

## NIST/UL Workshop on Photovoltaic Materials Durability

# Corrosion-induced AC Impedance Elevation in Crystalline Silicon Photovoltaic Cells/Modules

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December 13, 2019

Gaithersburg, Maryland, USA

### Contributors

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This work was supported by the New Energy and Industrial Technology Development Organization (NEDO), Japan.

# Final Destination: Service Lifetime Prediction

PV Modules exposed for **21 years**  
in Cfa climate (JP)

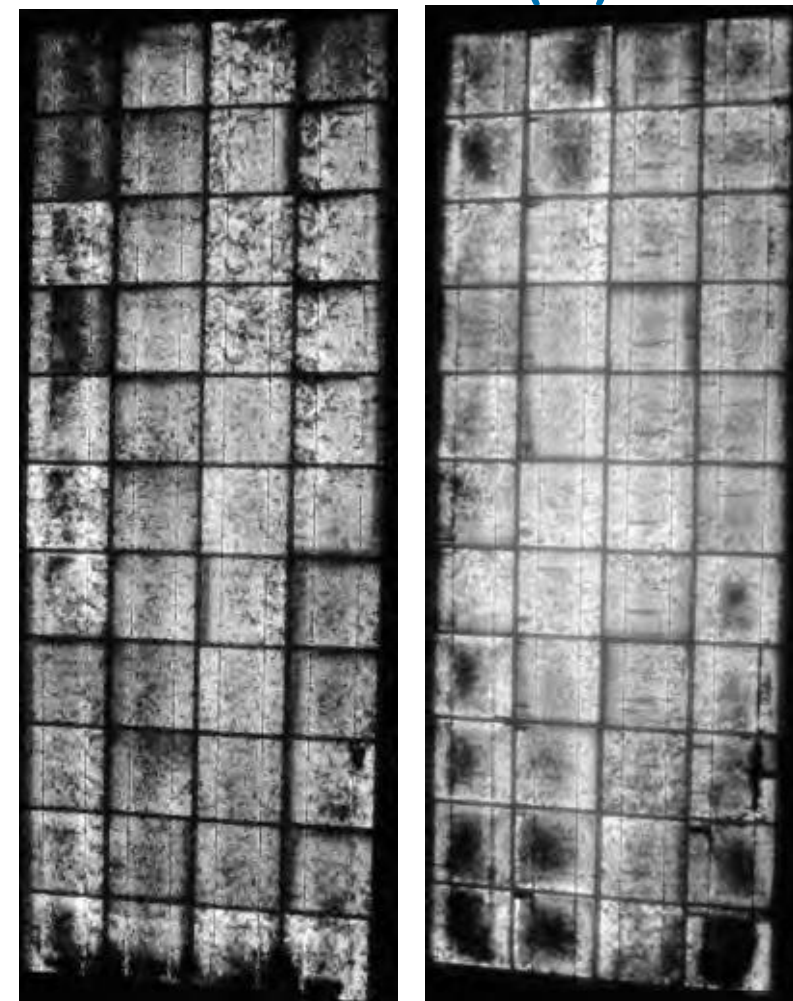
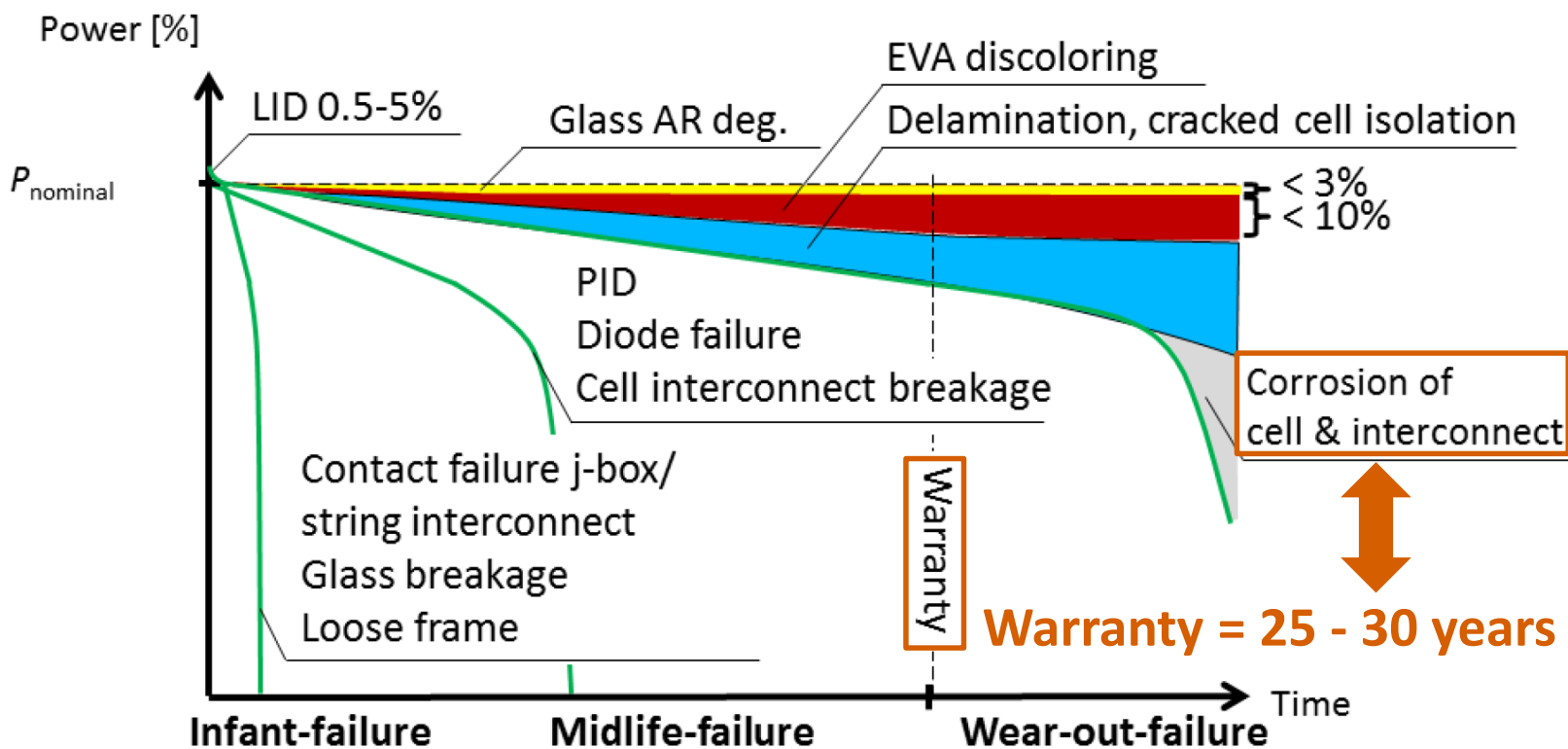


Fig. 3.1: Three typical failure scenarios for wafer-based crystalline photovoltaic modules are shown. Definition of the used abbreviations: LID – light-induced degradation, PID – potential induced degradation, EVA – ethylene vinyl acetate, j-box – junction box.

IEA-PVPS Task13 Team, “Review of Failures of Photovoltaic Modules.” Paris: International Energy Agency, 2014.

# Different EL appearances

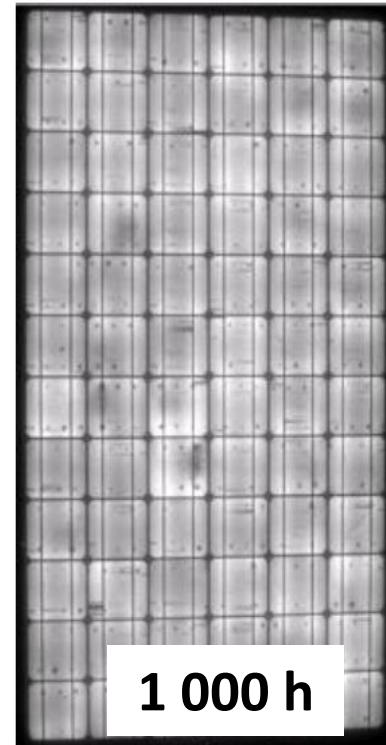
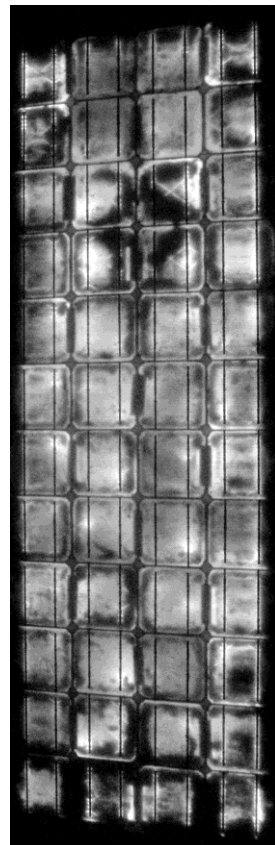
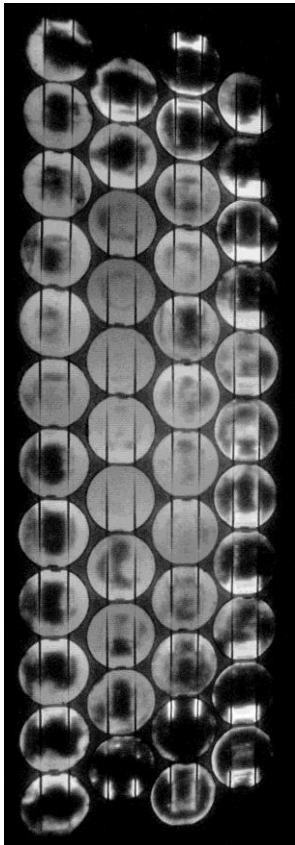
**There is no evidence that the failure mode observed after extended 85/85 exposure ever occurs in fielded modules.**

J. H. Wohlgemuth and M. D. Kempe in *Proc. 2013 IEEE 39th Photovolt. Spec. Conf.*, 2013, pp. 0126–0131.

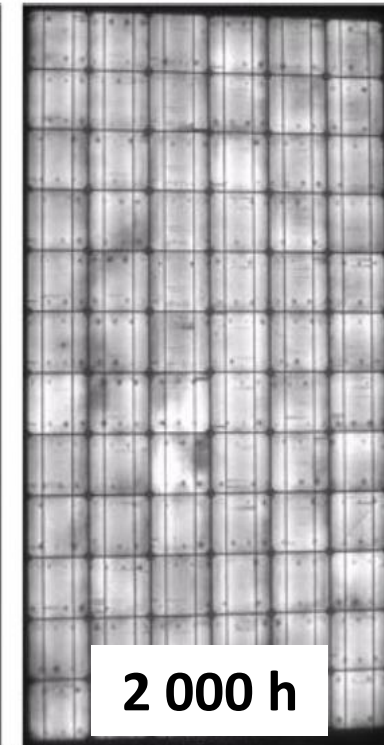
Exposed in a *Field* for ca. 30 Years



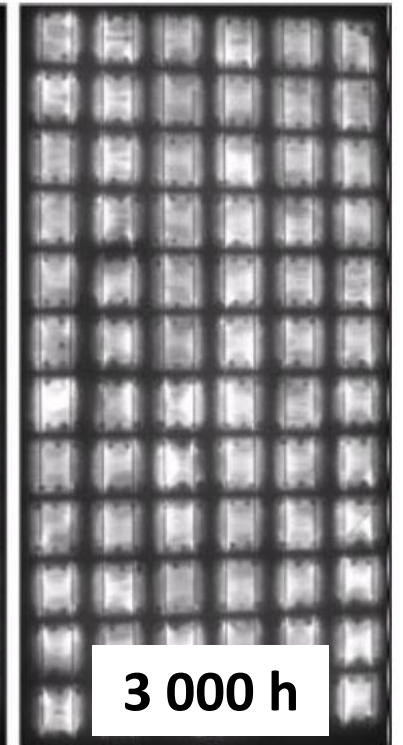
under *DH Stress Conditions*



1 000 h



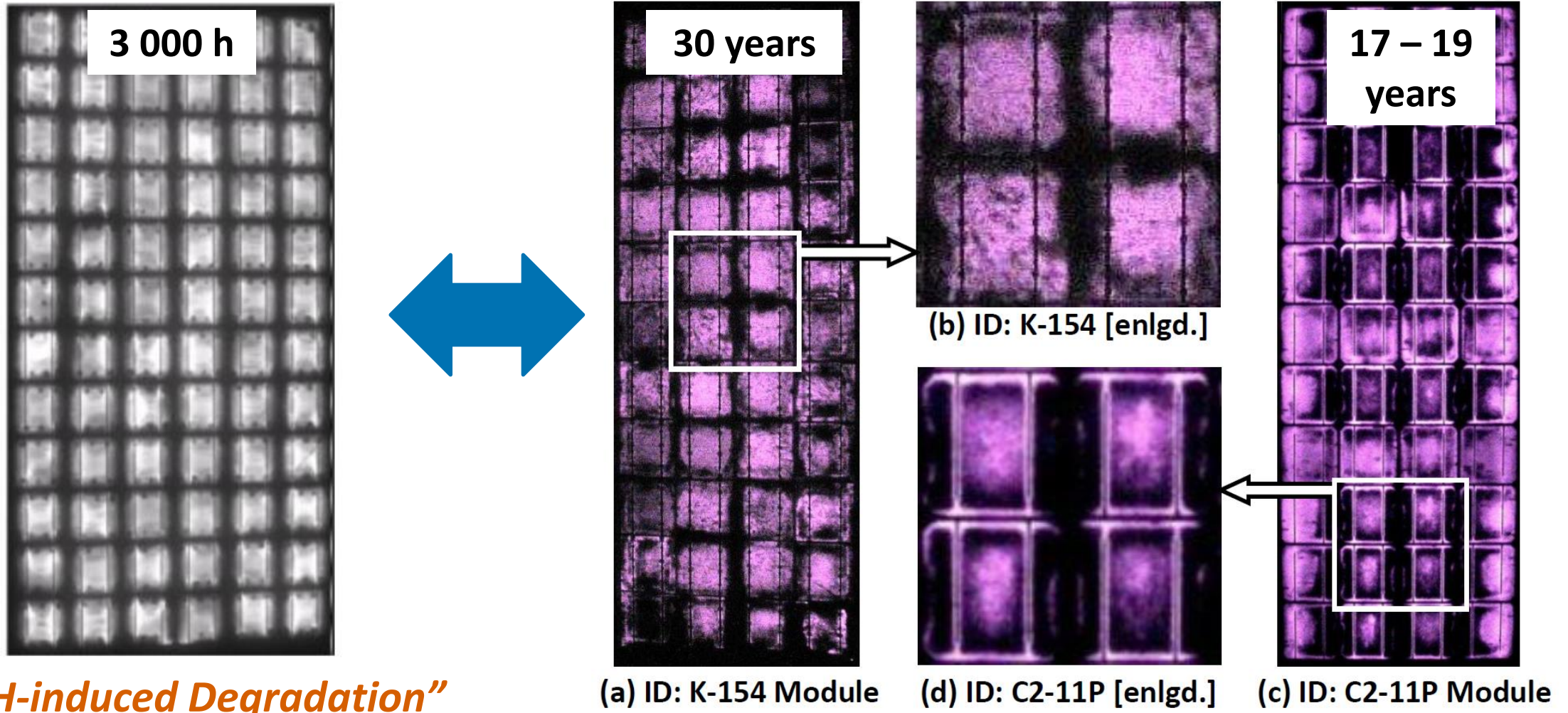
2 000 h



3 000 h

N. Bogdanski and W. Herrmann, in *Proc. 26th Eur. Photovolt. Sol. Energy Conf. Exhib.*, 2011, pp. 3093–3096.

However, we found **“DH-induced Degradation”-like EL appearance**  
 in some **PV modules exposed in fields.**



N. Bogdanski and W. Herrmann, in *Proc. 26th Eur. Photovolt. Sol. Energy Conf. Exhib.*, 2011, pp. 3093–3096.

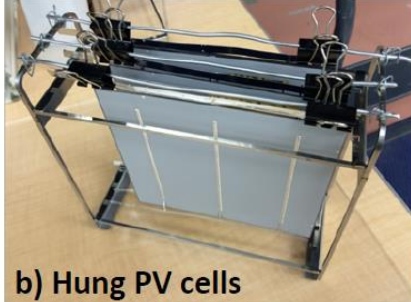
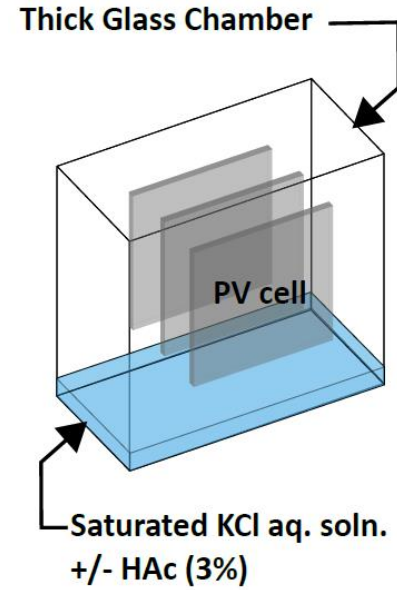
T. Tanahashi, Y. Hara, and A. Masuda, in *Proc. 33rd Eur. Photovolt. Sol. Energy Conf. Exhib.*, 2017, pp. 1462–1465.

Question?

These different EL appearances are induced by  
a common corrosion mechanism or not?

# We have 3 Experimental Procedures on Corrosion (HAc = Acetic Acid)

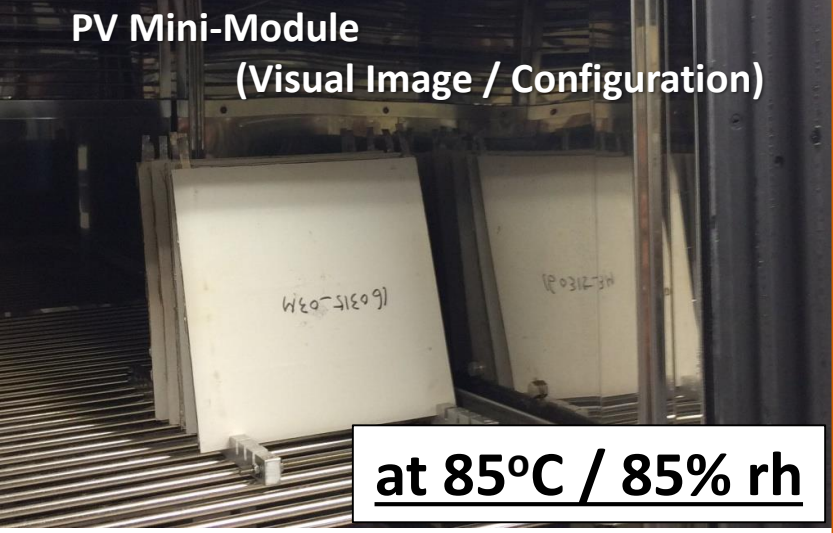
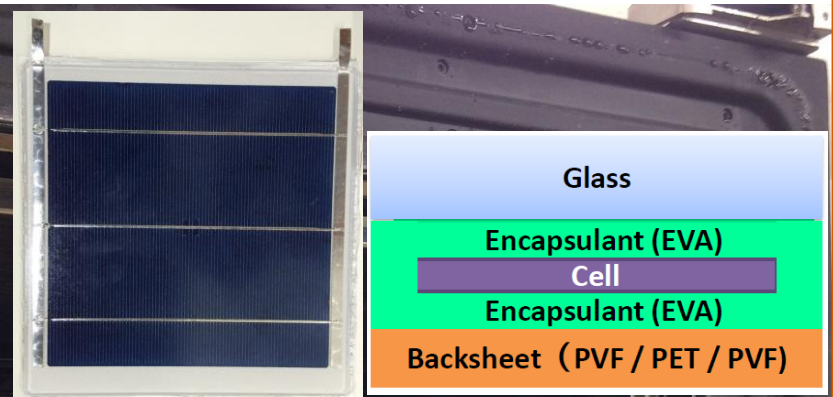
## HAc-Vapor Exposure of Bare PV Cells



**at 85°C / 80% rh**

T. Tanahashi et al., "Localization and characterization of a degraded site in crystalline silicon photovoltaic cells exposed to acetic acid vapor," *IEEE J. Photovolt.*, vol. 8, no. 4, pp. 997–1004, Jul. 2018.

## DH Stress Test of PV Modules



## This Presentation

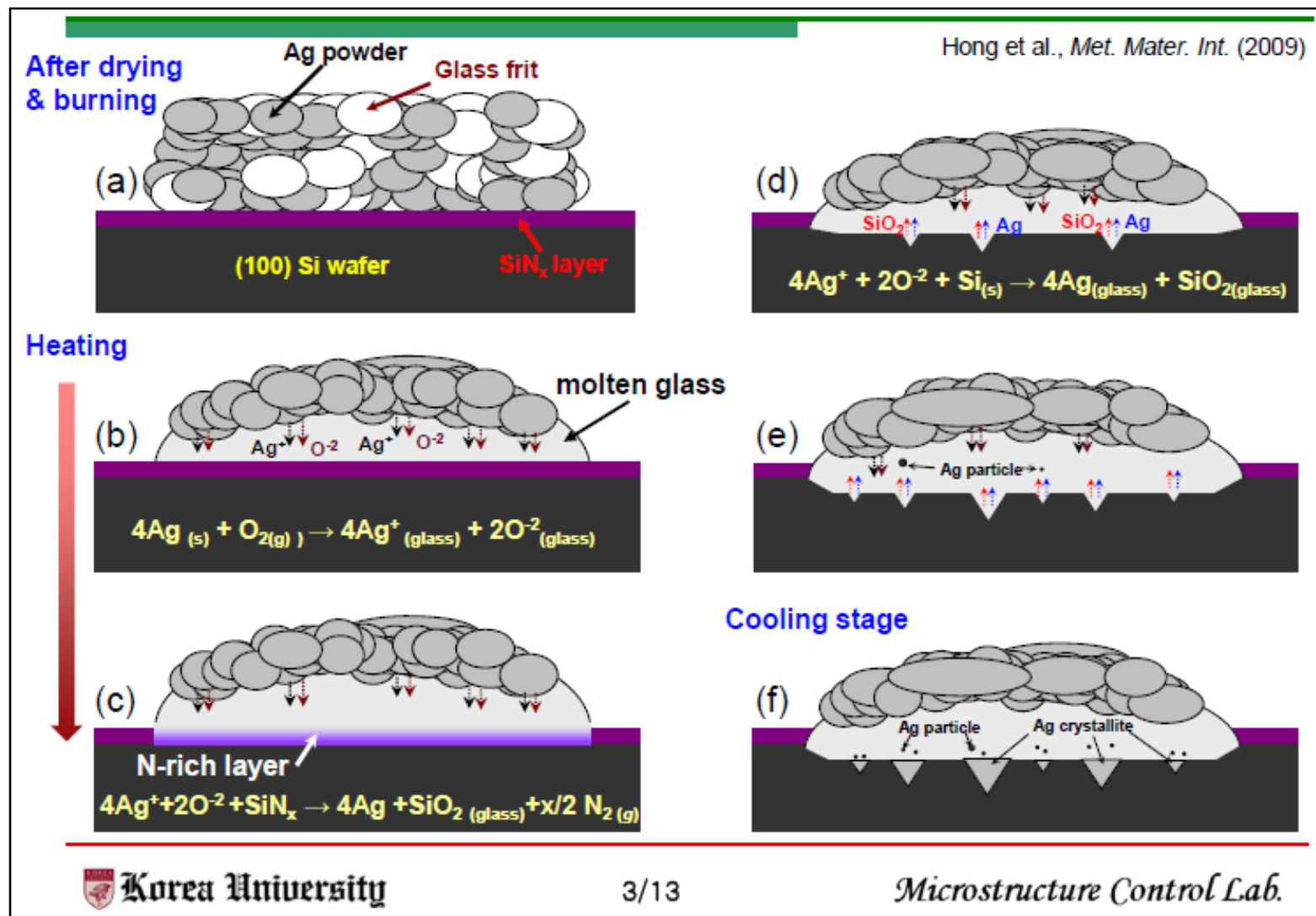
## Outdoor Exposure



**Ex. Outdoor Exposed PV Module from 1994 in Cfa Climate**

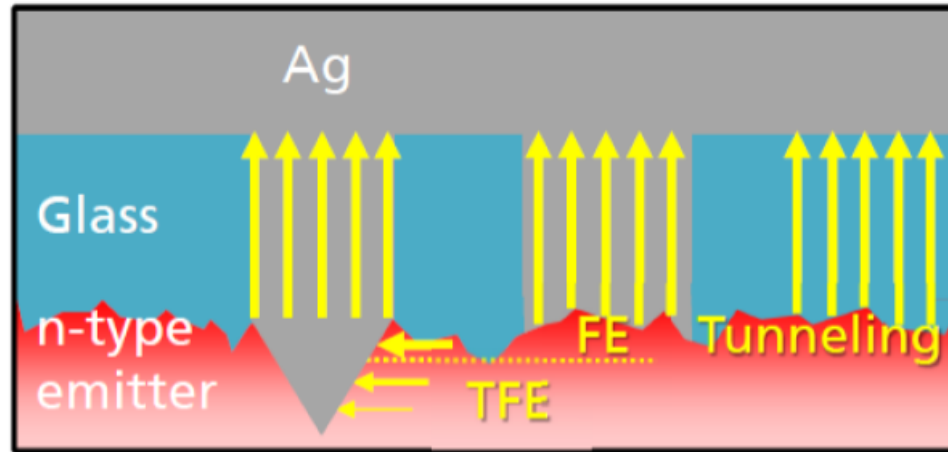
T. Tanahashi et al., "Corrosion-induced AC impedance elevation in front electrodes of crystalline silicon photovoltaic cells within field-aged photovoltaic modules," *IEEE J. Photovolt.*, vol. 9, no. 3, pp. 741–751, 2019.

# Silver Contact Formation during “Fire-Through” Process



Chou, S.-B., et al. “Effect of forming gas annealing on screen-printed Ag metallization of silicon solar cells”, 5th Metallization Workshop (20-21 October, 2014)

## Proposed Current Transport Mechanisms in Silver Contact<sup>1)</sup>



### Field Emission (FE)

$$N_D \geq 10^{20} \text{ cm}^{-3}$$

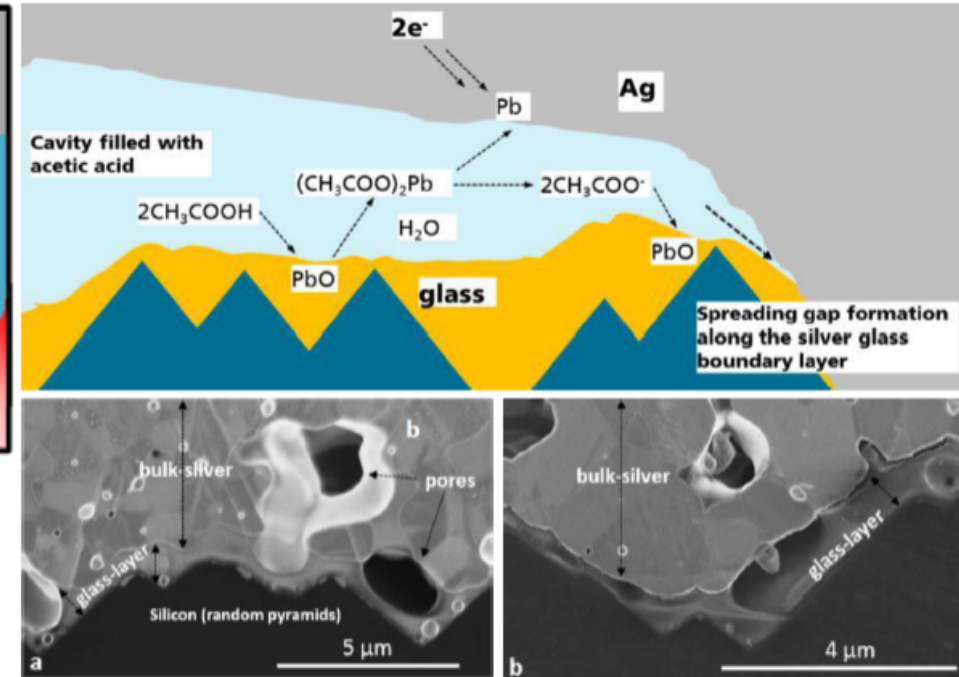
### Thermionic Field Emission (TFE)

$$10^{17} \text{ cm}^{-3} < N_D < 10^{20} \text{ cm}^{-3}$$

### Electron Tunneling

through glass layer  
(directly or *via* nano-Ag colloids)

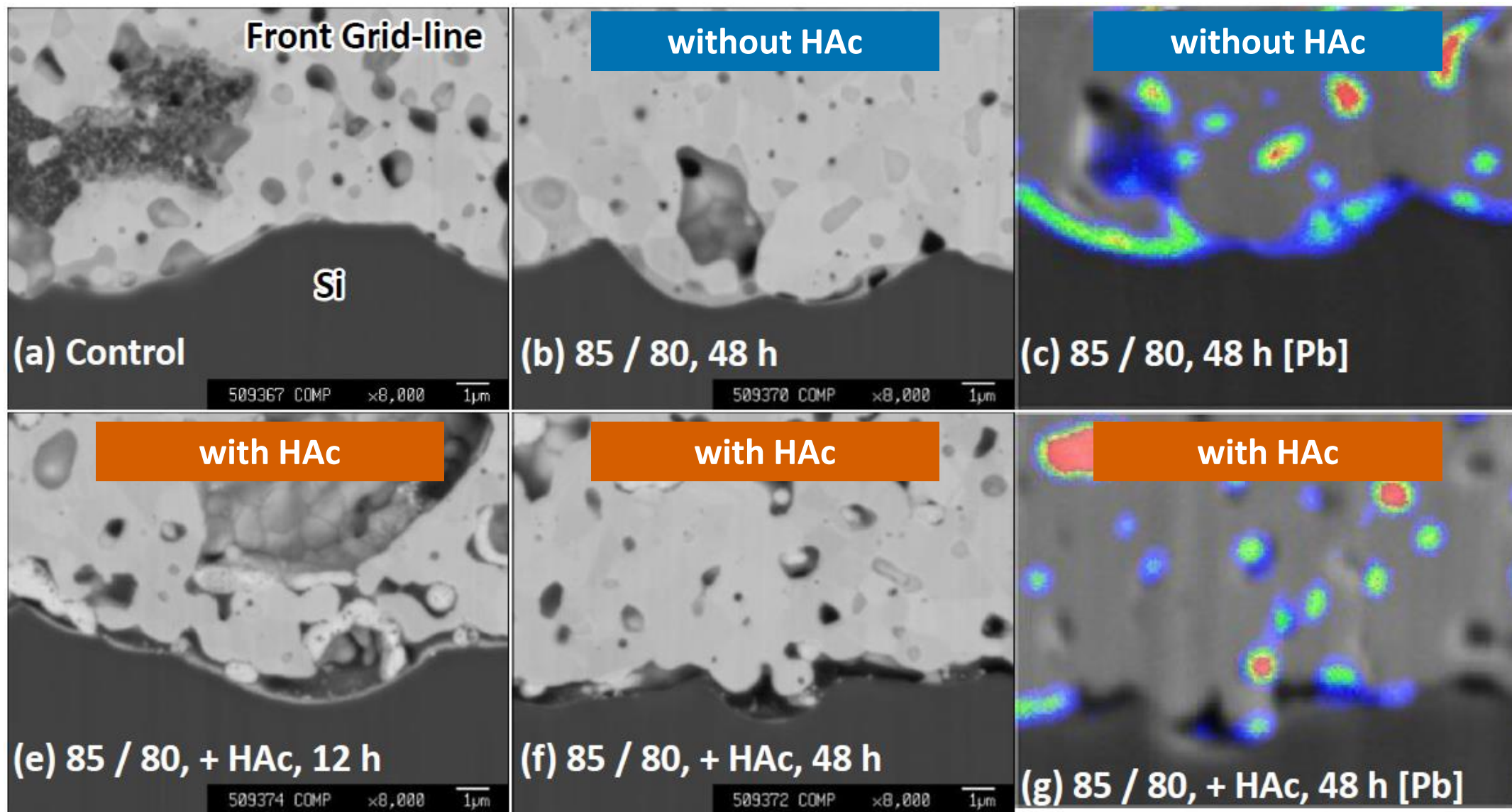
## Dissolution of Glass-Silver Boundary Layer by Acetic Acid<sup>2)</sup>



- 1) R. Hoenig et al., “Macroscopic and Microscopic Electrical Behavior of Screen Printed Silver Contacts to Phosphorus-Doped Emitters”, presented at 5th Metallization Workshop, 2014.
- 2) A. Kraft et al., “Investigation of Acetic Acid Corrosion Impact on Printed Solar Cell Contacts”, IEEE J. Photovolt. 5 (3): 736-743, 2015.

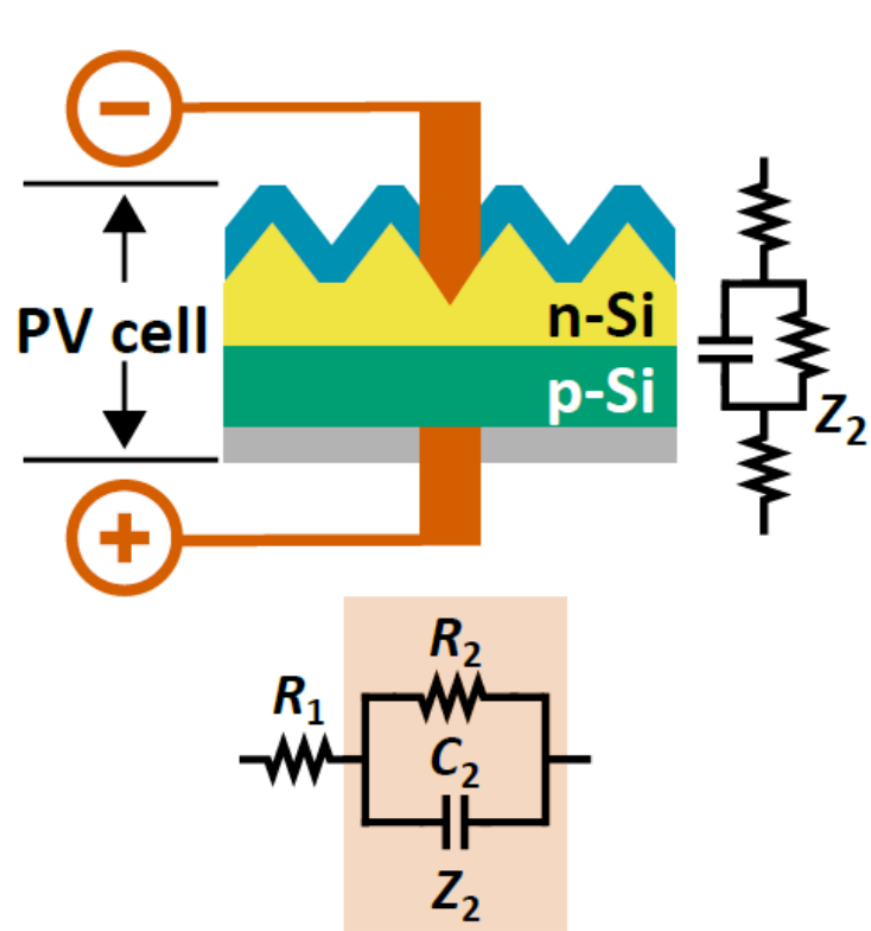


# Evolution of Gap at Ag-Si Interface (HAc-Vapor Exposure)

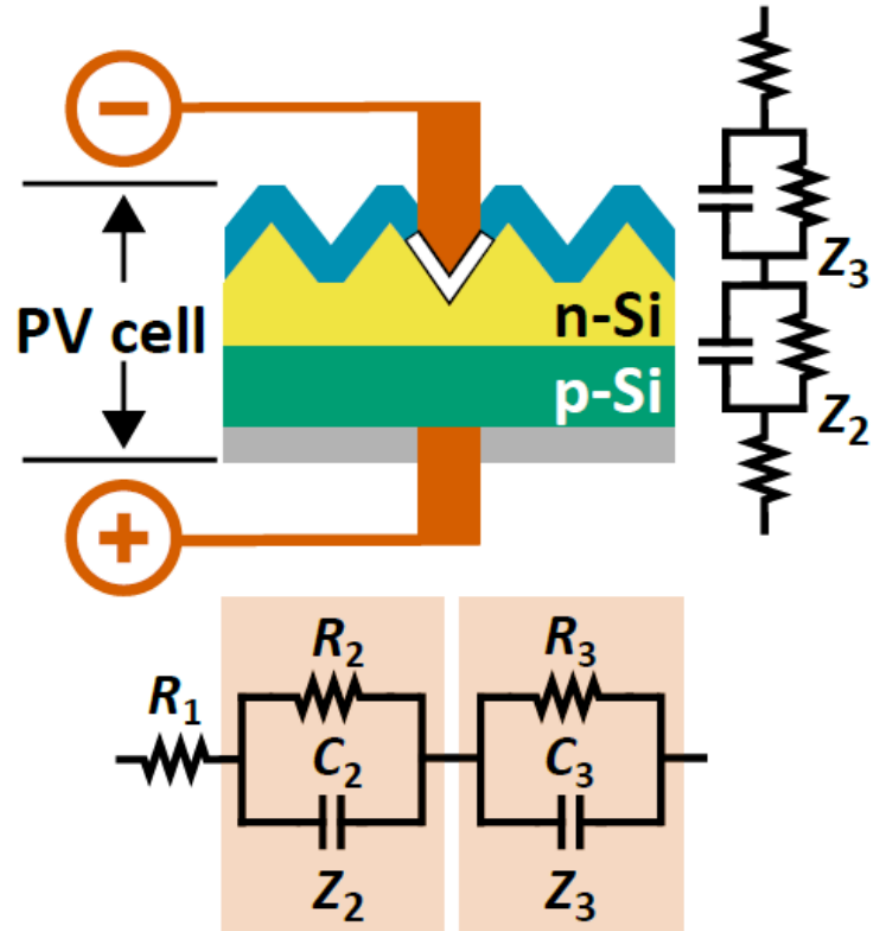


# Detection of Corrosion-induced AC Impedance Elevation

a) Intact Contact

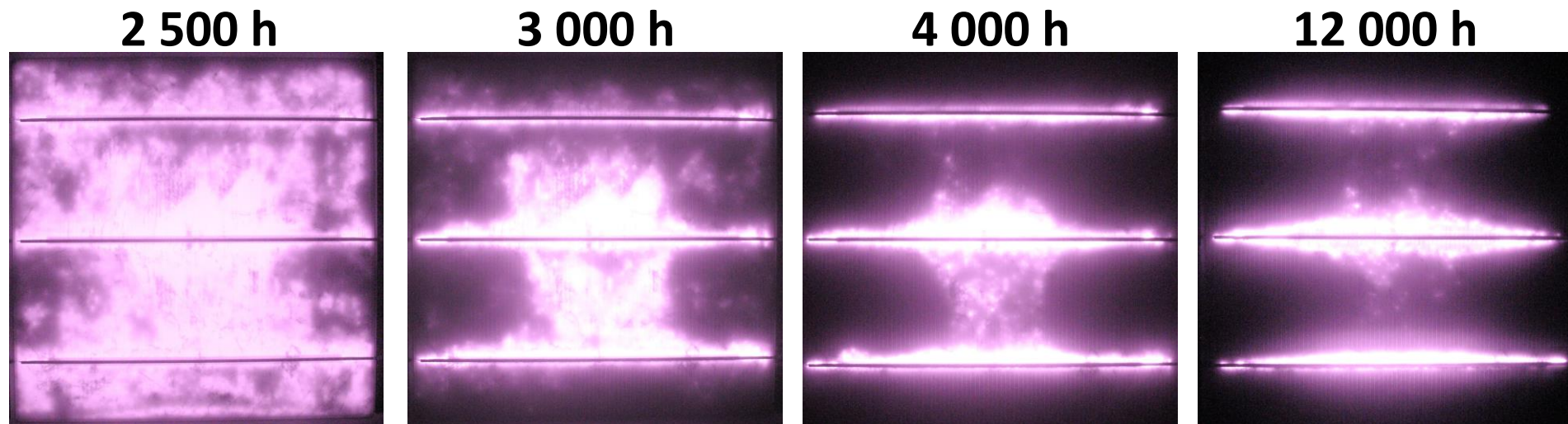


b) Corroded Contact

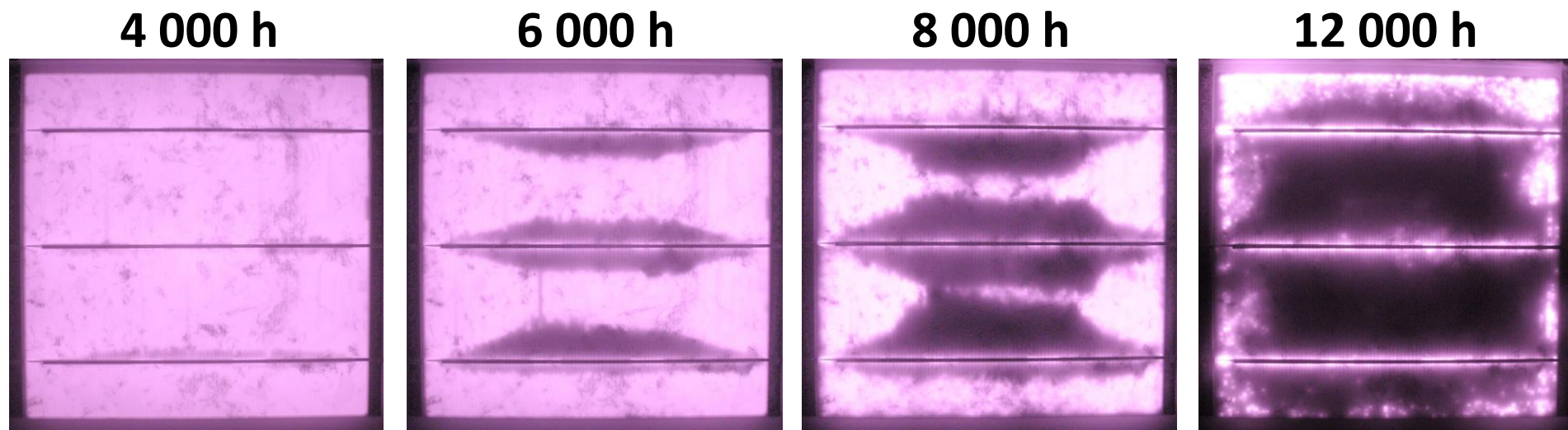


# DH Stress Test of PV Modules Evolution of EL Image

Module with Cell A

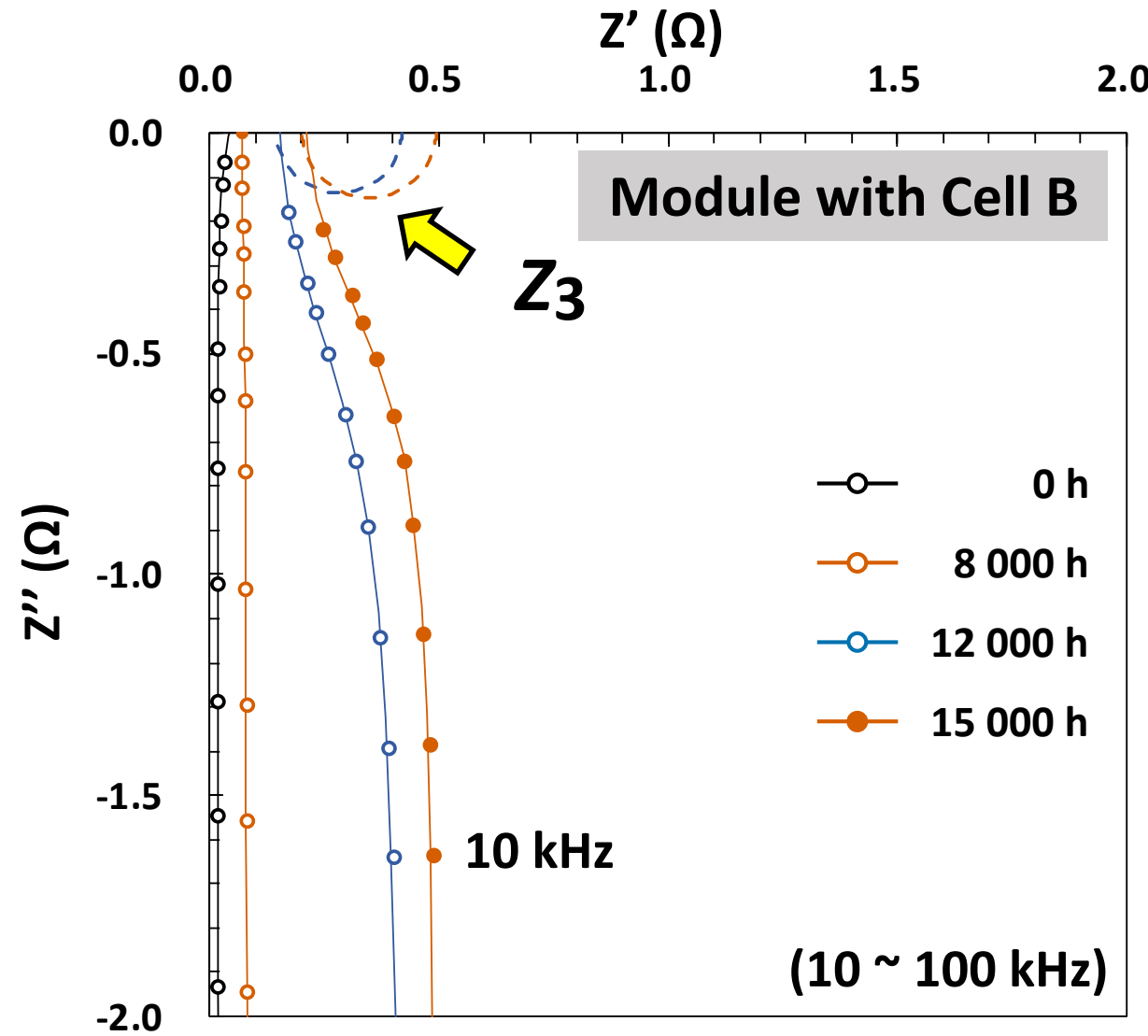
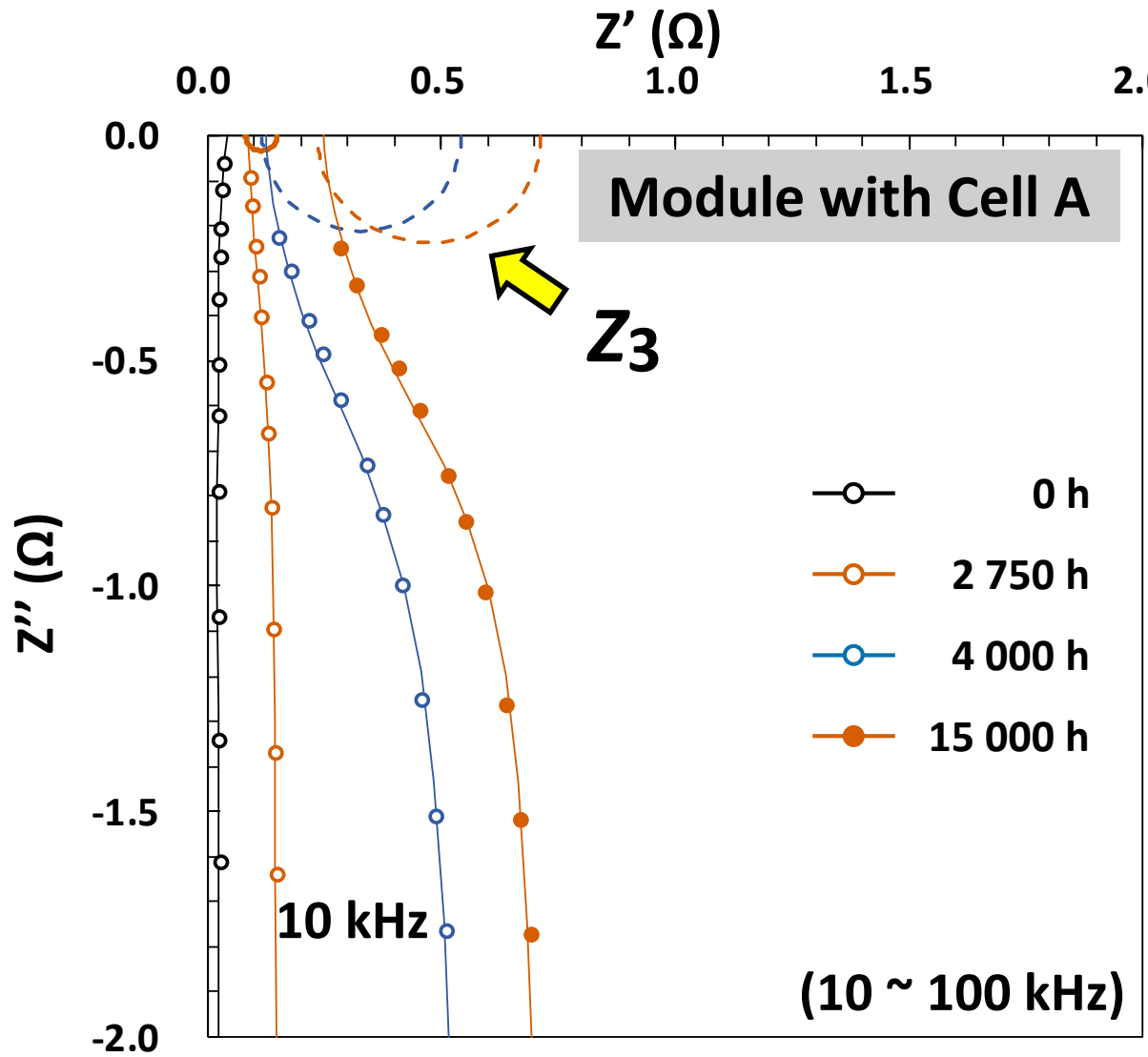


Module with Cell B



DH Stress Test of PV Modules

Emergent Incidence & Evolution of  $Z_3$



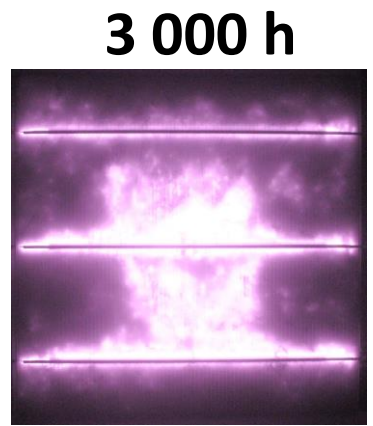
# DH Stress Test of PV Modules

## Evolution of Elec. Parameters

Module with Cell A

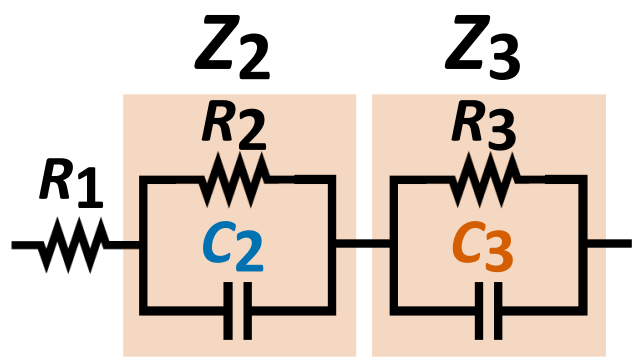
### Synchronized Changes

- FF /  $P_m$ : Reduction
- $R_1$  /  $R_3$ : Elevation
- $C_3$ : Emergent Expression / Decay

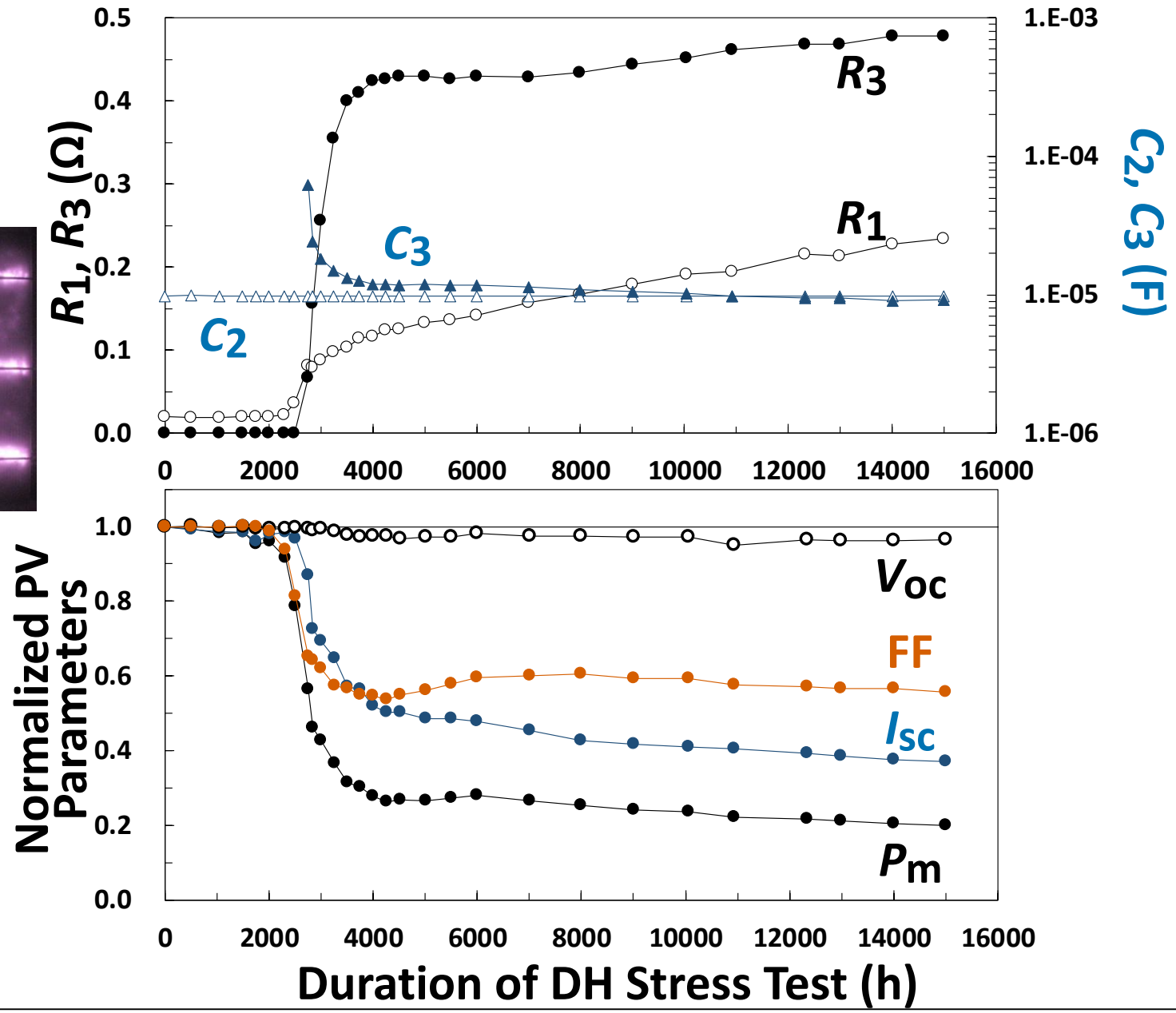


Constant

- $C_2$



AC Equivalent Circuit



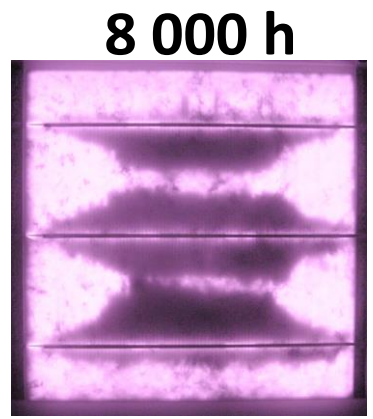
# DH Stress Test of PV Modules

## Evolution of Elec. Parameters

Module with Cell B

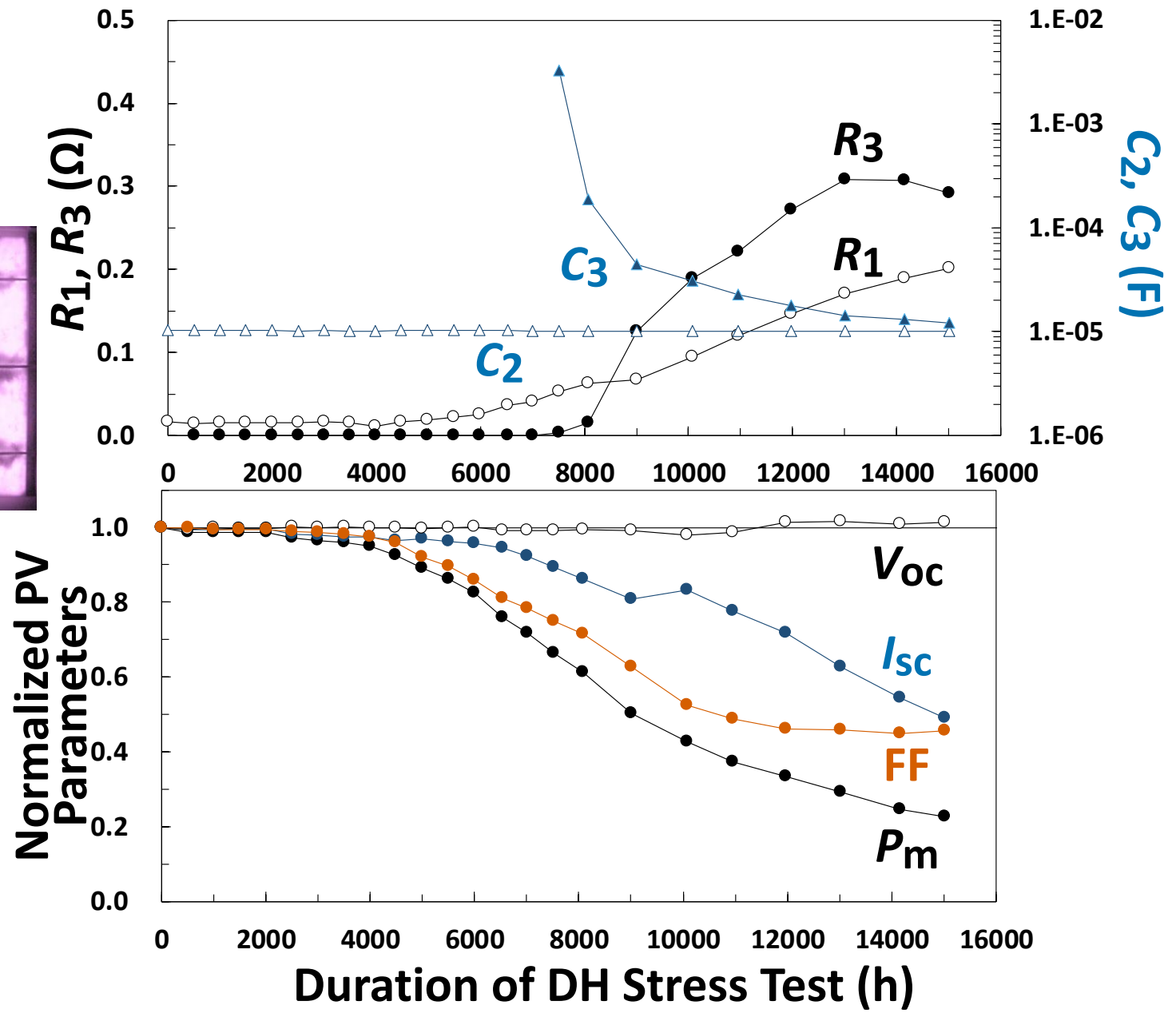
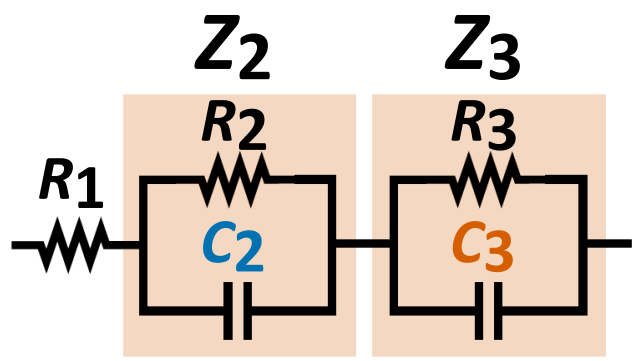
### Synchronized Changes

- FF /  $P_m$ : Reduction
- $R_1$  /  $R_3$ : Elevation
- $C_3$ : Emergent Expression / Decay



Constant

- $C_2$

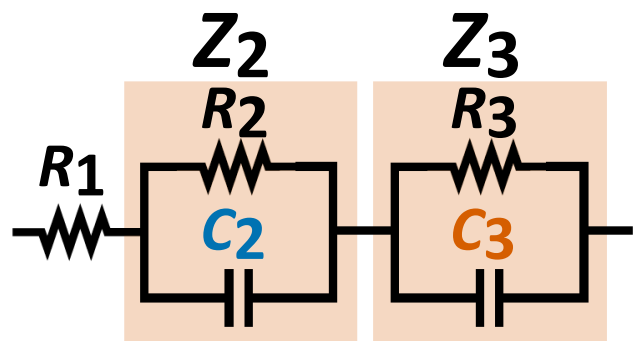


# DH Stress Test

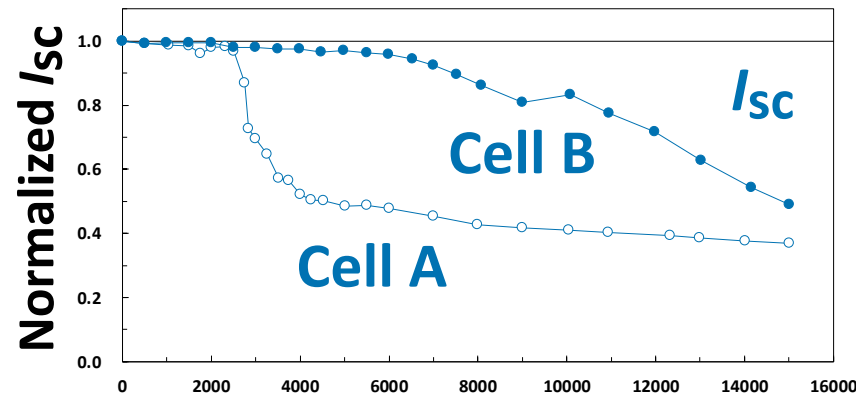
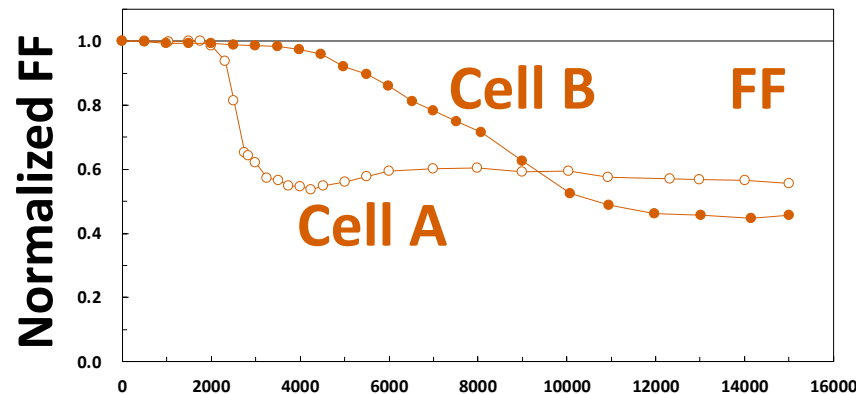
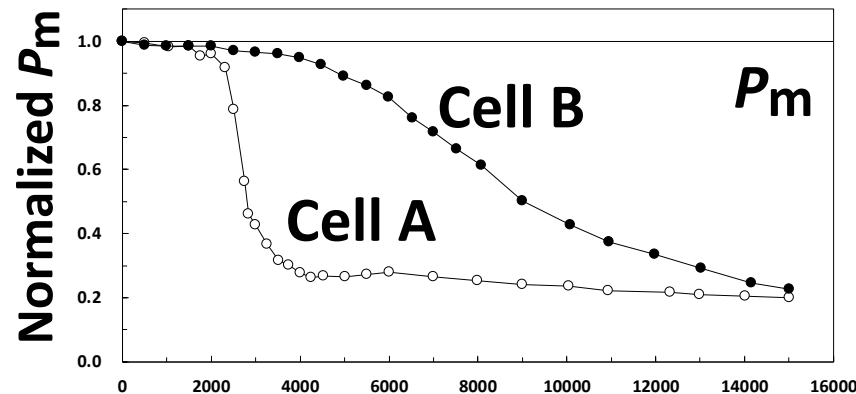
Module with Cell A

Module with Cell B

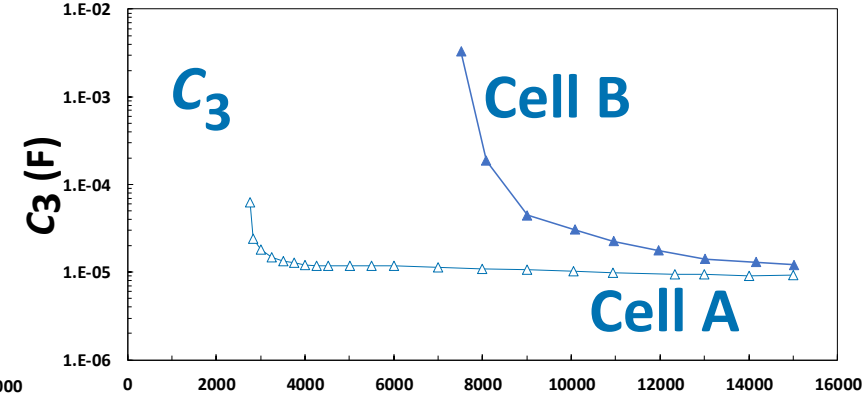
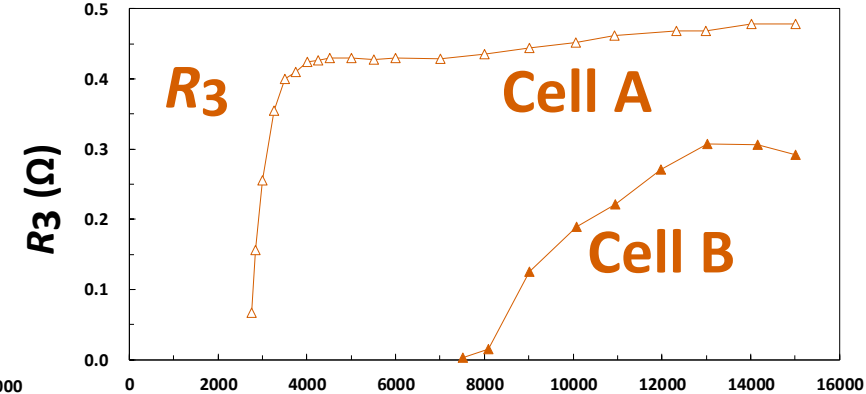
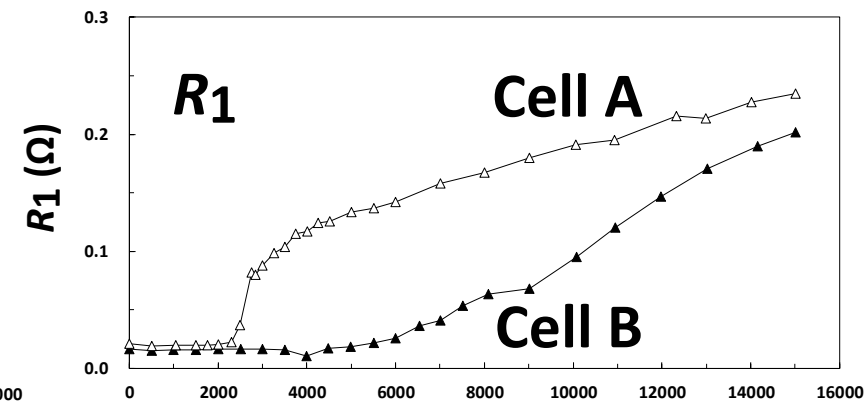
## Complete Differences in Degradation Kinetics



AC Equivalent Circuit



Duration of DH Stress Test (h)

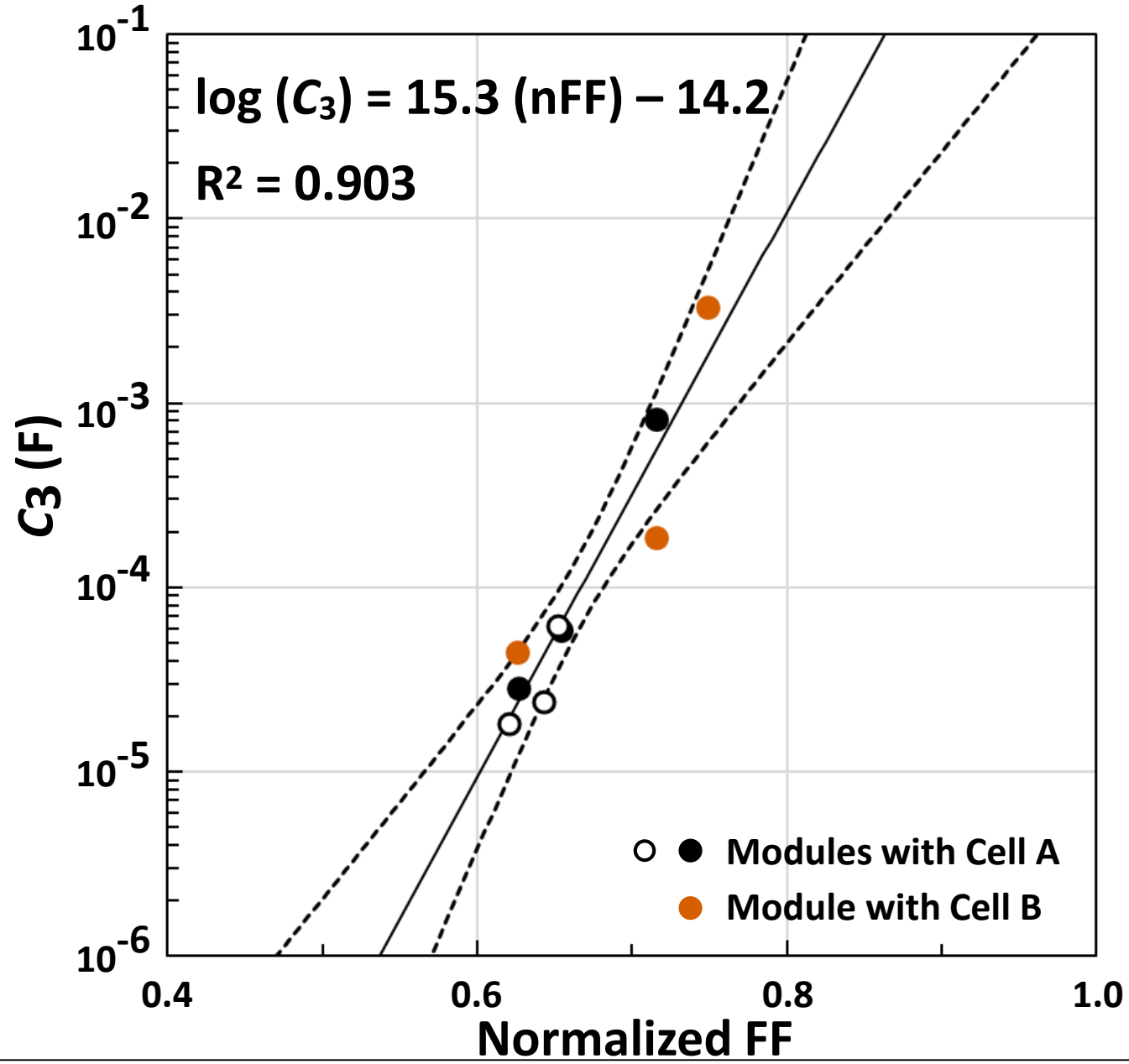
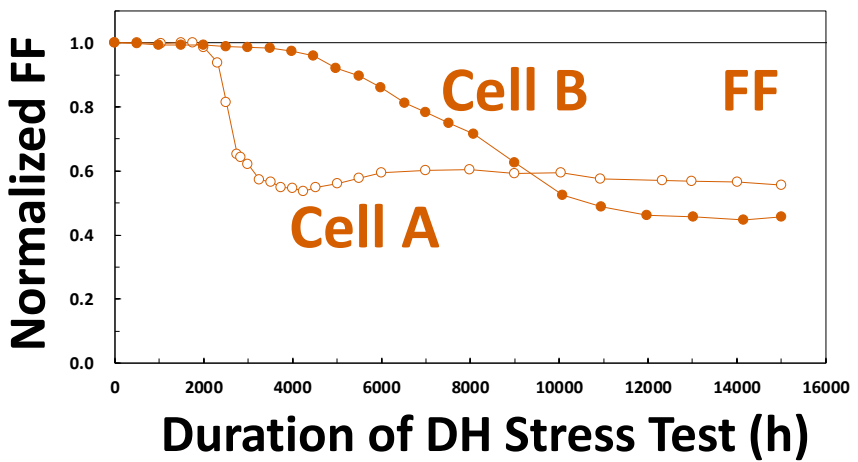


# DH Stress Test of PV Modules

## Correlation of $C_3$ with FF-Loss

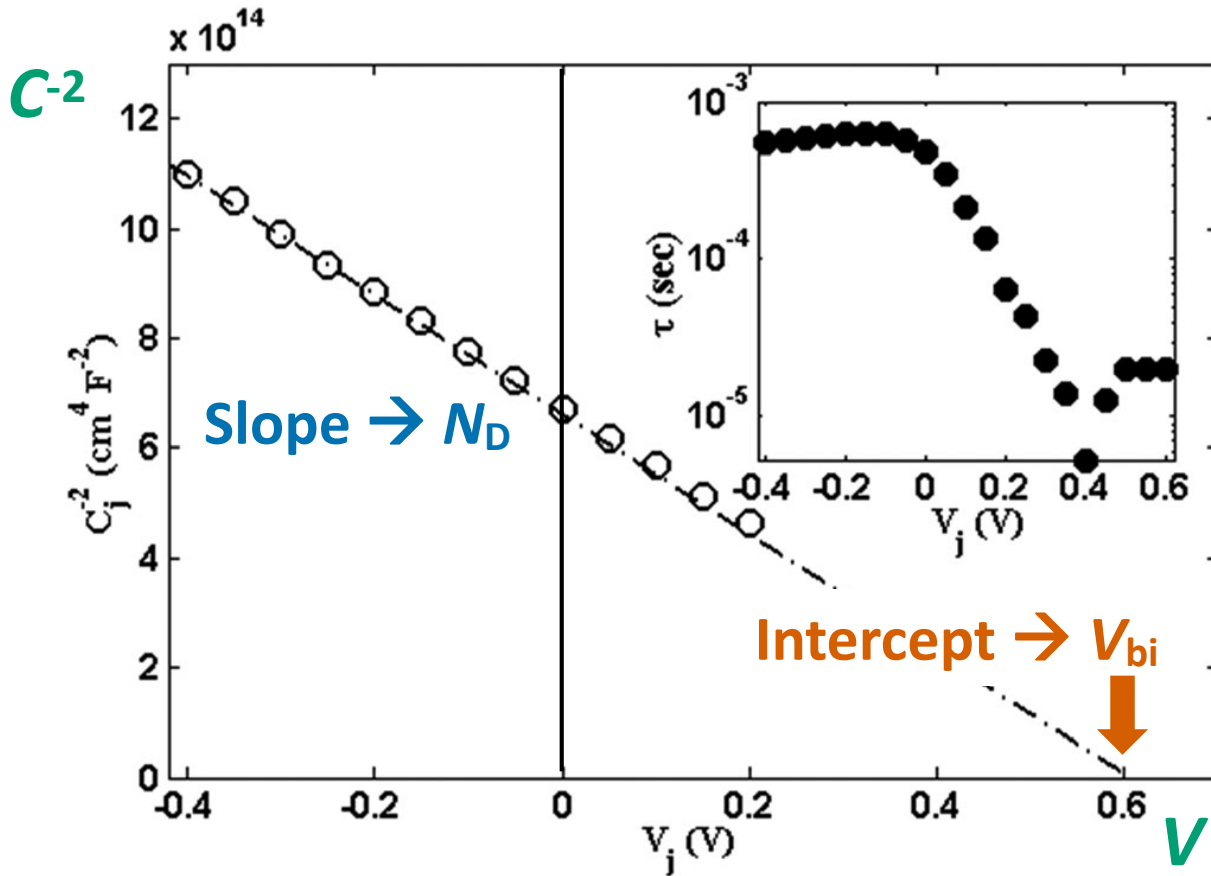
In both PV modules,  
FF-loss depends on  $C_3$  intensity

Capacitor Formation / Evolution  
 $\approx$  Gap / Dielectric Formation  
 in Si-Metallization Interface





# Mott-Schottky Plot



## Mott-Schottky plot for a c- Si solar cell

The inset shows the variation of the minority carrier lifetime as a function of the applied bias.

P. Yadav et al., *Phys. Chem. Chem. Phys.*, 16 (29):15469–15476, 2014.

$$C^{-2} = \frac{2}{qA^2 \epsilon N_D} (V + V_{bi})$$

$$N_D = \frac{2}{q\epsilon A^2 \left[ \frac{dC^{-2}}{dV} \right]}$$

$C$ : Capacitance

$V$ : Applied DC Voltage

$\epsilon$ : Permittivity

$q$ : Elementary Charge

$N_D$ : Doping Density

$V_{bi}$ : Build-in Potential

$A$ : Area

# DH Stress Test of PV Modules

# Mott-Schottky Plots [ $C_2$ ]

$V_{bi}$  :

Cell A =  $0.677 \pm 0.005$  V

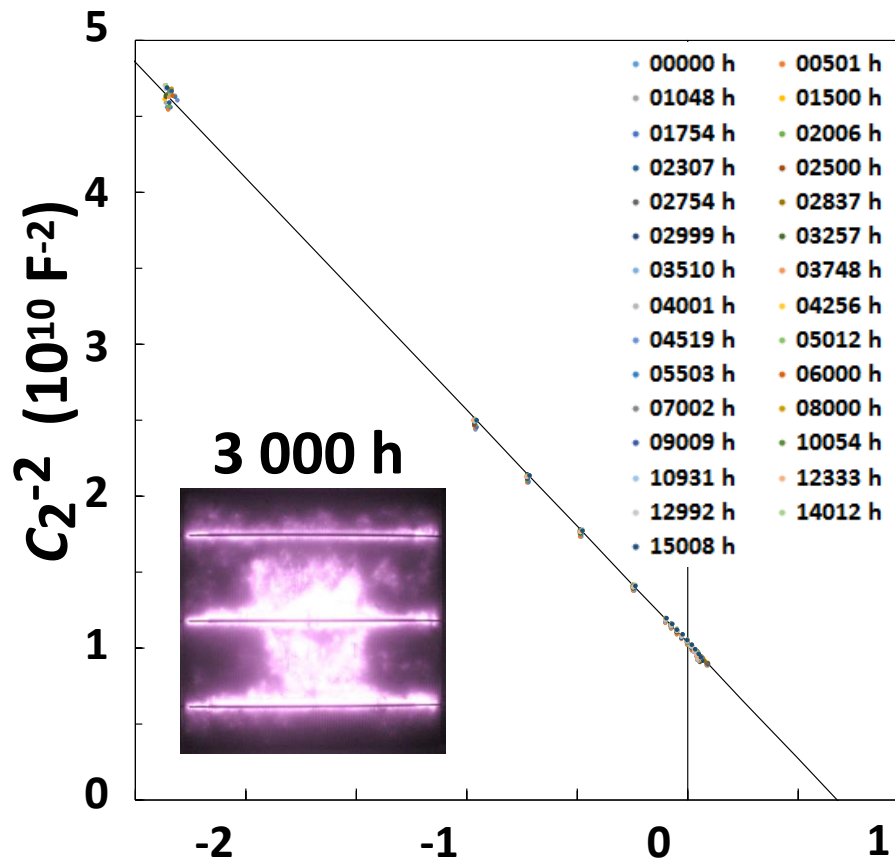
Cell B =  $0.636 \pm 0.021$  V

$N_D$  :

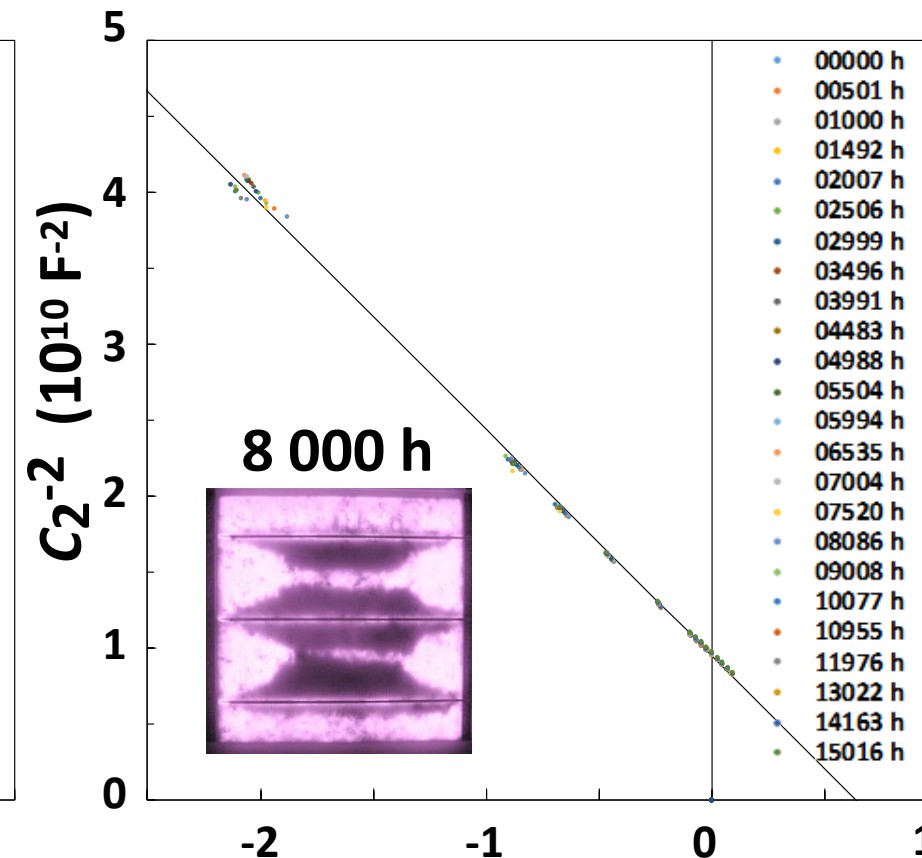
Cell A =  $1.33 \times 10^{16} \text{ cm}^{-1}$   
( $1.32 - 1.35 \times 10^{16}$ )

Cell B =  $1.37 \times 10^{16} \text{ cm}^{-1}$   
( $1.34 - 1.40 \times 10^{16}$ )

Module with Cell A



Module with Cell B



Applied DC Voltage (V)

Elec. Characteristics in p-n Junction: Const.

# DH Stress Test of PV Modules

# Mott-Schottky Plots [ $C_3$ ]

$C_3$ : non-Linear

$$C_3^{-2} = \alpha \exp(-\beta V) + \gamma$$

$\alpha$ : Reduction

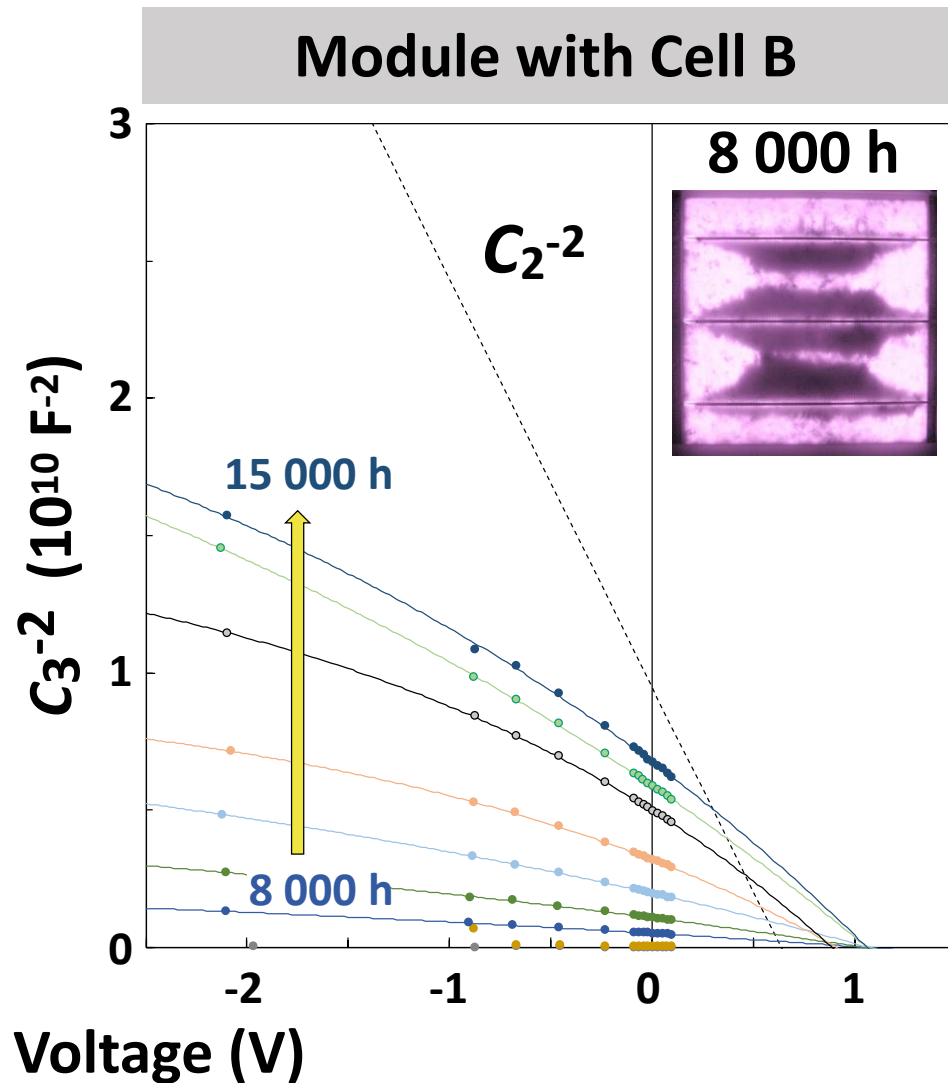
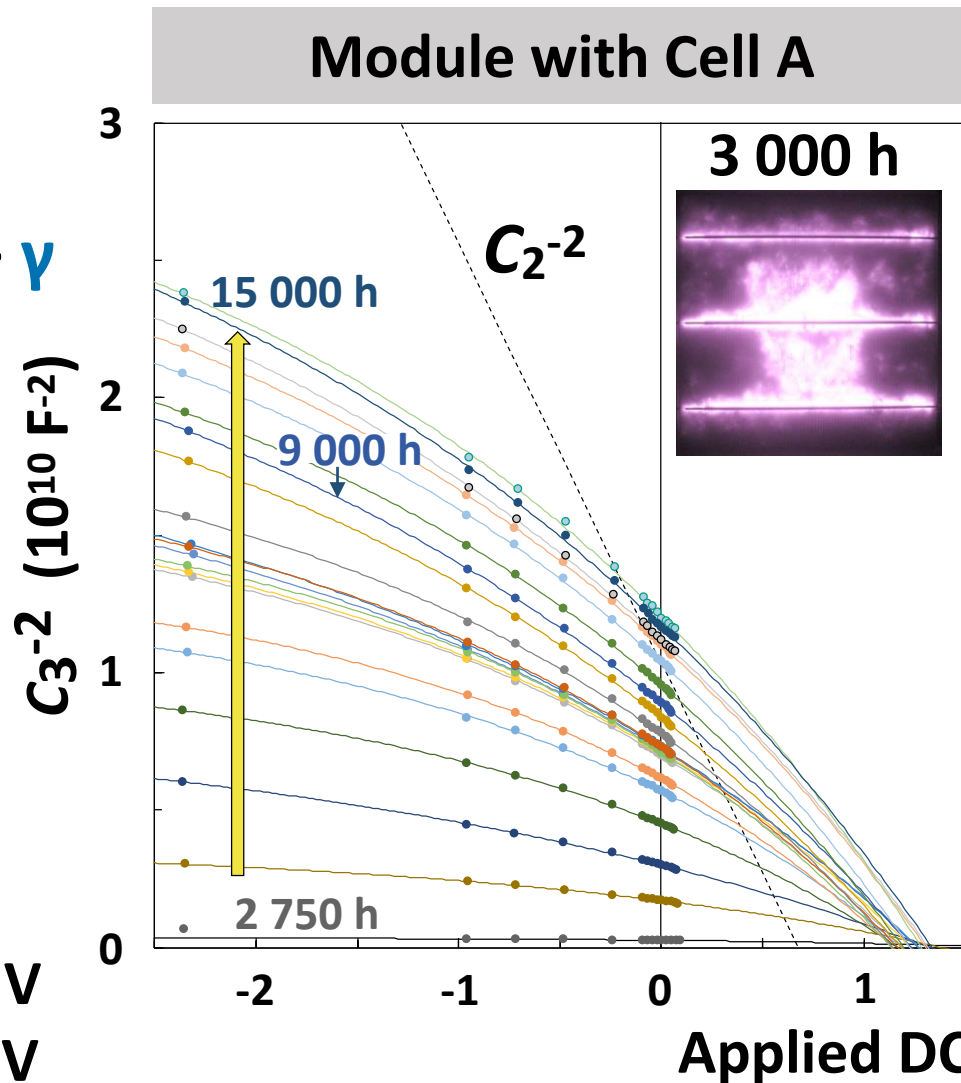
$\beta$ : nearly Const.

$\gamma$ : Elevation

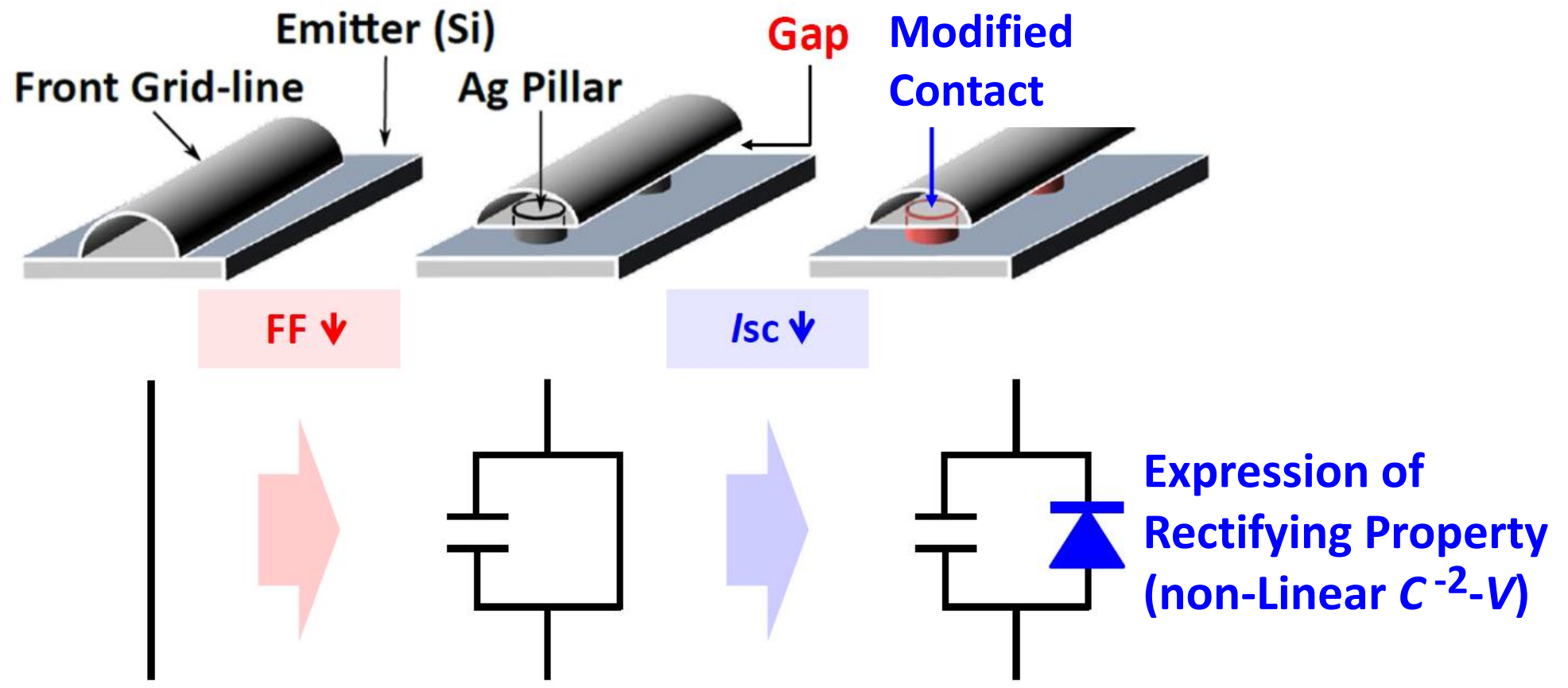
$V_{bi}$  :

Cell A =  $1.233 \pm 0.072$  V

Cell B =  $1.010 \pm 0.077$  V



# Degradation Mechanism / Model in Both Modules

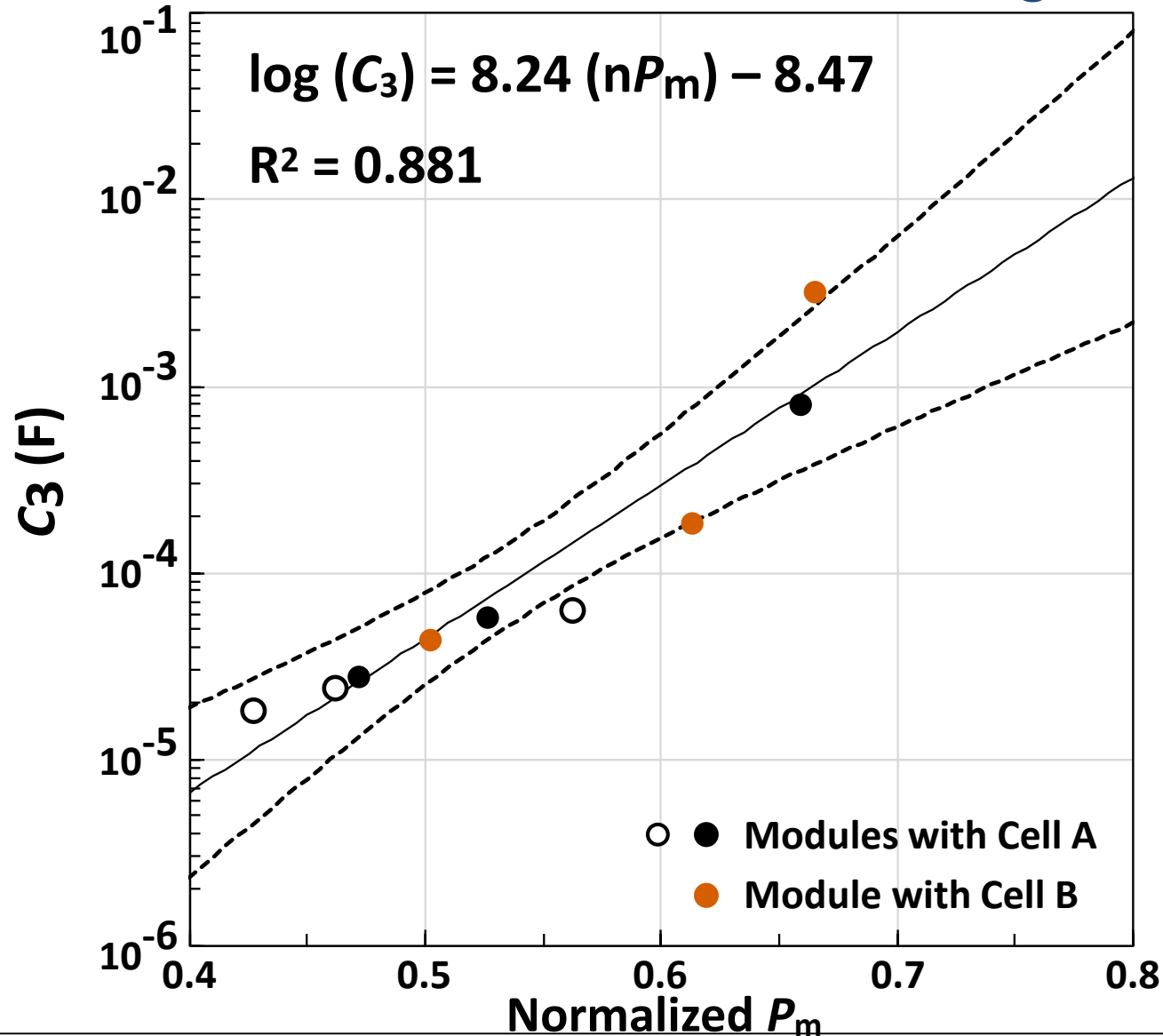


$$\log (C_3) = p (nFF) - q$$

$$C_3^{-2} = \alpha \exp(-\beta V) + \gamma$$

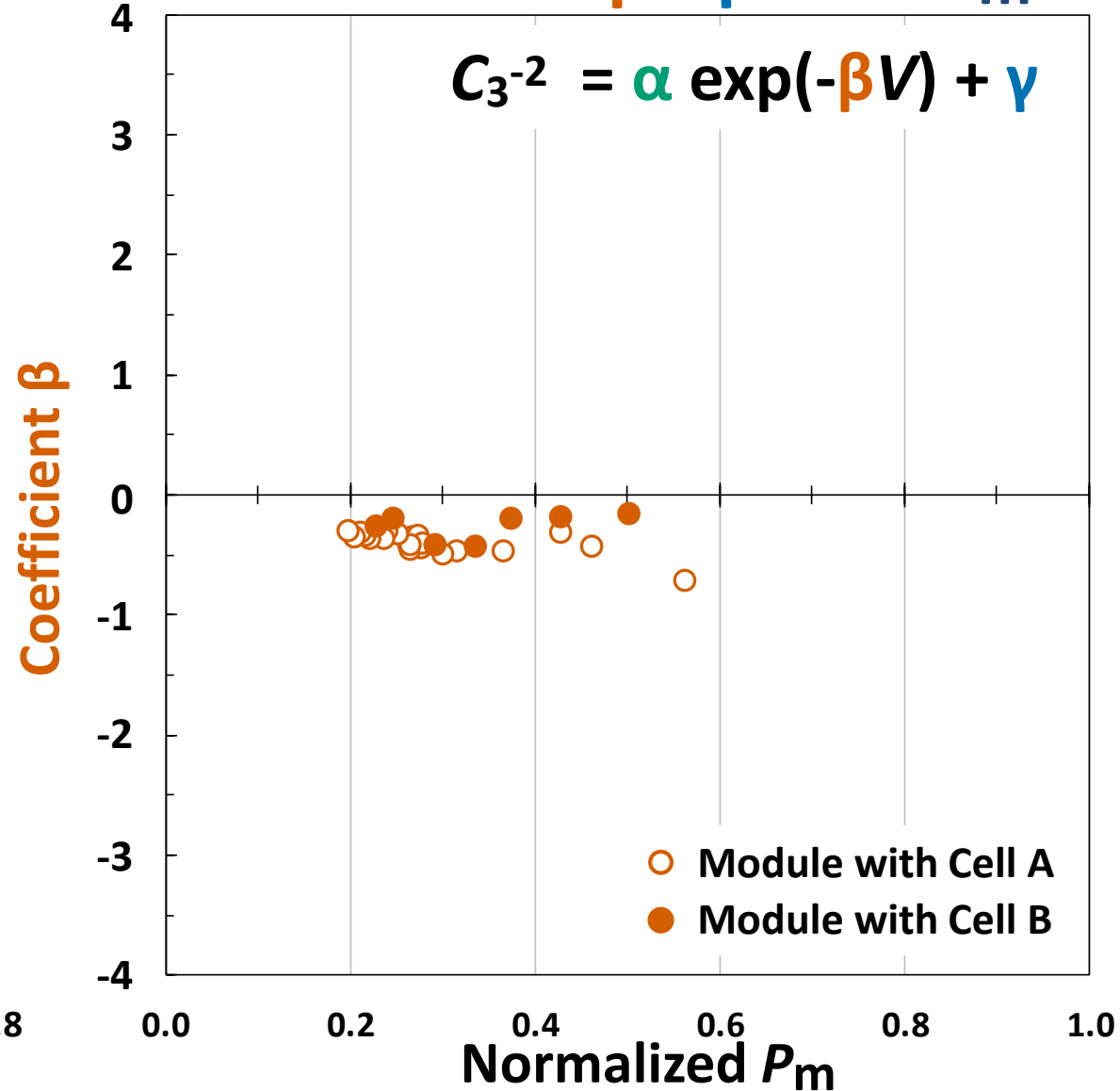
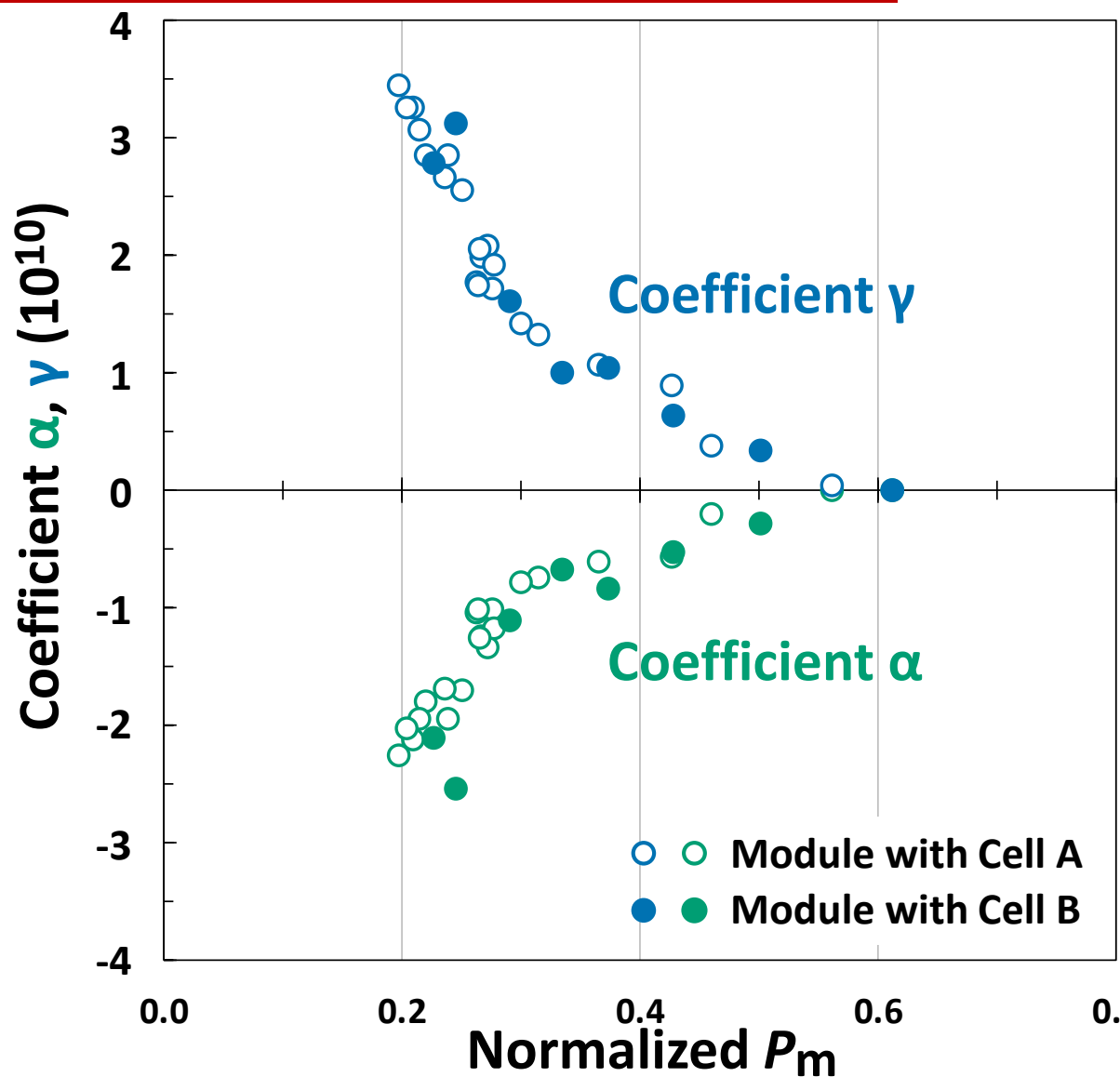
DH Stress Test of PV Modules

Correlation of  $C_3$  with  $P_m$ -Loss



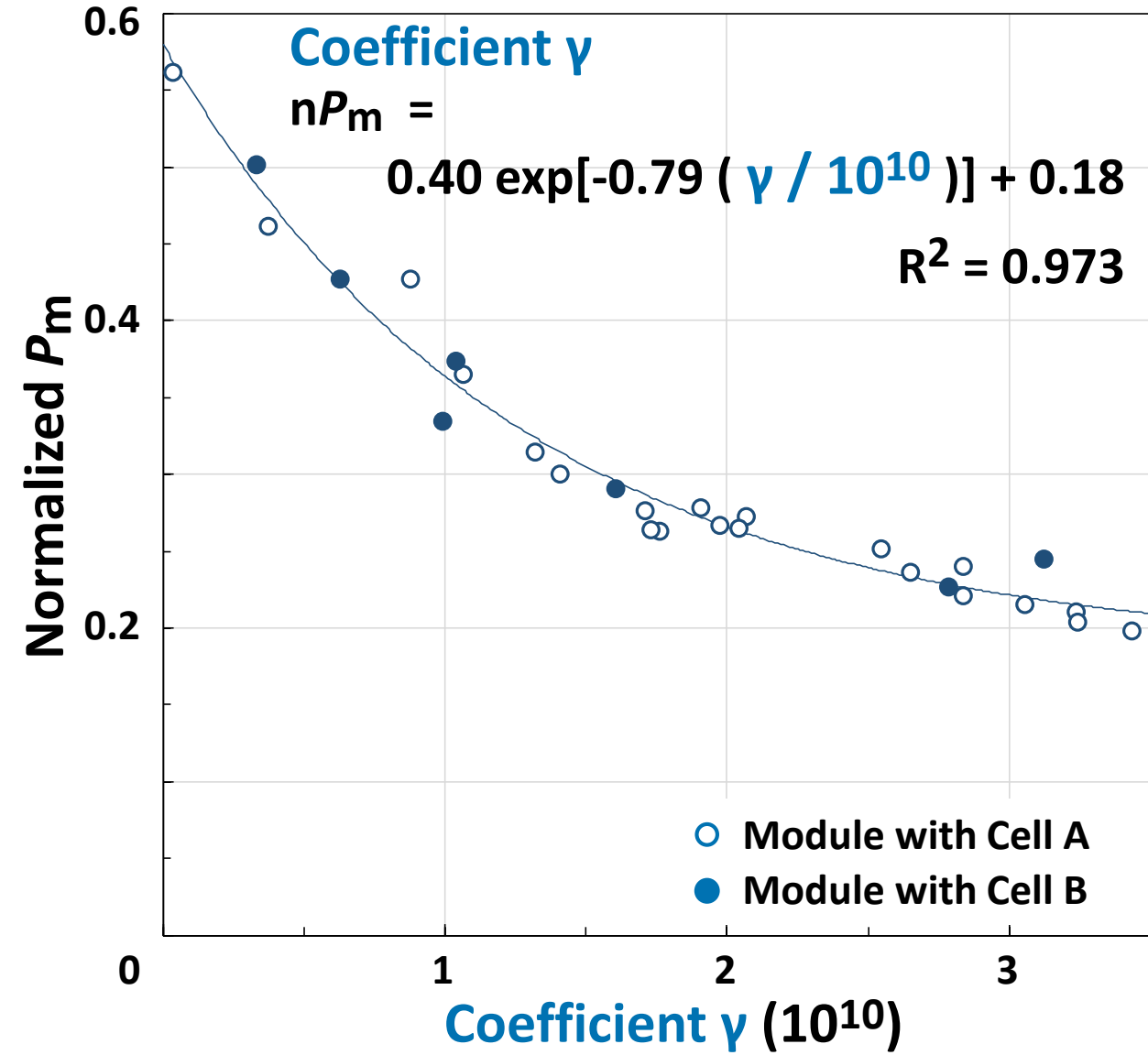
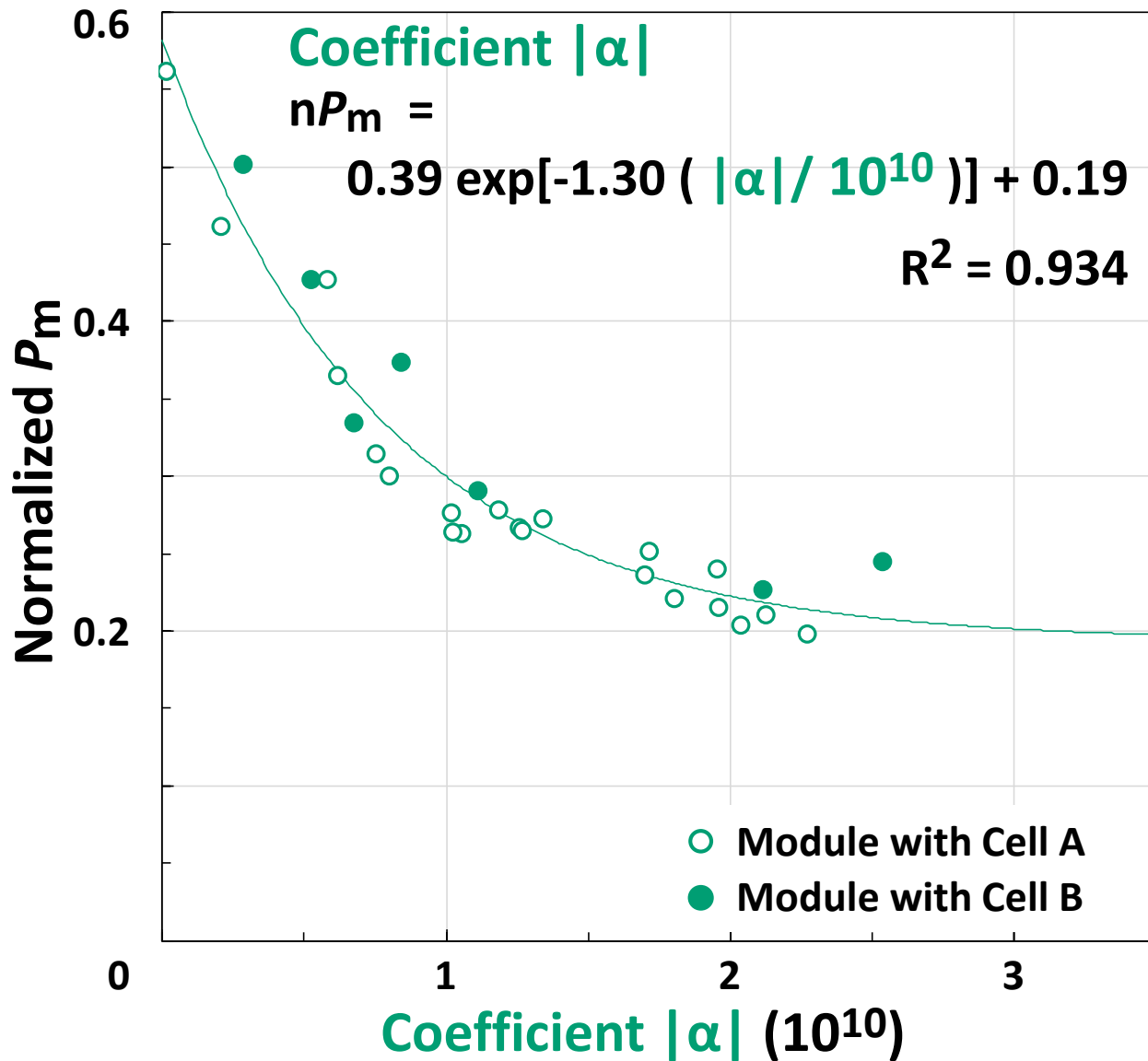
# DH Stress Test of PV Modules

## Correlation of Coeff. $\alpha \cdot \beta \cdot \gamma$ with $P_m$ -Loss

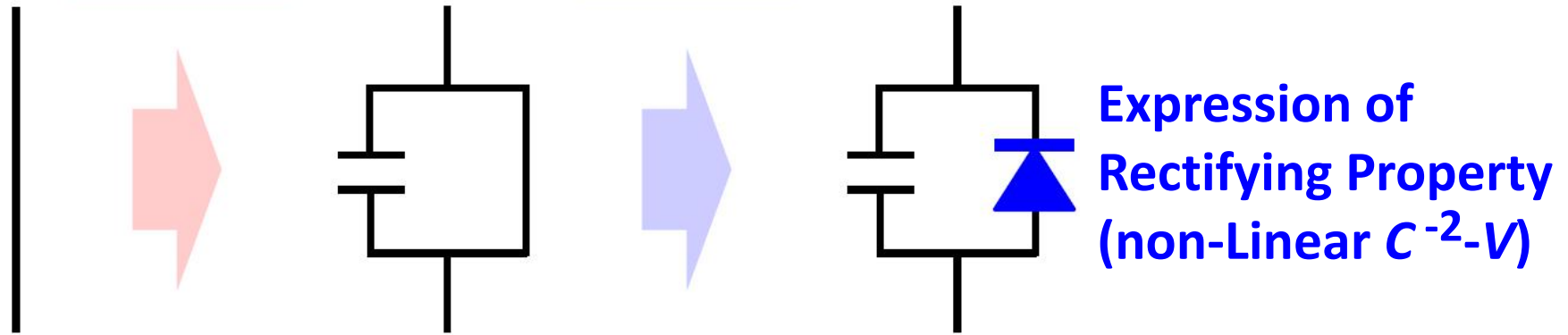
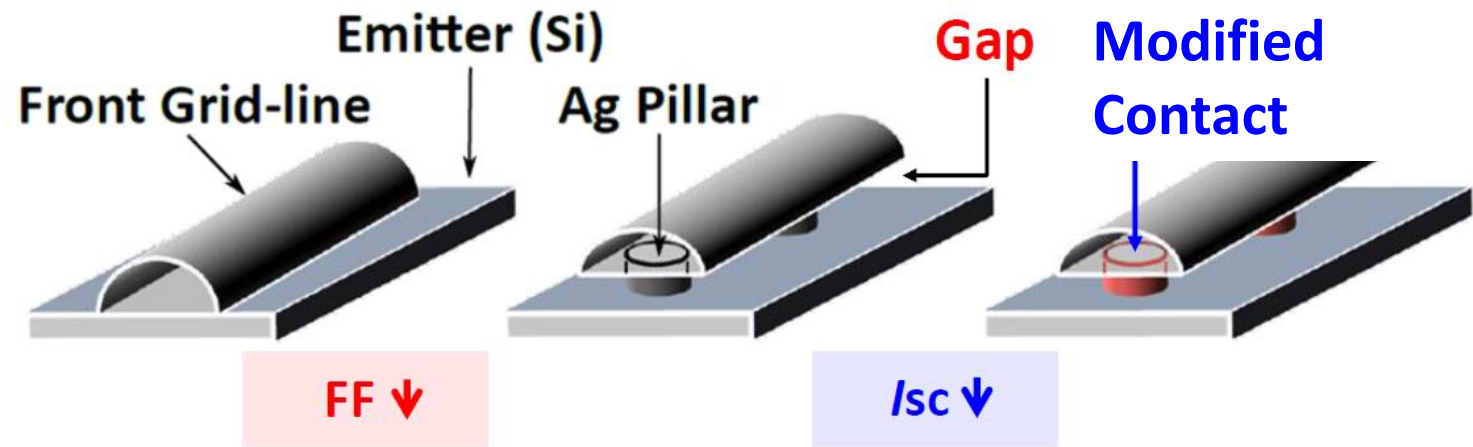


# DH Stress Test of PV Modules

## Correlation of Coeff. $|\alpha| \cdot \gamma$ with $P_m$ -Loss



# Common Degradation Mechanism / Model in Both Modules



$$P_m \leftarrow \log(C_3) = p(nFF) - q$$

$$P_m \leftarrow C_3^{-2} = \alpha \exp(-\beta V) + \gamma$$

*These degradations are simultaneously occurring within a cell.*

*→ Effect of moisture penetration...?*



# Summary:

$nP_m > \text{ca. } 0.4:$

$$\log(C_3) = p(nP_m) - q$$

$$\rightarrow nP_m = [\log(C_3) + q] / p$$

$\text{ca. } 0.6 > nP_m > \text{ca. } 0.2:$

$$C_3^{-2} = \alpha \times \exp(-\beta \times V) + \gamma$$

$$\rightarrow nP_m = r \exp(-s \cdot |\alpha|) + u$$

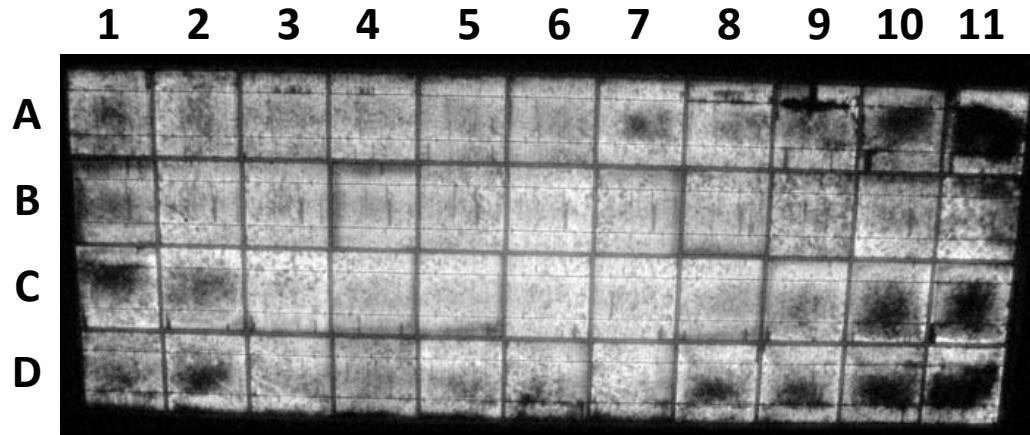
$$\rightarrow nP_m = v \exp(-w \cdot \gamma) + x$$

The parameters ( $\alpha \cdot \beta \cdot \gamma$ ) from both PV modules were completely overlaid each other, as a function of power-loss.

These observations indicate that *a common corrosion-mechanism works in both PV modules*, although the kinetics of corrosion occurring in the respective PV modules is extremely different.

# Outdoor Exposure

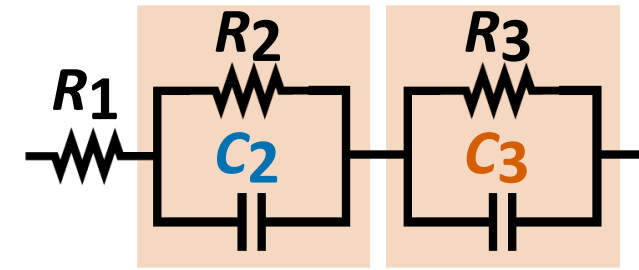
# K-64 PV Module (21 Years in Field)



← K64-A11 Cell

← K64-C11 Cell

← K64-D11 Cell

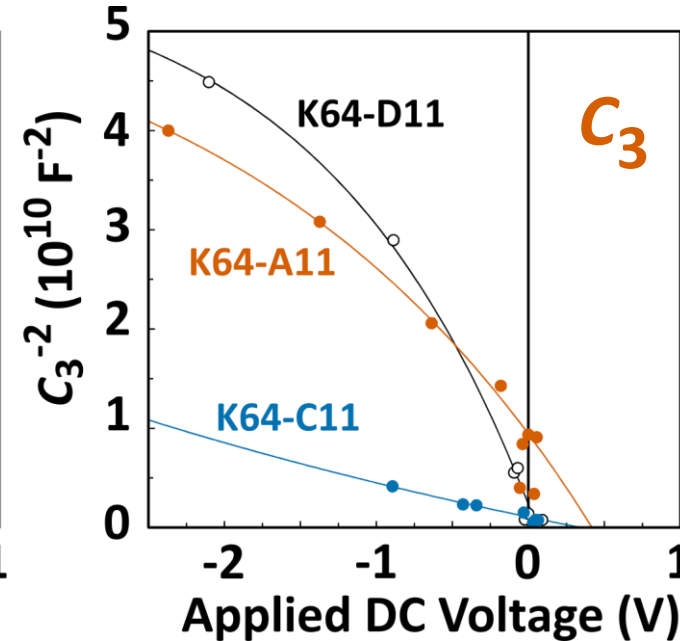
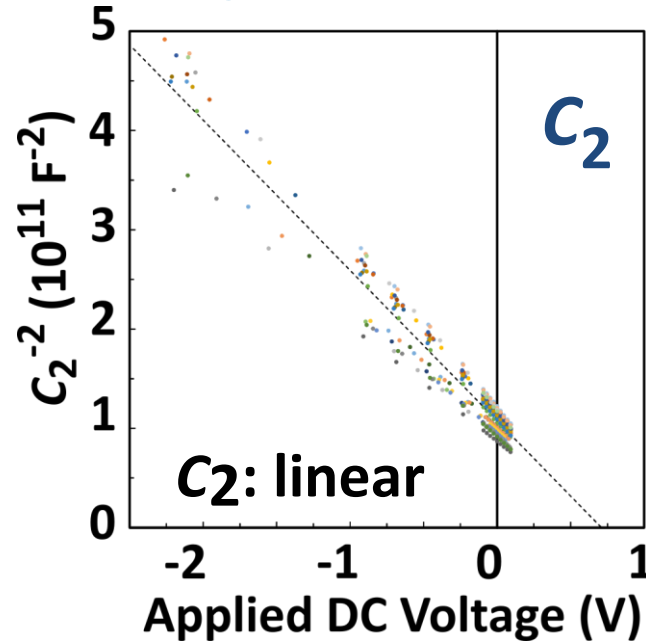


AC Equivalent Circuit

## Mott-Schottky Plots [ $C_2 \cdot C_3$ ]

$$C^{-2} = \frac{2}{qA^2 \epsilon N_D} (V + V_{bi})$$

- C: Capacitance
- V: Applied DC Voltage
- $\epsilon$ : Permittivity
- q: Elementary Charge
- $N_D$ : Doping Density
- $V_{bi}$ : Build-in Potential
- A: Area



**$C_3$ : non-linear**

$$C_3^{-2} = \alpha \exp(-\beta V) + \gamma$$

T. Tanahashi et al.,  
*IEEE J. Photovolt.*, vol. 9,  
no. 3, pp. 741–751, 2019.

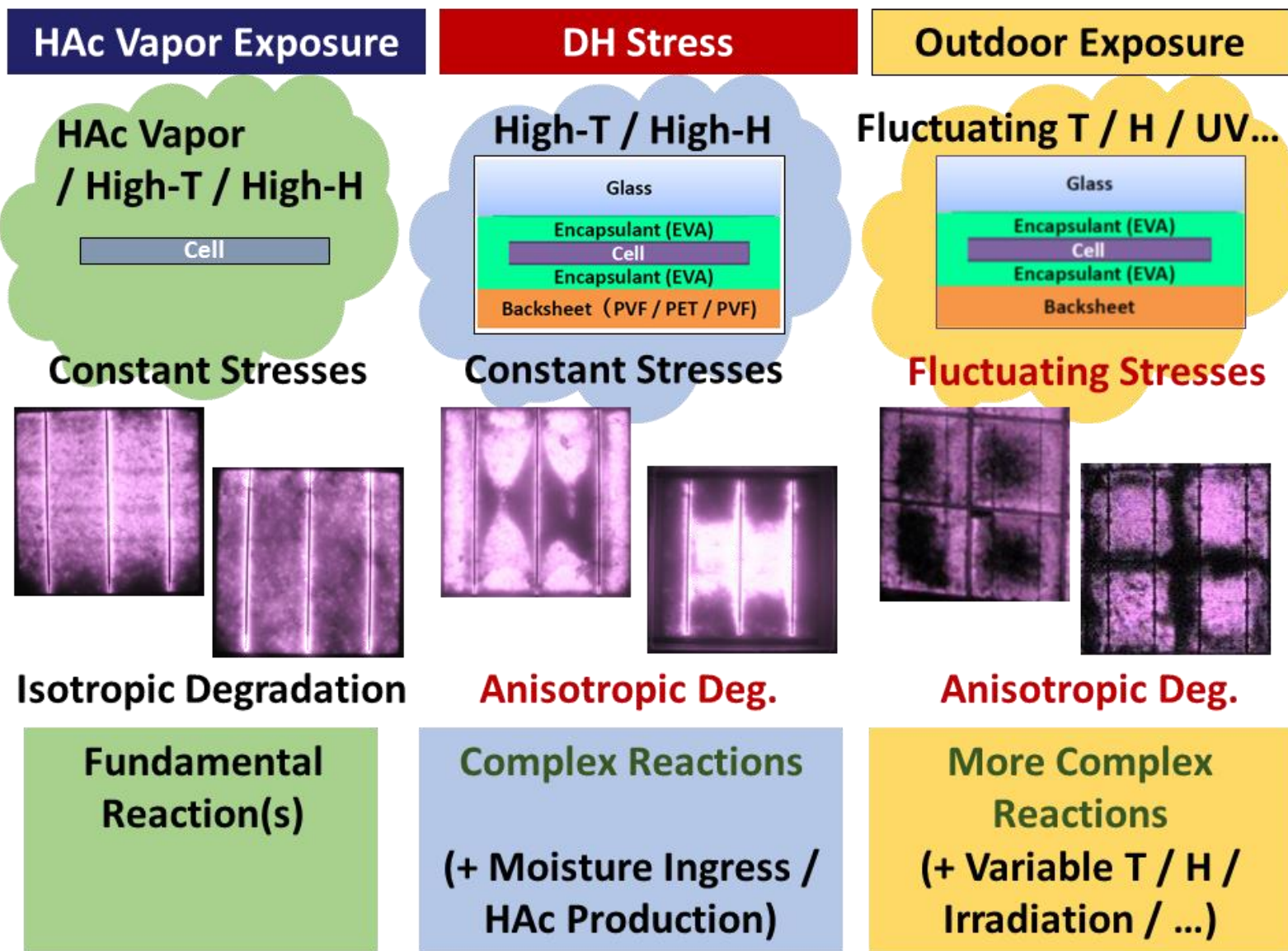
# Thank you for your attention!



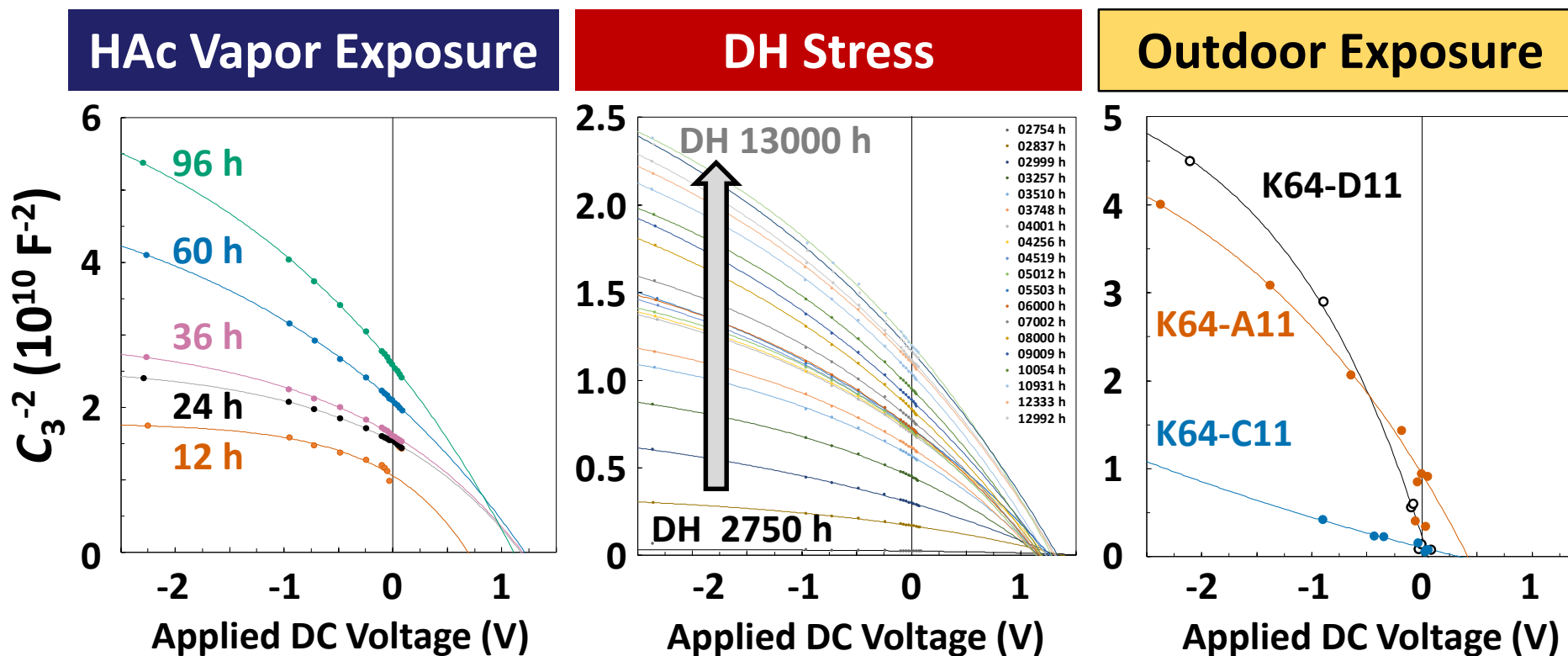
[https://unit.aist.go.jp/rcpv/ci/resources/MegaSolar/Htmls/AIST-MEGA-21\\_01.html](https://unit.aist.go.jp/rcpv/ci/resources/MegaSolar/Htmls/AIST-MEGA-21_01.html)

Backup

# Approach



# Mott-Schottky Plots [ $C_3$ ]



Corrosion mechanisms are quite similar, regardless of whether the PV modules are degraded under field conditions over many years or under accelerated artificial corrosive stress test conditions.