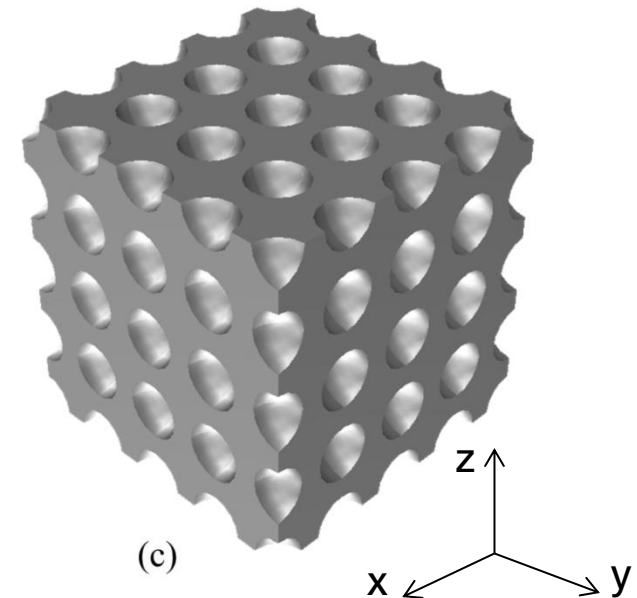
Random overlapping
spherical **solids**



Random overlapping
spherical **pores**



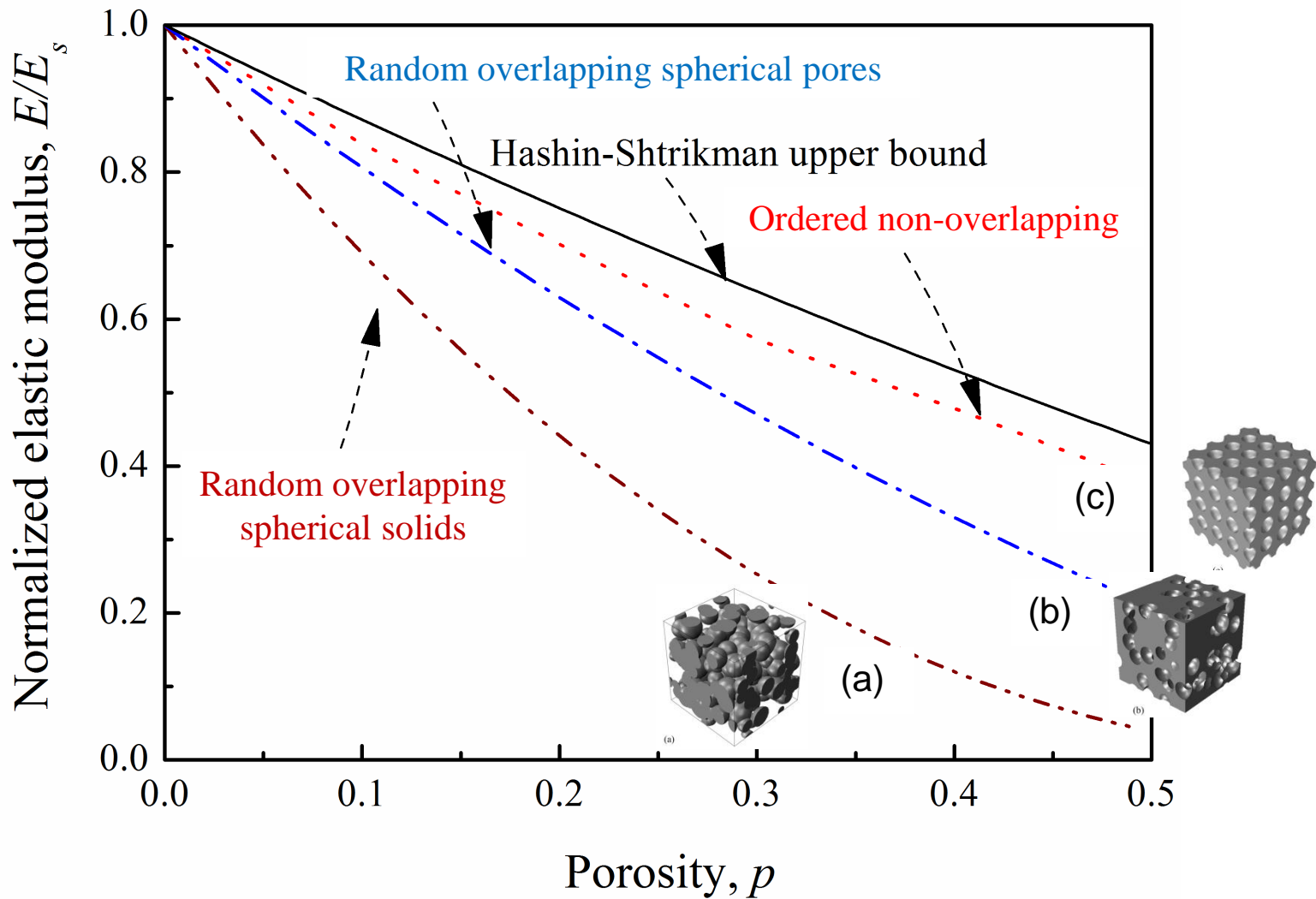
Ordered non-
overlapping



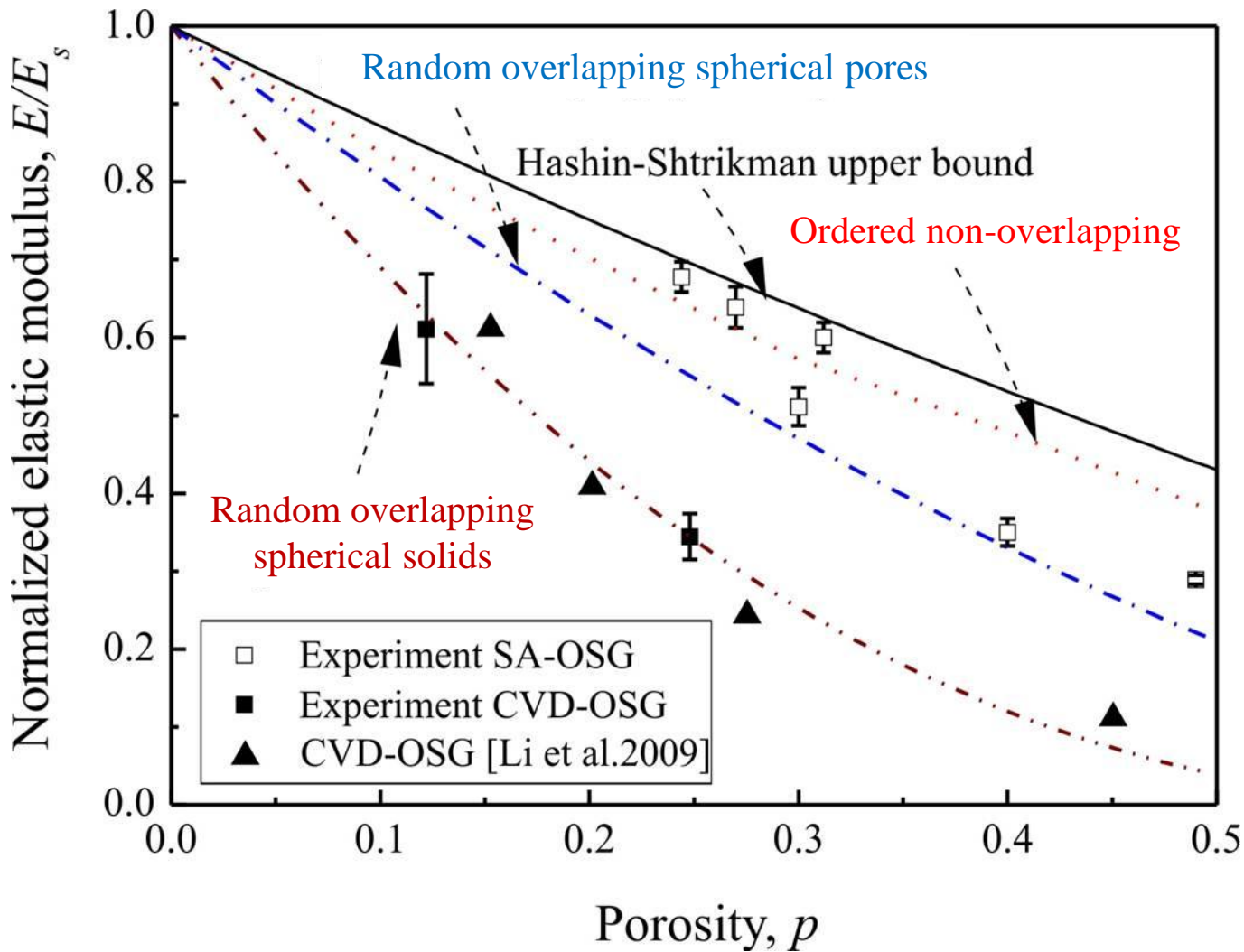
- Homogeneous normal displacement on XY planes, D_z
- Traction-free boundary condition on XZ and YZ planes
- Average stress divided by average strain
- Theoretical threshold value in the FE model is 0.52



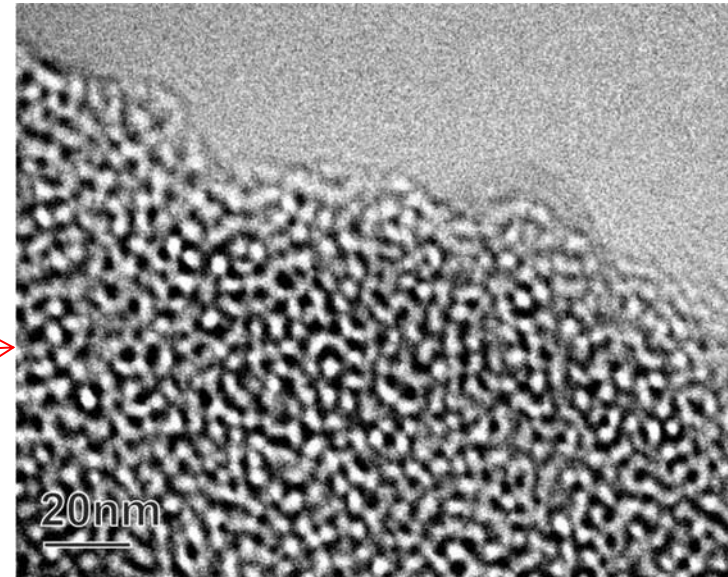
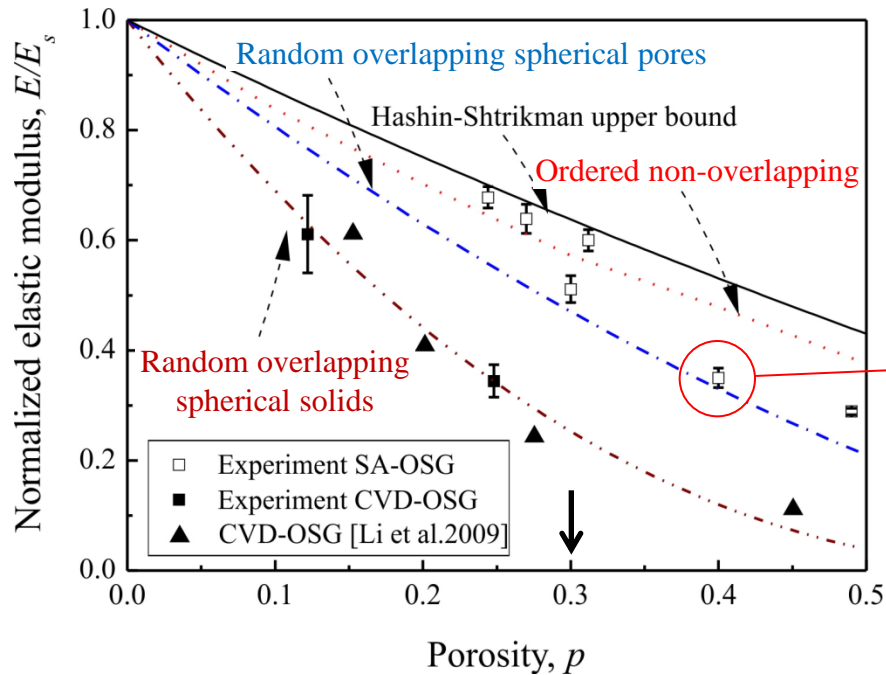
A general map of E/E_s vs. p for different porous structure



Pore topology prediction



Threshold porosity



- Threshold value before pores begin overlapping, $p_{\text{threshold}}=0.3$ for the SA-OSG.
- TEM image at $p=0.42$ shows random overlapping spherical pores with very narrow pore size distribution.

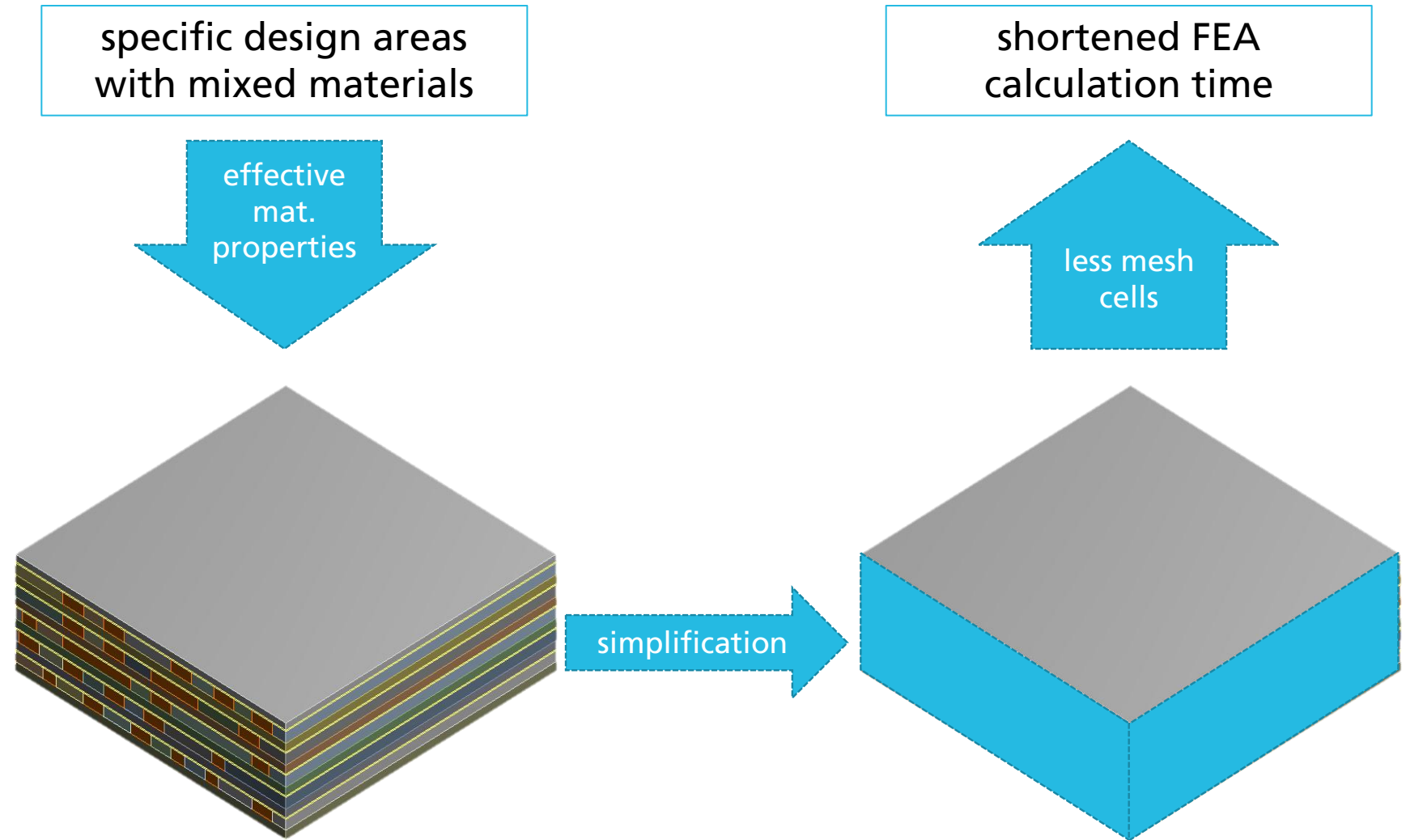


Coefficient of Thermal Expansion

CTE

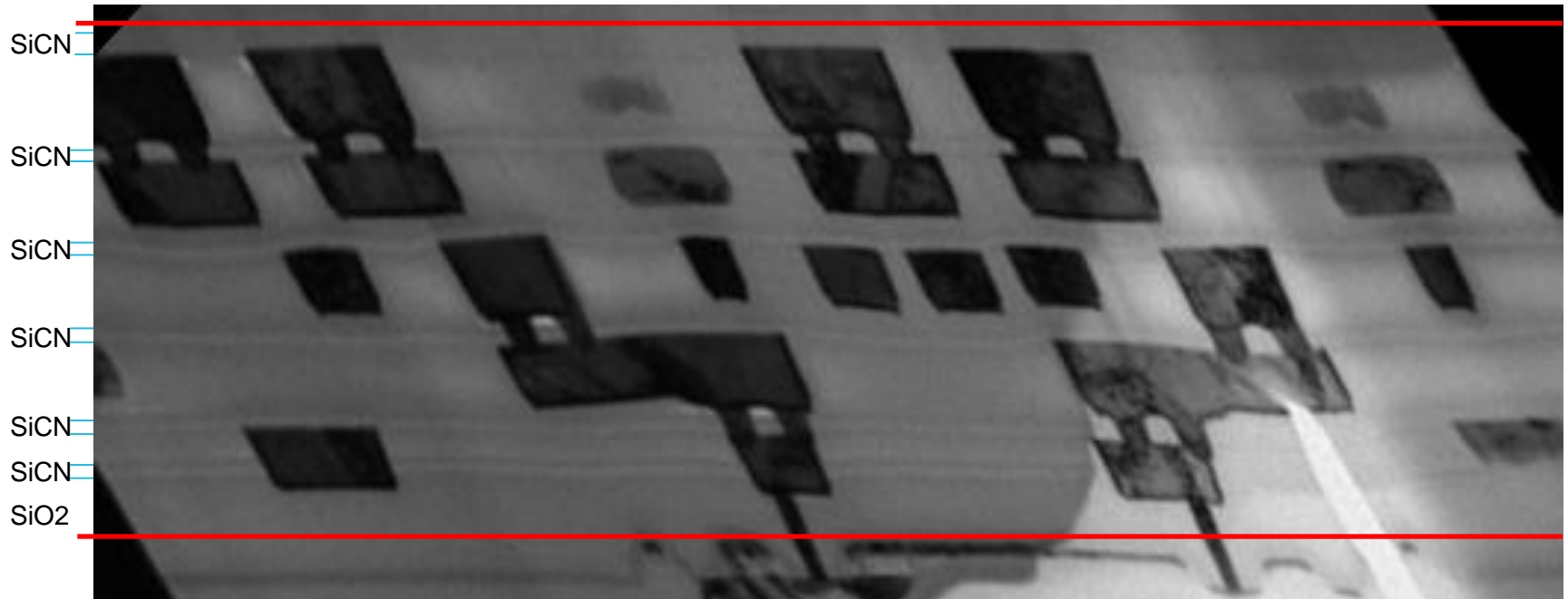


Motivation for effective CTE measurement



CTE – Volumetric balance

FIB cut lines in red



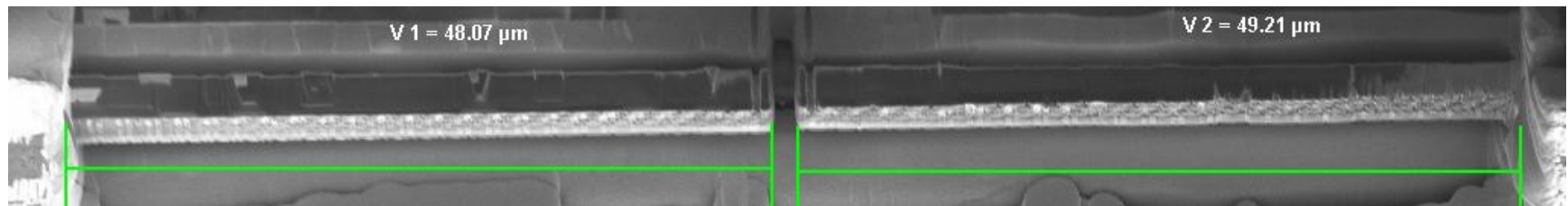
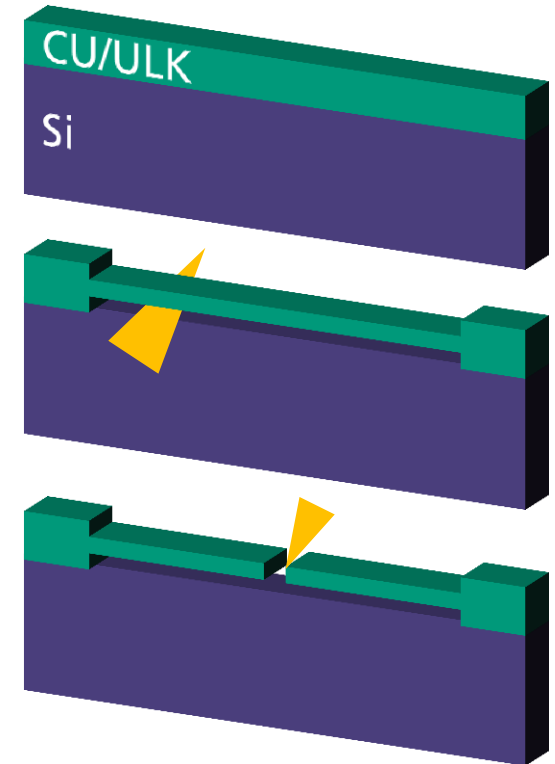
Note: We are measuring an effective CTE value, including some of the SiO₂ at the bottom CA layer, as well as SiCN layers in between.



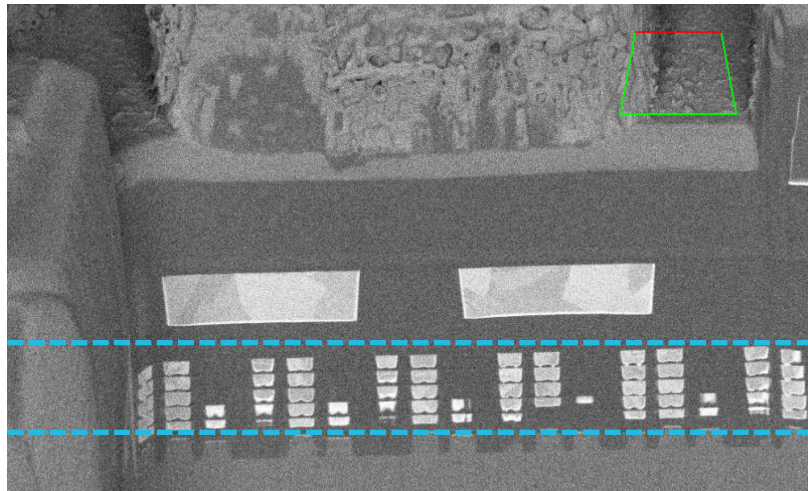
CTE measurements of BEoL: Preparation

First approach to determine CTE for Cu/ULK for a partially deprocessed 3DIC, by combination of FIB cutting and SEM (heating stage holder).

- ❑ isolate a bar
- ❑ separate in two bars of same length
- ❑ mount on heating stage and measure the gap in the middle during the experiment



CTE measurements of BEoL: Stack



Full metallization stack

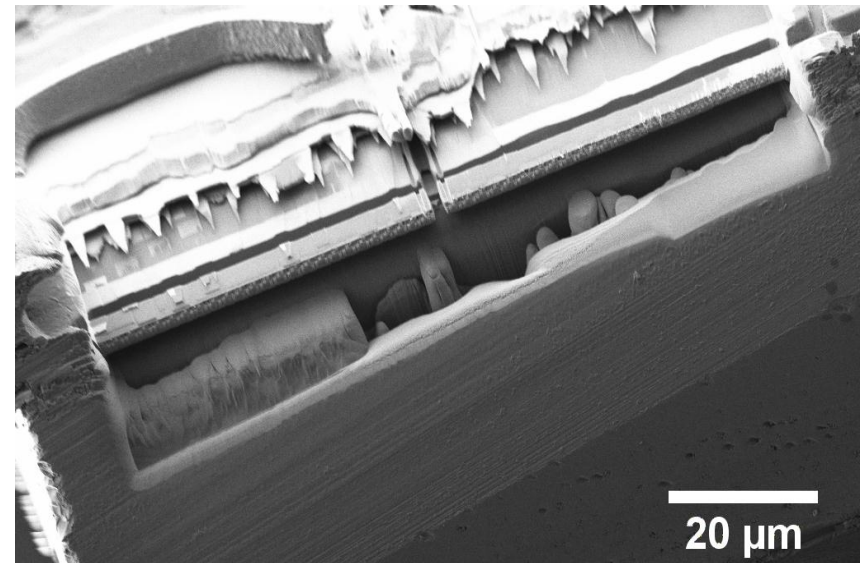
TEOS/SiN Passivation and Al

V5-M6 Thick Cu/(F)TEOS

M1-M5 Cu/ULK



FIB cutting to form two freestanding 50 μ m »cantilevers« which are free to expand towards the center (only Cu/ULK)



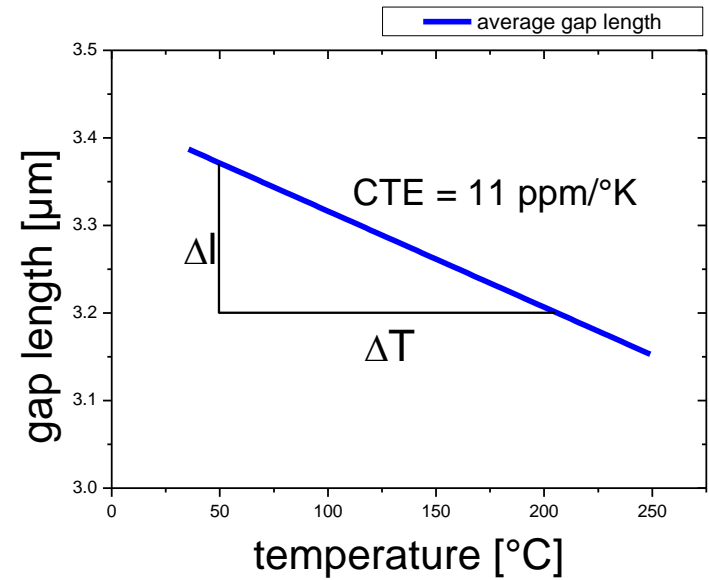
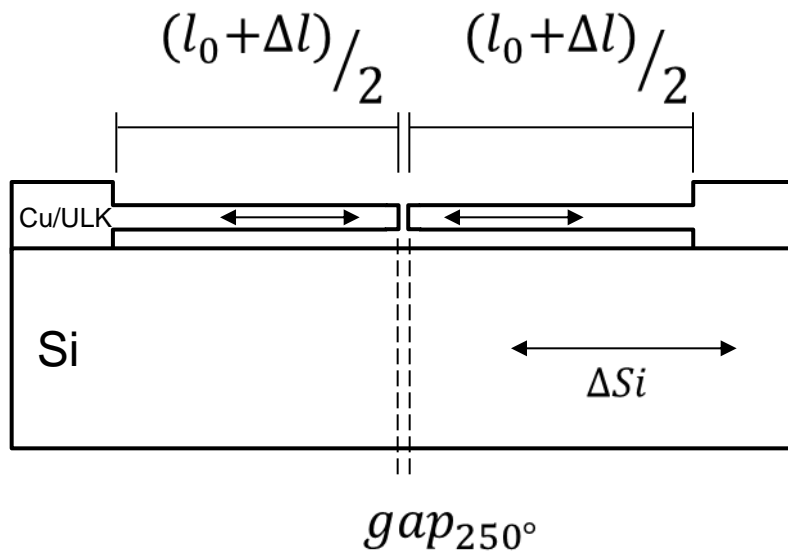
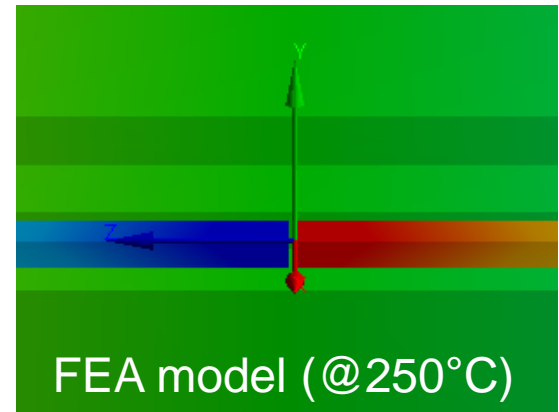
CTE measurements of BEoL: Basics (2)

$$\alpha_l = \frac{\Delta l}{l_0 \cdot \Delta T}$$

$$\Delta l = \Delta gap + \Delta Si$$

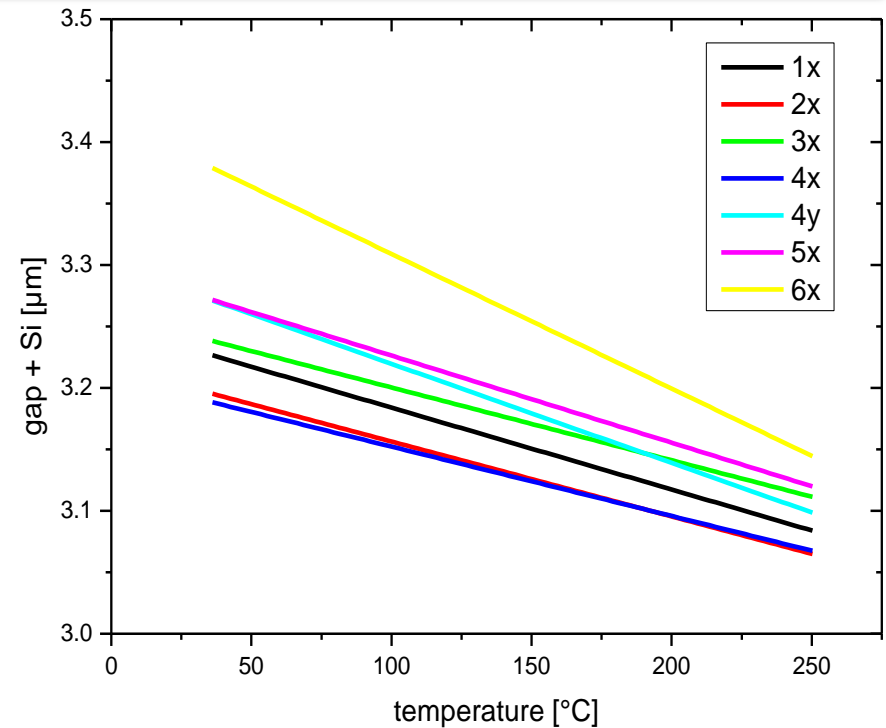
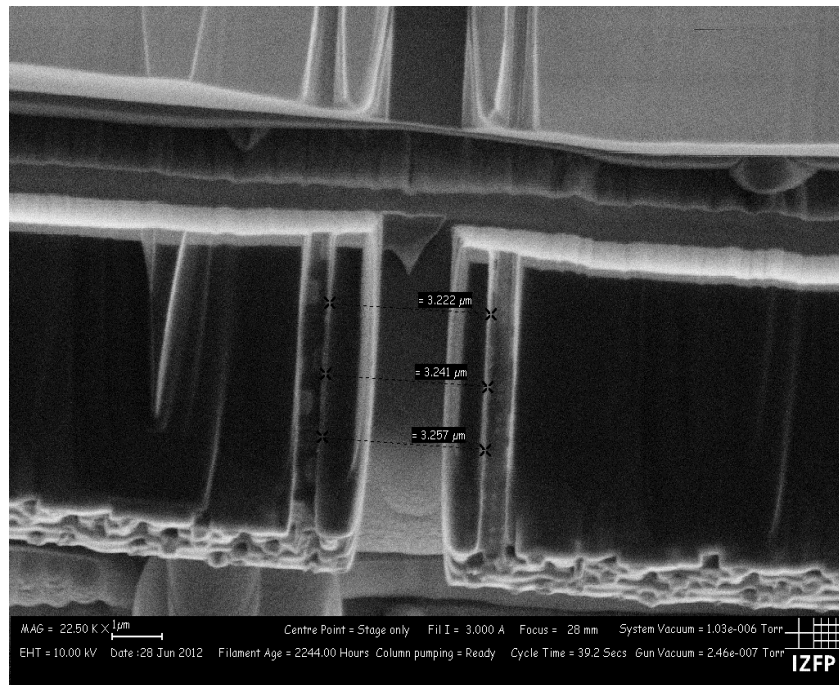
$$\Delta gap = gap_{25^\circ} - gap_{250^\circ}$$

$$\Delta Si = Si_{25^\circ} - Si_{250^\circ}$$

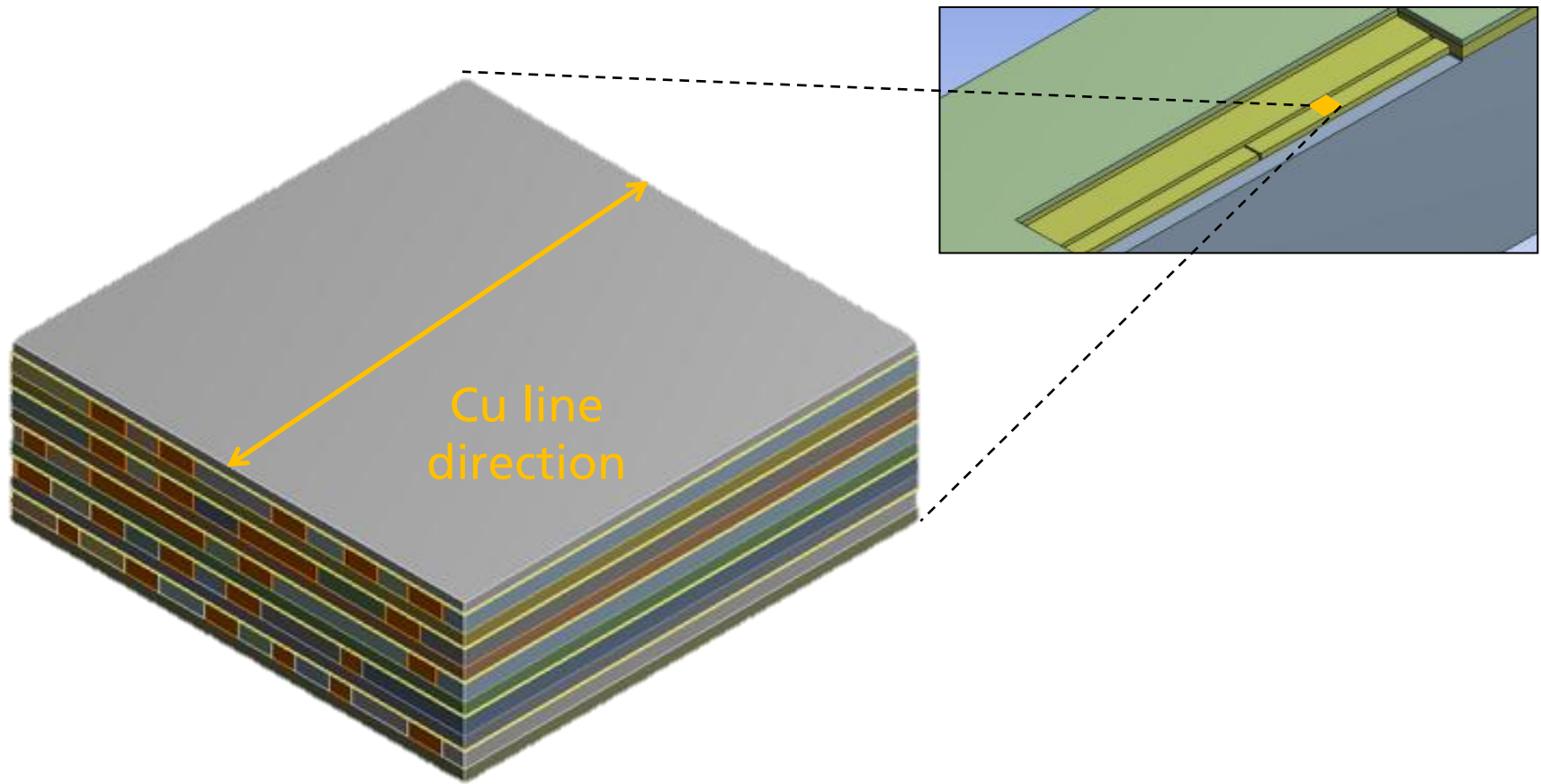


Effective CTE M1-M5/ULK

| spot | 1x | 2x | 3x | 4x | 4y | 5 | 6 |
|-------------|-------|-------|-------|-------|-------|-------|-------|
| CTE (ppm/K) | 6.7 | 6.1 | 5.9 | 5.6 | 8.0 | 7.1 | 11 |
| Cu % | 17.3% | 17.0% | 18.4% | 18.3% | 18.3% | 23.8% | 23.8% |



CTE – FEA simulation

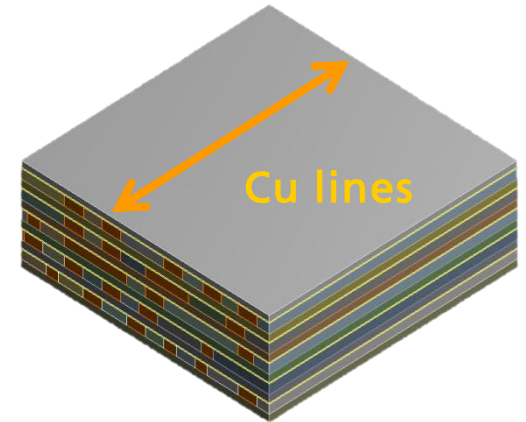
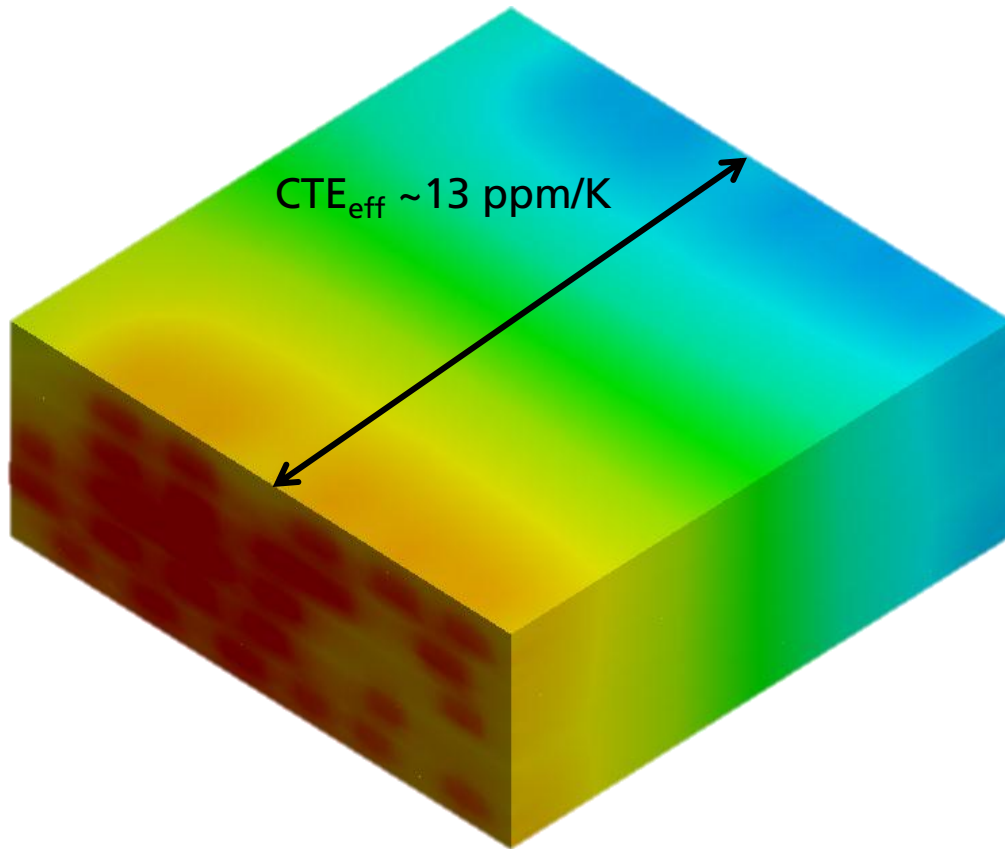


4 x 4 x 1.2 μm^3 part of CTE-bar



CTE – FEA simulation

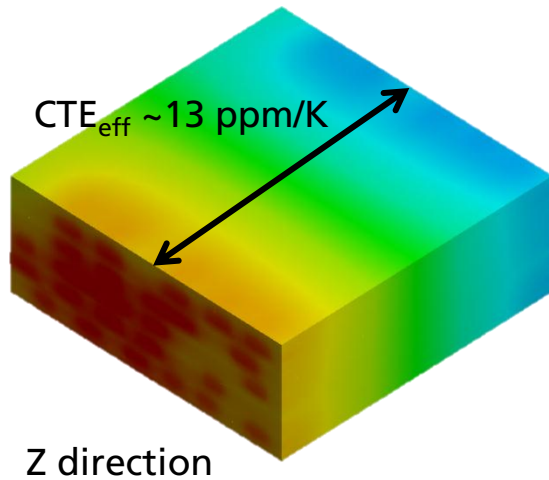
deformation in z direction – Cu inline



Cu randomly distributed
Cu density from real IC
dim. 4x4 μm^2

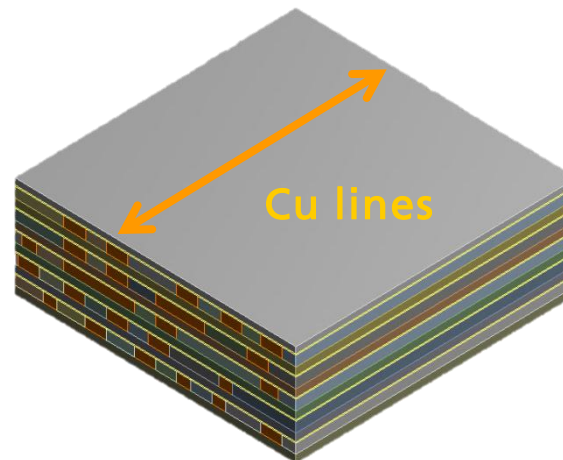
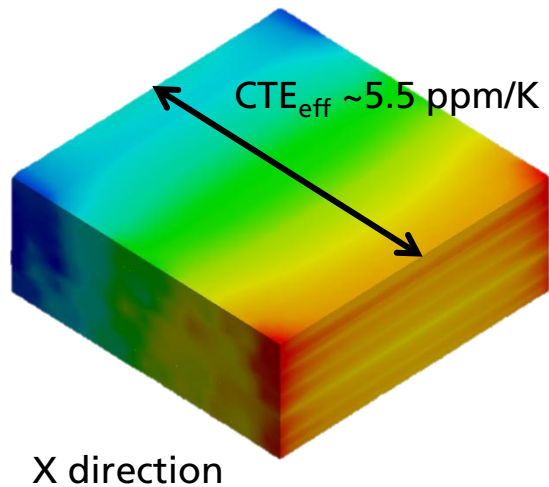


CTE – FEA simulation - Cu line direction



FEA results

- effective CTE highly constrained to design
- more information about Cu distribution and orientation needed
- simulated CTE_{eff} ~ 5.5 – 13 ppm/K matches exp. data



Adhesion

WEDGE-INDENTATION TECHNIQUE



Wedge Indentation Experiments

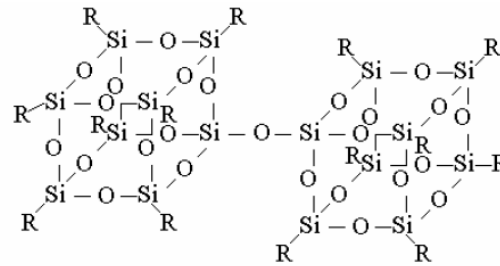


Hysitron TI-950

Low-k materials

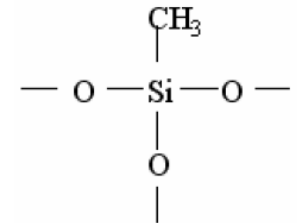
- Porous Spin-on glass (Methyl-silsesquioxane: **MSQ**)
- Densified PECVD glass (Black Diamond: **BD**)

MSQ, JSR LKD5102

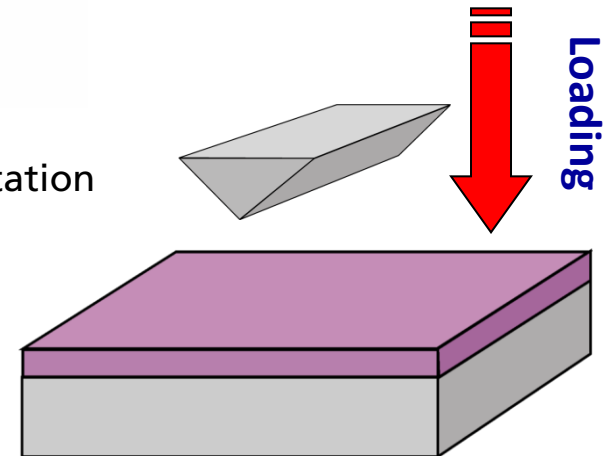


R=H, CH₃, ...

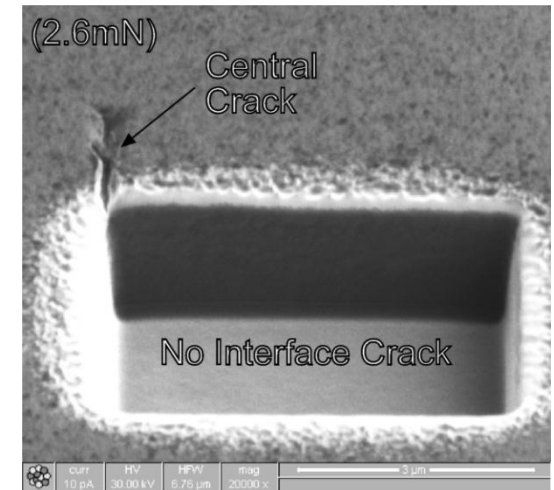
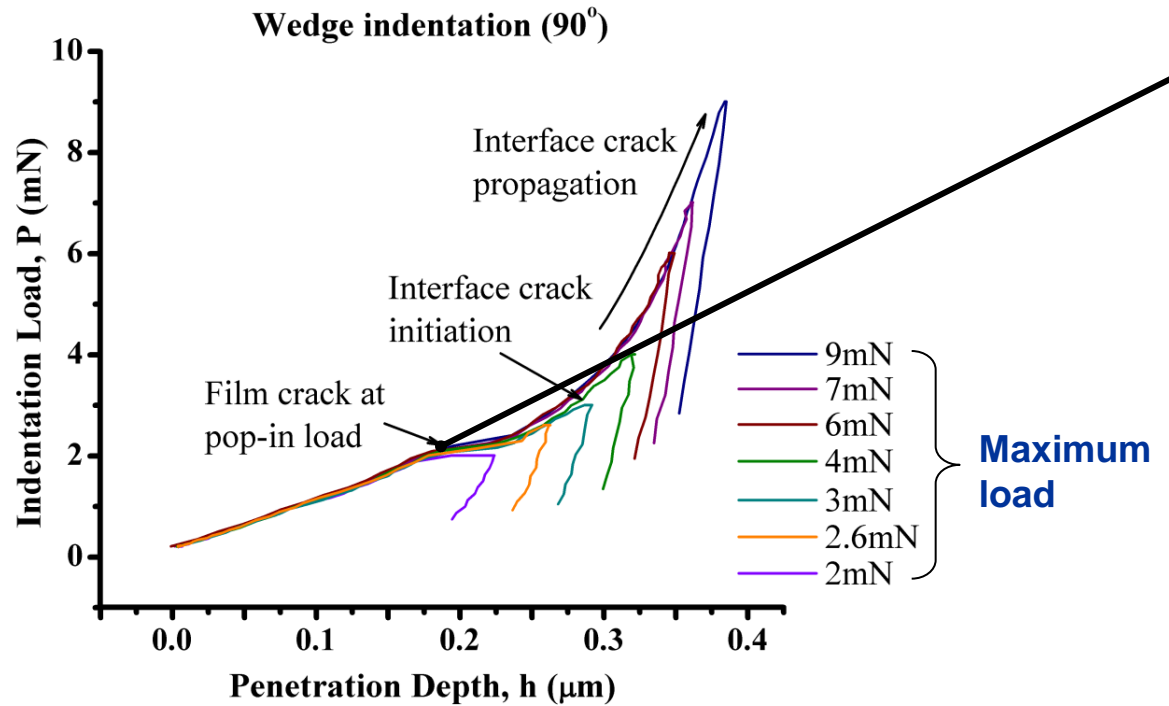
BD, Applied Materials



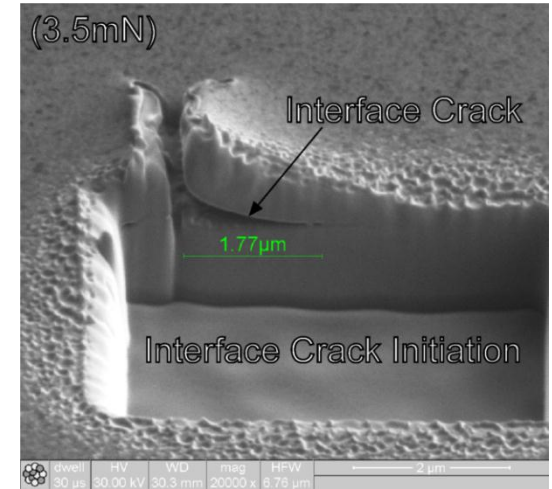
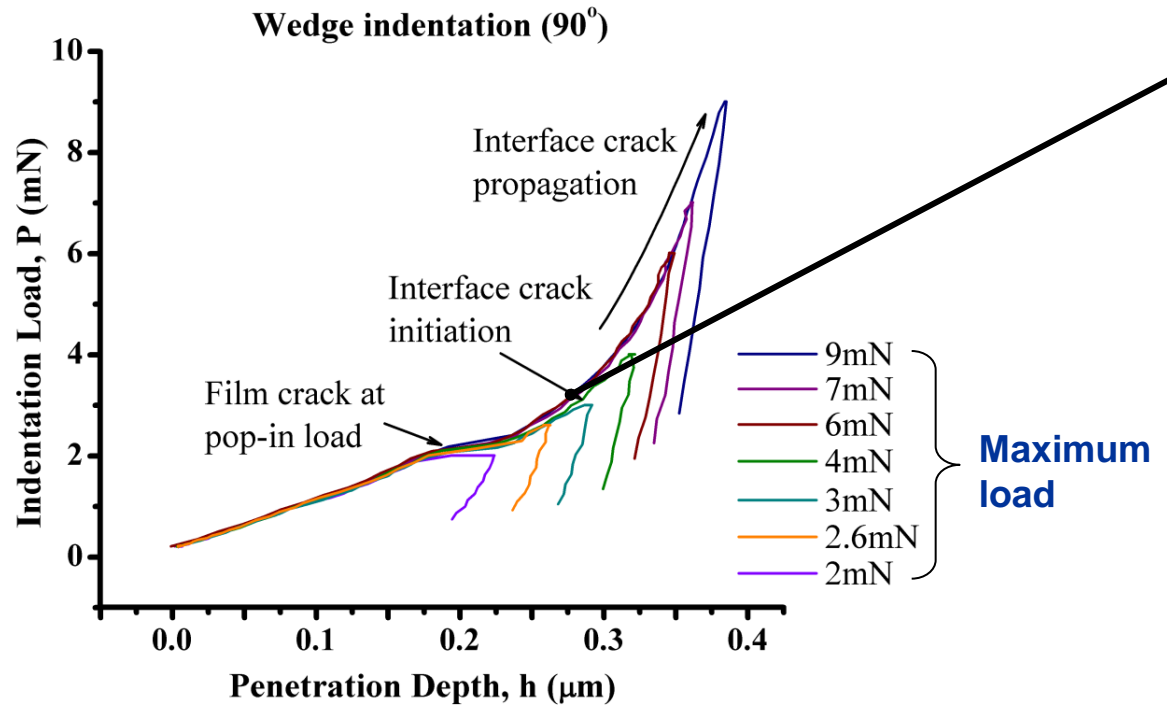
Wedge indentation



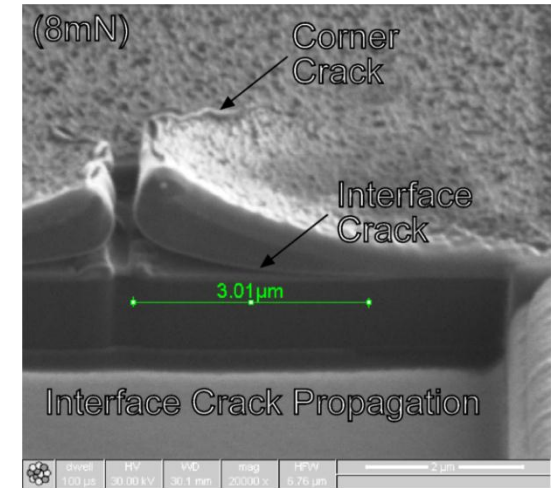
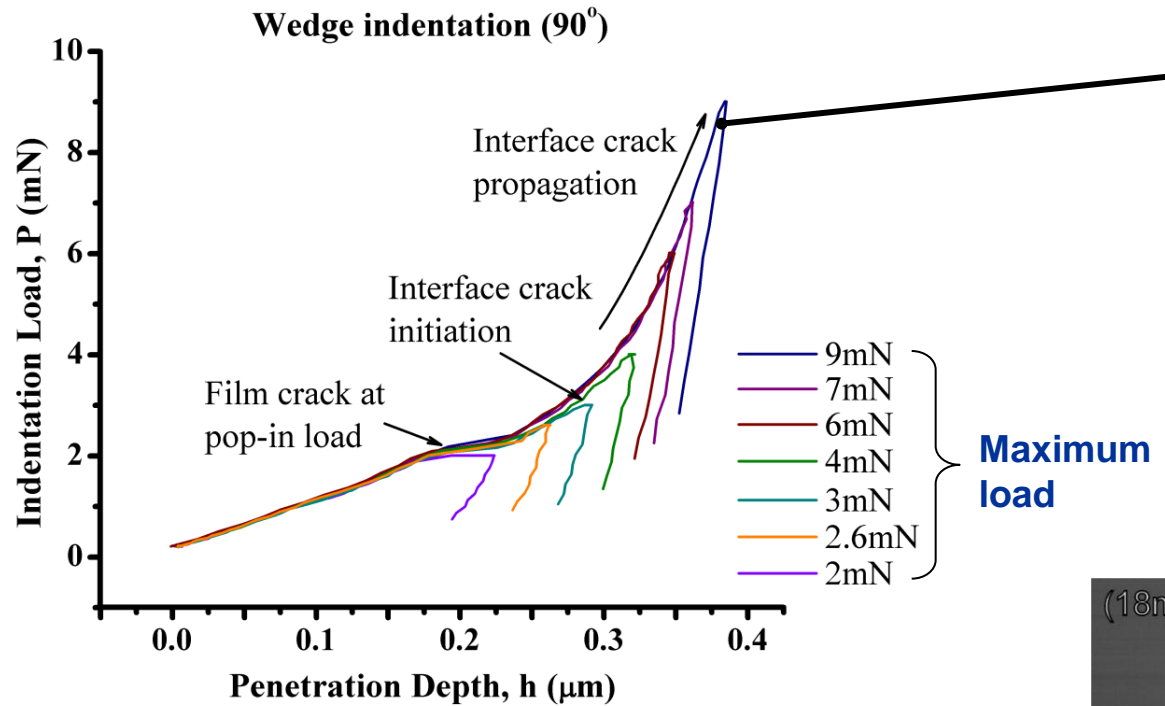
Indentation Induced Interfacial Fracture



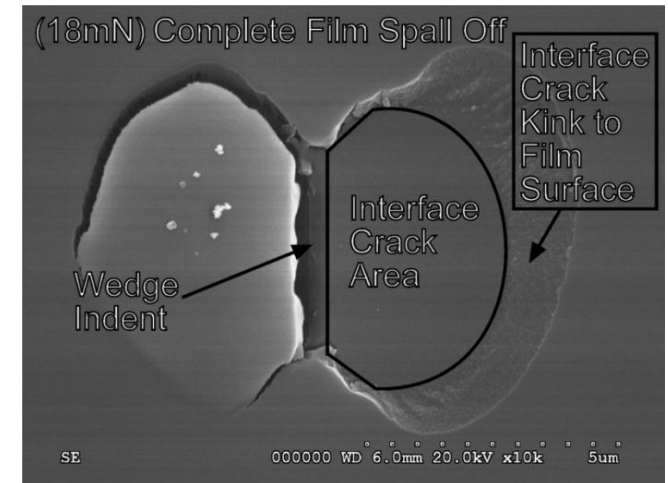
Indentation Induced Interfacial Fracture



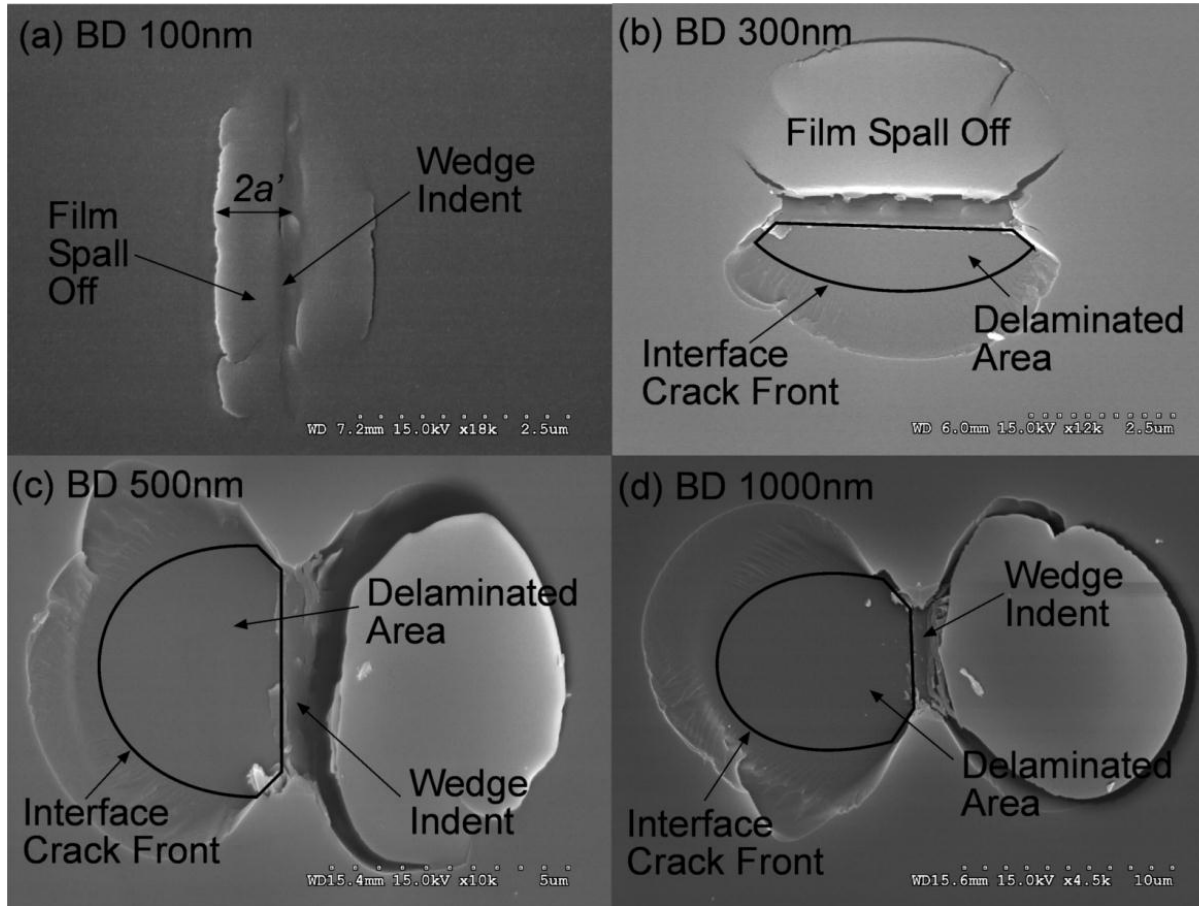
Indentation Induced Interfacial Fracture



Delamination Shape



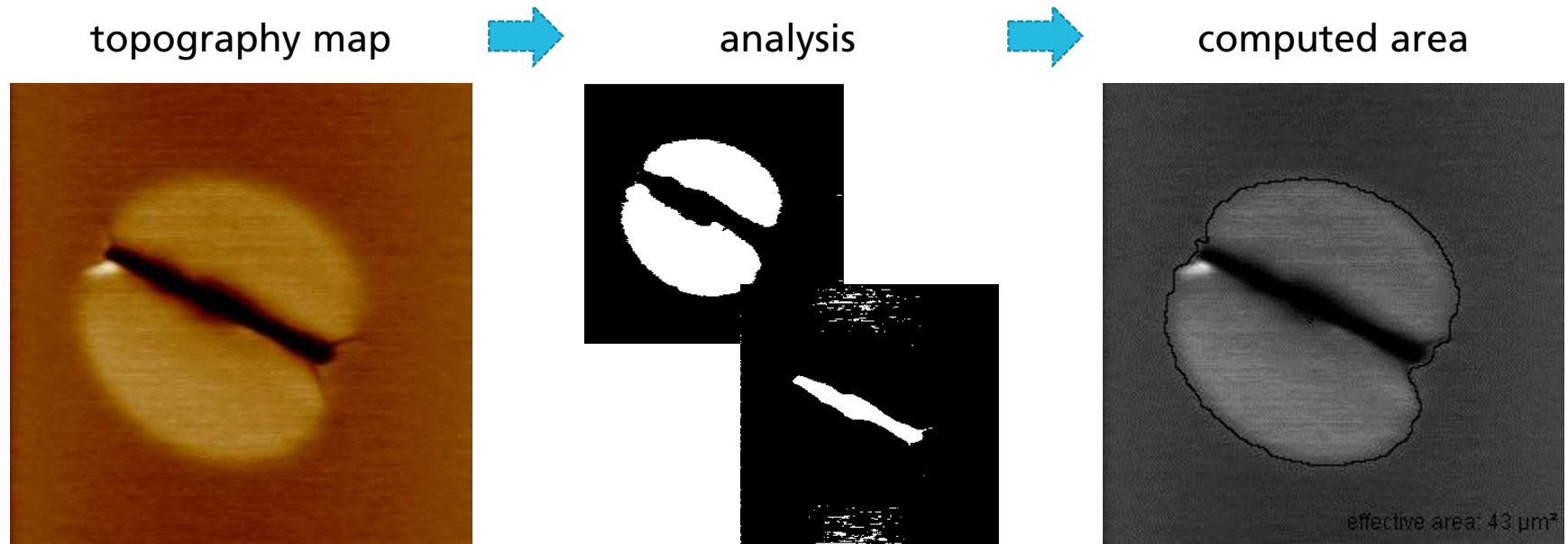
Interfacial toughness of varying film thicknesses



Varying film thickness results in different delamination shape.



Wedge Indentation – automated image analysis

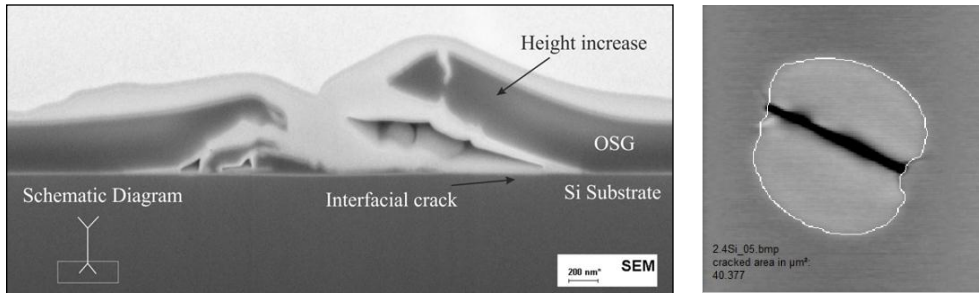


- Automated indentation and crack area mapping procedure with high local resolution
- Crack area and adhesion calculation software routine.



Wedge Indentation technique

Wedge Indentation results

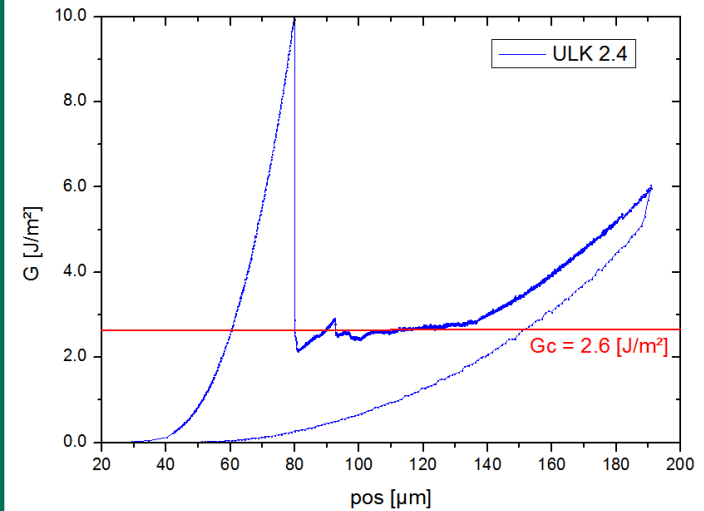


| Sample | G _c (J/m ²) | error | E (GPa) | error |
|---------|------------------------------------|-------|---------|-------|
| k = 2.7 | 4.24 | 0.29 | 8.86 | 0.63 |
| k = 2.5 | 3.38 | 0.31 | 6.22 | 0.19 |
| k = 2.4 | 2.79 | 0.18 | 4.42 | 0.32 |

Advantages:

- No sample preparation, fully automated.
- Statistical variation that represents the true adhesion variation, not the error of the experiment or sample prep.

4 Point Bending results



| Sample | G _c (J/m ²) |
|---------|------------------------------------|
| k = 2.7 | 4.3 |
| k = 2.5 | - |
| k = 2.4 | 2.6 |



Conclusion

- Mechanical test at a length scale similar to the pore size is very sensitive to small changes in the sample.
- Stiffening and hysteresis in **SA-OSG**: Porous structure and deformation mechanism.
- A **general map** of E/E_s vs p has been plotted.
- Effective **CTE** values have been determined for BEoL stack with different Cu line direction and density.
- The Wedge Indentation method delivers robust adhesion measurements without sample preparation.



Acknowledgement

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Martin Küttner,
Rüdiger Rosenkranz,
Zhongquan Liao

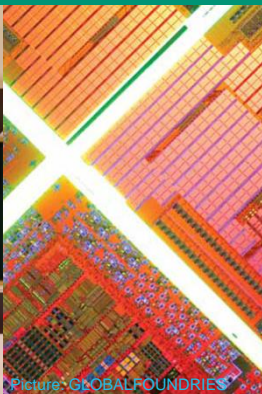
Thank you!



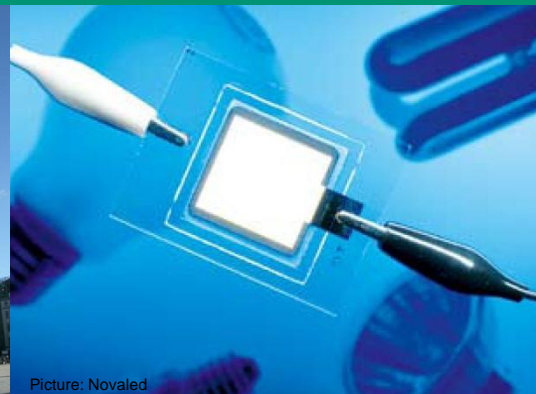
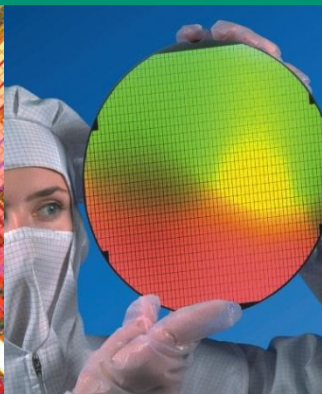
task 2246.001:
"Multi-Scale Materials Database for 3D
TSV Stacks – Input for Stress Simulation
and Model Validation"



Picture: Fraunhofer IPMS



Picture: GLOBALFOUNDRIES



Picture: Novaled

