

SOP No. 28
Recommended Standard Operating Procedure
for
Using Advanced Weighing Designs

1 Introduction

1.1 Purpose

Advanced weighing designs use a combination of double substitution comparisons of weights of equal nominal value or a series of weights in ascending or descending order; standard(s), unknown weights, and an additional standard called a check standard. The weights are intercompared using an equal-arm, single-pan mechanical, full electronic, or a combination balance utilizing built-in weights and a digital indication. The specific SOP for the double substitution procedure for each balance is to be followed. Weighing designs provide two methods of checking the validity of the measurement using an F-test to check the measurement process and a t-test to evaluate the stability of the standard and check standard. Hence, the procedure is especially useful for high accuracy calibrations in which it is critical to assure that the measurements are valid and well documented. This procedure is recommended for precision calibration of laboratory working standards that are subsequently used for lower level calibrations, for routine calibration of precision mass standards used for calibration of other mass standards, and for surveillance of mass reference and working standards.

1.2 Prerequisites

- 1.2.1 Calibrated mass standards, with recent calibration values and which have demonstrated metrological traceability to the international system of units (SI), which may be to the SI through a National Metrology Institute such as NIST.
- 1.2.2 Standards must be evaluated to ensure that standard uncertainties for the intended level of calibration are sufficiently small. Reference standards should only be used to calibrate the next lower level of working standards in the laboratory and should not be used to routinely calibrate customer standards.
- 1.2.3 Verify that the balance used is in good operating condition with sufficiently small process standard deviation as verified by F-test values, pooled short-term standard deviations, and by a valid control chart for check standards, or preliminary experiments to ascertain its performance quality when new balances are put into service. See NISTIR 5672¹ for a discussion on the performance levels expected for use of these procedures as part of a

¹Fraley, K. L., Harris, Georgia G. L., NISTIR 5672, Advanced Mass Calibration and Measurement Assurance Program for State Calibration Laboratories.

laboratory measurement assurance program to ensure traceability of laboratory standards.

- 1.2.4 Verify that the operator is experienced in precision weighing techniques, and has had specific training in SOP 2, SOP 4, SOP 5, SOP 29, and is familiar with the concepts in GMP 10. Further, the operator must have been trained in the creation of data files and the operation of the NIST Mass Code when it is used for data reduction as recommended. Example data sets and sample observation sheets are available in the Advanced Mass Seminar offered by the NIST Office of Weights and Measures.
- 1.2.5 Laboratory facilities must comply with the following minimum conditions to meet the expected uncertainty possible with this procedure and to comply with the balance manufacturer’s operating conditions specified for the balance. Equilibration of balances and weights requires environmental stability of the laboratory within the stated limits for a minimum of 24 hours before a calibration.

Table 1. Environmental conditions.

Echelon ²	Temperature Requirements During a Calibration	Relative Humidity (%)
I	OIML E ₁ , ASTM 000, 00, 0 Lower and upper limits: 18 °C to 23 °C Maximum changes: ± 0.5 °C / 12 h and ± 0.3 °C / h	40 to 60 ± 5 / 4 h
	OIML E ₂ , ASTM 1 Lower and upper limits: 18 °C to 23 °C Maximum changes: ± 1 °C / 12 h and ± 0.7 °C / h	

1.2.5.1 It is important that the difference in temperature between the weights and the air inside the mass comparator is as small as possible. Keeping the reference weight and the test weight inside, or next to, the mass comparator before and during the calibration can reduce this temperature difference. Standards and test artifacts must be allowed to reach equilibration in or near the balance before starting measurements.

² Echelon I corresponds to weights of Classes OIML E₁ and E₂, Echelon II corresponds to weights of Classes OIML F₁ and F₂.

2 Methodology

2.1 Scope, Precision, Accuracy

This method can be performed on any type of balance or mass comparator using the appropriate double substitution method for the weighing instrument. Because considerable effort is involved, this weighing design is most useful for calibrations of the highest accuracy. The weighing design utilizes a combination of double substitutions to calibrate a single unknown weight, or a group of related weights in a decade. This method introduces redundancy into the measurement process and permits two checks on the validity of the measurement; one on accuracy and stability of the standard using an integrated t-test and the other on process repeatability using an F-test. A least-squares best fit analysis is done on the measurements to assign a value to the unknown weights. The standard deviation of the process depends upon the resolution of the balance and the care exercised to make the required weighings. The accuracy will depend upon the accuracy and uncertainty of the calibration of the restraint weights and the precision of the comparison.

2.2 Summary

A restraint weight, S , in some cases two restraint weights, S_1 and S_2 , an unknown weight, X , or group of unknown weights, and a check standard, S_C are compared in a specific order typically using the double substitution procedure although other procedures may be appropriate. The balance and the weights must be prepared according to the appropriate method for the balance being used. Once the balance and weights have been prepared, all readings must be taken from the reading scale of the balance without adjusting the balance or weights in any way. Within a double substitution all weighings are made at regularly spaced time intervals to minimize effects due to instrument drift. Because of the amount of effort required to perform weighing designs, the procedure includes an air buoyancy correction using the average air density as determined immediately before and after the weighings, drift-free equation for calculating the observed differences, correction for the cubical coefficient of expansion when measurements are not made at 20 °C, an average sensitivity for the balance over the range of measurements made, and the international formula for air density.³

2.3 Apparatus/Equipment Required

2.3.1 Precision analytical balance or mass comparator with sufficient capacity and resolution for the calibrations planned.

³ See NISTIR 6969, Selected Procedures for Mass Calibrations, SOP 2, Air Density Calculations. Use Option B. The difference between Option A and Option B in SOP 2 is less than the uncertainty associated with assumptions made in the air density equations.

- 2.3.1. Calibrated reference standards (usually starting at 1 kg or 100 g), calibrated check standards for each decade (e.g., 1 kg, 100 g, 10 g, 1 g, 100 mg, 10 mg, 1 mg for the seven series between 1 kg and 1 mg) and working standards.
- 2.3.2. Calibrated sensitivity weights and tare weights selected to comply with the requirements of SOP 34. Note: The calculations performed by the Mass Code do not take into consideration the value of any tare weights used in the weighing design. Additional calculations will be required when tare weights are used.
- 2.3.3. Uncalibrated weights to be used to adjust the balance to the desired reading range if needed.
- 2.3.4. Forceps to handle the weights, or gloves to be worn if the weights are moved by hand. Forceps and gloves must be selected to avoid damage or contamination of mass standards.
- 2.3.5. Stop watch or other timing device to observe the time of each measurement (calibration not required; this is used to ensure consistent timing of the measurement). If an electronic balance is used that has a means for indicating a stable reading, the operator may continue to time readings to ensure consistent timing that can minimize errors due to linear drift.
- 2.3.6. Calibrated barometer with sufficiently small resolution, stability, and uncertainty (See SOP 2, e.g., accurate to ± 66.5 Pa (0.5 mmHg)) to determine barometric pressure.⁴
- 2.3.7. Calibrated thermometer with sufficiently small resolution, stability, and uncertainty (see SOP 2, e.g., accurate to ± 0.10 °C) to determine air temperature.⁴
- 2.3.8. Calibrated hygrometer with sufficiently small resolution, stability, and uncertainty (see SOP 2, e.g., accurate to ± 10 percent) to determine relative humidity.⁴

2.4 Procedure

2.4.1 Preliminary Procedure

2.4.1.1 Weights are visually inspected for cleanliness and damage.

2.4.1.2 If cleaning weights, it is important to clean weights before any measurements are made because the cleaning process may change the mass of the weight. Cleaning should not remove any significant

⁴ The barometer, thermometer, and hygrometer are used to determine the air density at the time of the measurement. The air density is used to make an air buoyancy correction. The limits specified are recommended for high precision calibration.

amounts of weight material. Weights should be handled and stored in such a way that they stay clean. Before calibration, dust and any foreign particles shall be removed. Care must be taken not to change the surface properties of the weight (i.e. by scratching the weight). If a weight contains significant amounts of dirt that cannot be removed by the methods cited above, the weight or some part of it can be washed with clean alcohol, distilled water, or other solvents. Weights with internal cavities should normally not be immersed in the solvent to avoid the possibility that the fluid will penetrate the opening. If there is a need to monitor the stability of a weight in use, the mass of the weight should, if possible, be determined before cleaning.

2.4.1.3 If weights are cleaned with solvents, they must be stabilized for at least 7 to 10 days.

2.4.1.4 Before making measurements, place the test weight and standards in the balance chamber or near the balance overnight to permit the weights and the balance to attain thermal equilibrium, or use a thermal soaking plate next to the balance with weights covered. Thermal equilibration time is particularly important with weights larger than 1 gram. An alternative heat source such as a heat lamp may further improve temperature stability in front of the balance. Conduct preliminary measurements to determine the size of the sensitivity weight and any tare weights that are required following SOP 34; adjust the balance to the appropriate reading range of the balance indications and exercise the balance. Refer to the appropriate double substitution method for details.

2.4.2 Weighing Designs

Table 2 shows the most common comparisons to be made as referenced in NBS Technical Note 952, Designs for the Calibration of Standards of Mass, J. M. Cameron, M. C. Croarkin, and R. C. Raybold, 1977. Each series is characterized by the number of observations, n , the degrees of freedom, $d.f.$, associated with the standard deviation, the number of weights in each design, k (not shown in this table), the number of restraints (standards), and check standards, along with appropriate positions within the design*.

*Positions for check standards must be carefully considered as subsequent equations may be dependent on the position of use.

Table 2. Common weighing designs.

Design ID	Description	<i>n</i> Observations	<i>d.f.</i> Degrees of freedom	Restraint Position	Check Std Position ^a
A.1.1	3-1 Weighing Design ⁵	3	1	1	3
A.1.2	4-1 Weighing Design	6	3	1, 2	3 or 4
A.1.4	5-1 Weighing Design	10	6	1, 2	3, 4, or 5
A.2.1	6-1 Weighing Design	8	3	1, 2	3, 4, 5, or 6
C.1 ^a	5, 3, 2, 1, 1 Design (descending)	8	4	1, 2, 3	5 or 4
C.1	5, 3, 2, 1, 1 Design (ascending)	8	4	5	4
C.2	5, 3, 2, 1, 1, 1 Design (descending)	11	6	1, 2, 3	4, 5, or 6
C.2	5, 3, 2, 1, 1, 1 Design (ascending)	11	6	6	4 or 5
C.9 ^a	5, 2, 2, 1, 1 Design (descending)	8	4	1, 2, 3, 4	5
C.9	5, 2, 2, 1, 1 Design (ascending)	8	4	5	4
C.10	5, 2, 2, 1, 1, 1 Design (descending)	8	3	1, 2, 3, 4	5 or 6
C.10	5, 2, 2, 1, 1, 1 Design (ascending)	8	3	6	4 or 5

^aIf these designs are NOT the last in a series, there is no position for a check standard.

The “restraint” is another name for the standard used in the comparison. Matrices are shown in Technical Note 952. Determine the best design prior to beginning the series. The series shown allow calibration of any commonly found set of mass standards in the 5, 2, 2, 1 combination or the 5, 3, 2, 1 combination. See the supplemental job aid spreadsheet associated with NISTIR 5672 for many additional weighing designs that identify associated restraint and check standard positions, with the associated K_1 and K_2 values needed for calculating between-time standard deviations.

2.4.3 Measurement Procedure

Record the pertinent information for all weights being intercompared on a suitable data sheet unless an automated data collection system is being used to collect the data and create a data file. Record or collect the laboratory ambient temperature, barometric pressure, and relative humidity immediately before and immediately after each series of intercomparisons.

3 Calculations

Calculations are completed by the NIST Mass Code as described in NBS Technical Note 1127, National Bureau of Standards Mass Calibration Computer Software, R. N. Varner,

⁵Design a.1.1. with inverted order (y₃, y₂, and y₁), with restraint in position 1 (B) is detailed in SOP 5.

and R. C. Raybold, July 1980, with updates to conform to the international formula for calculating air density and the ISO/IEC Guide to the Expression of Uncertainties as described in the NIST Technical Note 1297 and minor error corrections to the original code. The Mass Code performs two statistical tests (t-test and F-test) to verify both the value of the restraints and check standards, and to verify that the measurement process was in control during the comparisons.

3.1 Calculating Effective Densities and Coefficients of Expansion for Summations⁶:

Some designs use a summation mass and sometimes the individual masses of this summation will be constructed from different materials that have different densities and coefficients of expansion. The following equations will be used to calculate the effective density and effective coefficient of expansions for the summation that will be needed as input for the data file. The subscripts 5, 3, and 2 refer to the individual masses that comprise the summation. This approach may also be needed with a 5, 2, 2, 1 combination. E.g., a summation of 1 kg, might be 500 g, 300 g, and 200 g (or 500 g, 200 g, 200g, and 100 g). A summation for 100 g would be 50 g, 30 g, and 20 g (or the equivalent of a 5221 series). A metric calibration of a 4 oz weight would need to add up to 113.389 g (probably 100 g, 10 g, 3 g, 300 mg, 100 mg) and then must also address unequal nominal values as shown in the equations in SOP 4, 5, and 7 as applicable.

$$\text{Effective Density} = \frac{M_5 + M_3 + M_2}{\left(\frac{M_5}{\rho_5}\right) + \left(\frac{M_3}{\rho_3}\right) + \left(\frac{M_2}{\rho_2}\right)} \quad \text{Eqn. (1)}$$

$$\text{Effective Cubical Coefficient of Expansion} = \frac{\left(\frac{M_5}{\rho_5}\alpha_5\right) + \left(\frac{M_3}{\rho_3}\alpha_3\right) + \left(\frac{M_2}{\rho_2}\alpha_2\right)}{\left(\frac{M_5}{\rho_5}\right) + \left(\frac{M_3}{\rho_3}\right) + \left(\frac{M_2}{\rho_2}\right)} \quad \text{Eqn. (2)}$$

Table 3. Variables for Above Equations.

Variable	Description
<i>M</i>	Mass (g)
<i>ρ</i>	Density (g/cm ³)
<i>α</i>	Cubical Coefficient of Expansion (/ ^o C)

4 Measurement Assurance

4.1. The within process standard deviation is incorporated into the NIST Mass Code and is used to conduct an F-test of the observed standard deviation versus the pooled/accepted standard deviation of the process at a 95 % confidence level. See NISTIR 6969, Section 8.9 for details of the F-test.

⁶Jaeger, K B., and R. S. Davis, NIST Special Publication 700-1, A Primer for Mass Metrology, November 1984.

- 4.2. Weighing designs integrate a suitable check standard (See GLP 1, SOP 9 and SOP 30).
- 4.3. The check standard value is calculated and immediately evaluated to verify that the mass is within established limits; a t-test is incorporated to compare the observed value against accepted value at a 95 % confidence level. This statistical test is incorporated in the NIST Mass Code. See NISTIR 6969, Section 8.16 for details and statistics that are used.
- 4.4. The mean value of the check standard over time is also compared to an appropriate reference value of the check standard with respect to their applicable expanded uncertainties to evaluate bias and drift over time. Excessive drift or bias must be investigated and followed with suitable corrective action. See NISTIR 6969, SOP 9, Section 3.6 for assessment methodology.
- 4.5. Check standard measurement results obtained over time are used to calculate the standard deviation of the measurement process, s_r .

5 Assignment of Uncertainty

The NIST Mass Code generates uncertainties as a part of the data reduction. Proper input in the data file is critical for obtaining valid results and is dependent upon a well characterized measurement process. See NISTIR 5672 for a discussion on the input for standard uncertainties in the data file. Comprehensive calculations of the uncertainties for weighing designs must be completed outside of the NIST Mass Code at this time, and a supplemental job aid spreadsheet is posted on the NIST OWM website with this SOP for that purpose.

5.1 Calculating the standard uncertainty, u_s , of the starting restraint in the first series:

Usually the starting restraint will be one or several 1 kg (or 100 g) mass standards that have calibrations and density determinations from a National Metrology Institute or an accredited laboratory. The uncertainty of the standard as stated on a calibration report is divided by the appropriate coverage factor, dependent on the confidence interval stated in the calibration certificate.

- 5.1.1 One starting restraint scheme (a single starting standard), where U_s is the uncertainty from NIST which must be divided by the proper coverage factor, k .

$$u_s = \frac{U_s}{k} \quad \text{Eqn. (3)}$$

5.1.2 Multiple starting restraint schemes with standards calibrated at the same time against the same starting standards, i.e., dependent calibration (more than one starting standard):

$$u_s = \frac{U_{s1}}{k_1} + \frac{U_{s2}}{k_2},$$

or

Eqn. (4)

$$u_s = \frac{U_{s1}}{k_1} + \frac{U_{s2}}{k_2} + \frac{U_{s3}}{k_3}, \text{ etc.}$$

5.1.3 Multiple starting restraint schemes with standards *NOT* calibrated at the same time as the starting standards, i.e., independent calibration (more than one starting standard):

$$u_s = \sqrt{\left(\frac{U_{s1}}{k_1}\right)^2 + \left(\frac{U_{s2}}{k_2}\right)^2},$$

or

Eqn. (5)

$$u_s = \sqrt{\left(\frac{U_{s1}}{k_1}\right)^2 + \left(\frac{U_{s2}}{k_2}\right)^2 + \left(\frac{U_{s3}}{k_3}\right)^2}, \text{ etc.}$$

5.2 Calculating the within-process standard deviation, s_w , for each series:

For each weighing design, the observed within process standard deviation, s_w , along with its degrees of freedom, df , is pooled using the technique described in NISTIR 6969 Section 8.4.

$$s_w = \sqrt{\frac{(df_1)s_1^2 + (df_2)s_2^2 + \dots + (df_k)s_k^2}{df_1 + df_2 + \dots + df_k}} \quad \text{Eqn. (6)}$$

5.3 Calculating the between-time standard deviation, s_b , for each series:

Establish a standard deviation over time, s_t , for each check standard over time. If a plot of the check standard shows no apparent drift, the between-time standard deviation may be calculated. The following formulae are used to calculate the between-time standard deviation for the series. If s_b^2 is less than zero, then s_b is treated as zero. See the supplemental job aid spreadsheet associated with NISTIR

5672 for many additional weighing designs, and variations on the designs noted in this section. The file lists restraint and check standard positions, with the associated K_1 and K_2 factors needed for calculating between-time standard deviations. Because of the way the K_n values are used to solve for s_b , it is possible to get a negative value in which case, zero is used as the value for s_b . NOTE: K factors as used in this section are not the same coverage factors that use the lower case k in uncertainty calculations.

5.3.1 For the 3-1 design with a single restraint, and a check standard that is either another single weight or a summation, the between time standard deviation is calculated using the following formula. The check standard may be in any other position.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.8165$$

$$K_2 = 1.4142$$

$$s_b = \frac{1}{1.4142} \sqrt{s_t^2 - 0.8165^2 s_w^2}$$

Eqn. (7)

5.3.2 Using a 4-1 design with two restraints, and the check standard is the difference between the two restraints, the next equation may be used to calculate the between-time standard deviation. If another weight in the series is used as the check standard, another equation is needed.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.7071$$

$$K_2 = 1.4142$$

$$s_b = \frac{1}{1.4142} \sqrt{s_t^2 - 0.7071^2 s_w^2}$$

Eqn. (8)

5.3.3 Using a 4-1 design with two restraints, and with a single check standard occupying any of the remaining positions, the next equation may be used to calculate the between-time standard deviation.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 + K_1^2 s_w^2}$$

$$K_1 = 0.6124$$

$$K_2 = 1.2247$$

$$s_b = \frac{1}{1.2247} \sqrt{s_t^2 - 0.6124^2 s_w^2}$$

Eqn. (9)

- 5.3.4 Using a 5-1 design with two restraints, and the check standard is the difference between the two restraints, the next equation may be used to calculate the between-time standard deviation. If another weight in the series is used as the check standard, another equation is needed.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.6325$$

$$K_2 = 1.4142$$

$$s_b = \frac{1}{1.4142} \sqrt{s_t^2 - 0.6325^2 s_w^2}$$

Eqn. (10)

- 5.3.5 Using a 5-1 design with two restraints, and with a single check standard occupying any of the remaining positions, the next equation may be used to calculate the between-time standard deviation.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.5477$$

$$K_2 = 1.2247$$

$$s_b = \frac{1}{1.2247} \sqrt{s_t^2 - 0.5477^2 s_w^2}$$

Eqn. (11)

- 5.3.6 In the second descending series (C.2), six weights are involved (500 g, 300 g, 200 g, 100 g, Check 100 g, and a summation 100 g). Calculate the standard deviations of the mass values for the Check 100 g (s_t) and plot the results to evaluate the presence or lack of drift. If no drift is present, the following formula is used to calculate the between-time standard deviation for this series and all subsequent C.2 series. Subsequent series include the following check standards: 100 g, 10 g, 1 g, 100 mg, 10 mg, and 1 mg. If s_b^2 is less than zero, then s_b is treated as zero.

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.3551$$

$$K_2 = 1.0149$$

$$s_b = \frac{1}{1.0149} \sqrt{s_t^2 - 0.3551^2 s_w^2}$$

Eqn. (12)

5.3.7 If a C.1 descending series is used, the following equation is used to calculate the between-time standard deviation when the check standard is in either of the last two positions:

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

$$K_1 = 0.4175$$

$$K_2 = 1.0149$$

$$s_b = \frac{1}{1.0149} \sqrt{s_t^2 - 0.4175^2 s_w^2}$$

Eqn. (13)

5.3.8 The between-time formulae shown here are those that are most common and are for descending series only. If another restraint or check standard is used, or if an ascending series is used, another formula will be needed. These formulae are statistically derived, based on the least squares analysis of the weighing design, and assume a normal, non-drifting distribution of measurement results. Equations for some other weighing designs may be calculated using the NIST Electronic Engineering Statistics Handbook. Section 2.3.3.2 “Solutions to Calibration Designs” gives an overview for deriving the solutions to weighing designs. It also provides the unifying equation for s_b (it is called s_{days} in the electronic handbook). To clarify the difference in terminology and notation the unifying equation for s_b is presented as:

$$s_{days} = \frac{1}{K_2} \sqrt{s_2^2 - K_1^2 s_1^2}$$

$$s_{days} \equiv s_b$$

$$s_1 \equiv s_w$$

$$s_2 \equiv s_t$$

$$s_b = \frac{1}{K_2} \sqrt{s_t^2 - K_1^2 s_w^2}$$

Eqn. (14)

Section 2.3.4.1 “Mass Weights” provides the solutions for 17 weighing designs used for decreasing weight sets, 6 weighing designs for increasing weight sets and 1 design for pound weights. K_1 is found in the portion of the solution titled “Factors for Repeatability Standard Deviations”, and K_2 is found in the portion titled “Factors for Between-Day Standard Deviations”.

5.3.9 Note that there is a supplemental job aid spreadsheet that is available and includes many weighing designs with associated K_1 and K_2 values and the equations for calculating between time standard deviations. The latest version of this spreadsheet is posted on the NIST website with this Standard Operating Procedure. An additional spreadsheet job aid is available for final calculations of uncertainty using the output of the Mass Code report.

5.4 Uncertainty associated with bias, u_d . Any noted bias that has been determined through analysis of control charts and round robin data must be less than limits

provided in SOP 29 and may be included if corrective action is not taken. (See NISTIR 6969, SOP 29 for additional details.)

5.5 Example components to be considered for an uncertainty budget table are shown in the following table.

Table 4. Example Uncertainty Budget Table.

Uncertainty Component Description	Symbol	Source	Typical Distribution
Uncertainty of the standard mass(es) (5.1)	u_s	Calibration certificate	Expanded uncertainty divided by coverage factor; combined for summations per SOP 29, restraint uncertainties assigned based on design calculations in the associated spreadsheet
Accepted standard deviation of the process as standard deviation over time, within-process standard deviation, and between time standard deviations (5.2, 5.3)	s_p s_t s_w s_b	Control chart, standard deviation chart	Normal Calculated based on K_1 and K_2 values for designs used
Uncertainty of the buoyancy correction	u_b	OIML R111	Rectangular
Air temperature (for air density)	u_t	SOP 2 or OIML R111	Rectangular
Air pressure (for air density)	u_p	SOP 2 or OIML R111	Rectangular
Air relative humidity (for air density)	u_{RH}	SOP 2 or OIML R111	Rectangular
Air density (formula)	u_{ρ_a}	SOP 2 or OIML R111	Rectangular
Mass densities	u_{ρ_m}	Measured and reported value OIML R111 Table B.7 Typically, 0.03 g/cm ³ to 0.05 g/cm ³	Rectangular
Uncertainty associated with bias (5.4)	u_d	Control chart, proficiency tests	See NISTIR 6969, SOP 29

5.6 Draft a suitable uncertainty statement for the certificate (e.g.,)

The uncertainty reported is the root sum square of the standard uncertainty of the standard, the standard deviation of the process, and the uncertainty associated with the buoyancy corrections, multiplied by a coverage factor of 2 ($k = 2$) for an approximate 95 percent confidence interval (95.45 %). Factors not considered in the evaluation: magnetism (weights are considered to meet magnetism specifications unless measurement aberrations are noted), balance eccentricity and linearity (these

factors are considered as a part of the measurement process when obtaining the standard deviation of the process when using a check standard with adequate degrees of freedom.

NOTE: Where inadequate degrees of freedom are available, k , is determined using the appropriate degrees of freedom and the 95.45 % column in the table from Appendix A of NISTIR 6969, SOP 29.

6 Certificate

6.1 See NISTIR 6969, SOP 1, for Preparation of Calibration Certificates. Report measurement results as printed in Tables I and II as generated by the Mass Code. Actual text of the Mass Code certificate must be modified for each laboratory to be ISO/IEC 17025 compliant and to reflect accurate uncertainty values. Report the mass, conventional mass, environmental conditions during the calibrations, mass density used (reported, measured, or assumed (specify which type is used)), and calculated expanded uncertainties with coverage factors.

6.2 Compliance assessments.

Evaluate compliance to applicable tolerances as needed or required by the customer or by legal metrology requirements. Decision criteria for uncertainty and tolerance evaluations include two components: 1) the expanded uncertainty, U , must be $< 1/3$ of the applicable tolerances published in ASTM E617 and OIML R111 standards and 2) the absolute value of the conventional mass correction value plus the expanded uncertainty must be less than the applicable tolerance to confidently state that mass standards are in or out of tolerance. Compliance assessments must note the applicable documentary standard and which portions of the standard were or were not evaluated.